

THE EISENHOWER LIBRARY



3 1151 02671 0826

182,669



The
Orbit of the Planet

'Uranus'

By
Charles A. Horsko
"



Johns Hopkins University.

1892.

The following work is respectfully
submitted as a Thesis for the Degree of Doctor of Philosophy.

John Hopkins University,

1892.

Progr.

The minor planet number (270), "Anahita", is the third known planet in order of distance from the sun in the minor planet group.

This planet has been chosen in order to make a practical application of the theory; first, of determining the elements of a celestial body from four observations; secondly, of correcting the elements thus derived by means of additional observations; and finally as an application of the theory of Special Perturbations.

In making a complete discussion of this subject, since much difficulty is often encountered by students of Astronomy who have not had

practical experience in making numerical calculations, the arrangement of the formulae and the calculation are given quite fully in the following pages, with the hope that the work might prove suggestive to students pursuing for the first time this line of investigation, by making the path much easier to follow.

Determination of the Orbit of 'Anahita'



The work of determining the elements of a comet and of determining the position of the orbit consists in the calculation of what may be called an approximate orbit from three or four observed positions of a celestial body. The orbit thus derived will conform more or less closely to the true orbit according as the observed data are more or less accurate. The value of the latter will not only depend on the skill with which the observations have been made, but also on the assumed positions of the comparison stars. Hence it becomes a matter of the greatest importance in selecting the observations to be used and in computing the elements, to see that the best determined places of the stars of comparison, that can be had, are used.

The second part is the problem of

finding the elements of the orbit of the planet which must be compared with the calculated places of the celestial body. Thus, by means of the discrepancies which are found between the observed and computed places a closer approximation to the true orbit is found.

Finally, the third part consists in finding the influences that any planet may have in producing perturbations upon the celestial body, and in comparing the values of the elements with the lapse of time, from the epoch of the calculation of the planet's orbit.

Part First.

Determination of the elements of an orbit from given
observed places. — Equations which determine the
place the data lead to the elements.

Determination of the place of the orbit to that of the celestial
small, an orbit determined from three observed positions is un-
certain. To obtain an exact result, a fourth position must be
observed places. Under all circumstances this method, while it involves
somewhat more labor, can, nevertheless, be relied upon in its results.

Five elements are to be found from
the given data. The heliocentric co-ordinates and the distance are
functions of these unknown quantities.

The quantities which enter into the work of this investigation is
as follows: —

t	the time	
a	the semi-major axis	
e	the eccentricity of the orbit	
i	the inclination of the orbit to the plane of the ecliptic	
ϵ	mean longitude at epoch, $t = 0$	
π	longitude of the perihelion	
Ω	longitude of the ascending node	
ω	distance of the perihelion from the node, $= \pi - \Omega$	
f	the true anomaly	
E	the eccentric anomaly	
λ	the ~~true~~ anomaly	
r	the radius vector	
k	a constant quantity, termed the Gaussian constant, and having the value	

the six elements of the orbit.
 (1.3.) If seventh element, m , the mass, may be

$$\log a = 8.2355514414 - 10$$

$$c = 3.5500065746, \text{ when expressed in seconds of arc,}$$

a celestial body around the sun, are

$$\frac{d^2x}{dt^2} + k^2 \frac{x}{r^3} = 0,$$

$$\frac{d^2y}{dt^2} + k^2 \frac{y}{r^3} = 0,$$

$$\frac{d^2z}{dt^2} + k^2 \frac{z}{r^3} = 0,$$

or, since,

$$\frac{dx}{dt} = x', \quad \frac{dy}{dt} = y', \quad \frac{dz}{dt} = z',$$

we can write

$$\frac{d^2x'}{dt^2} + k^2 \frac{x'}{r^3} = 0,$$

$$\frac{d^2y'}{dt^2} + k^2 \frac{y'}{r^3} = 0,$$

$$\frac{d^2z'}{dt^2} + k^2 \frac{z'}{r^3} = 0;$$

the integration of the above equations expresses the integrals in the form

$$\begin{matrix} x, y, z, \\ x', y', z' \end{matrix} = c_1(a, e, i, \pi, b, e, t);$$

and so with we find

$$\begin{matrix} a, e, i, \\ \pi, b, e \end{matrix} = c_2(x, y, z, x', y', z')$$

six functions of the seven variables, which may be regarded as constant.

Since the above equations are first order, we obtain

The observations themselves do not afford the means of determining immediately the heliocentric co-ordinates, since they do not furnish directly the geocentric distances.

Let ξ, η, ζ , be the geocentric rectangular co-ordinates of the celestial body, which in terms of the polar co-ordinates are given by the formulae

$$\xi = \rho \cos \lambda \cos \beta$$

$$\eta = \rho \sin \lambda \cos \beta$$

$$\zeta = \rho \sin \beta$$

where λ and β are the longitude and latitude given by observation, and ρ the geocentric distance.

By referring to the Nautical Almanac we find the geocentric co-ordinates of the sun X, Y, Z , from the data of our observations. We have then to express the heliocentric co-ordinates of the celestial body by the formulae

$$x = \xi - X$$

$$y = \eta - Y$$

$$z = \zeta - Z$$

where x, y, z are the heliocentric co-ordinates of the body.

Since x , y , and z are functions of the
 elements of the orbit, each one of the observations gives
 an equation of three elements. Three equations of this
 kind, however, will not determine the elements of the orbit,
 because the geocentric distance ρ is not known. A second observation will introduce only one
 new unknown quantity, ρ , and the third observation, which
 it introduces three new quantities, will only add one new unknown
 quantity. Thus three observations will give nine equations containing
 nine unknown quantities, and, with the exception where the inclination
 is small, these nine equations would solve the problem.

Let us first establish the conditions to
 be fulfilled for three given positions of the celestial body in space,
 found in the same plane passing through the center of the sun,
 and then it becomes very simple to pass to four places.

Designating respectively by x', y', z' ,
 x'', y'', z'' , and x''', y''', z''' the coordinates of the three
 given positions. The equation of the plane which

passes through the origin of co-ordinates (the center of the sun) and these three positions, gives

$$Ax' + By' + Cz' = 0$$

$$Ax'' + By'' + Cz'' = 0$$

$$Ax''' + By''' + Cz''' = 0$$

In this case A , B and C are functions of the longitude of the node and of the inclination of the orbit.

These three quantities can easily be eliminated in the following manner: multiply the first equation by z' and the second by z'' , then subtracting

$$A(x'z'' - x''z') + B(y'z'' - y''z') = 0.$$

From the first and the third in the same manner

$$A(x'z''' - x'''z') + B(y'z''' - y'''z') = 0.$$

Multiply now the first of these last equations by $y'z'' - y''z'$ and the second by $y''z' - y'z''$ and add; then will B be eliminated and we have

$$A \begin{bmatrix} x'y'z''z''' - x''y'z'z''' \\ -x'y'''z'z'' + x'y'''z'z' \\ +x'y'z''z''' - x'y'z'z''' \\ -x'''y'z'z'' + x'''y'z'z'' \end{bmatrix} = 0;$$

the first and the sixth terms vanish and the others contain Az' as a common factor. As that quantity will generally be different from zero, and as the second member of the formula is nil, in suppressing the factor Az' , we obtain for the equation of condition relative to the plane of the orbit,

$$0 = -x'y'z''' - x'y'''z'' + x''y'''z' + x'y''z''' + x''y'z'' - x'''y''z'; \quad (1)$$

This equation can be written under three different forms

$$0 = x'(y''z''' - y'''z'') - x''(y'z''' - y'''z') + x'''(y'z'' - y''z');$$

$$0 = y'(x''z''' - x'''z'') - y''(x'z''' - x'''z') + y'''(x'z'' - x''z');$$

$$0 = z'(x''y''' - x'''y'') - z''(x'y''' - x'''y') + z'''(x'y'' - x''y');$$

The factors in parenthesis have a geometric significance: for example, in the first of these equations, its factors contain respectively the co-ordinates of the projections upon the plane of yz , of the second and third, first and third, first and second positions of the celestial body. By considering in the same way the second and third equations, we see that the factors in parenthesis are the co-ordinates of the analogous projections upon the plane xz and xy . These factors in question are not double for any of the three positions of the

projections and the origin.

Designate by ixy, ixz, iyz , the inclination of the plane of the orbit, respectively, to the three coordinate planes xy, xz, yz . In replacing double the area of the triangle composed between the three radii vectors, introduce the symbols

$$[r'r''] : [r''r'''] \text{ and } [r'r''']$$

which represent, respectively, double the triangular areas, between the first and second, second and third, and first and third positions.

We will have the triangle

$$\Delta = \frac{1}{2} [r'r'''] \cos ixy.$$

Transforming in the same way all the factors which enter into the last equations, we find the relations.

(vide next page.)

$$[r''r'''] \cos i y z = (y''z''' - y'''z'')$$

$$[r' r'''] \cos i y z = (y'z''' - y'''z')$$

$$[r' r''] \cos i y z = (y'z'' - y''z')$$

$$[r''r'''] \cos i x z = (x''z''' - x'''z'')$$

$$[r' r'''] \cos i x z = (x'z''' - x'''z')$$

$$[r' r''] \cos i x z = (x'z'' - x''z')$$

$$[r''r'''] \cos i x y = (x''y''' - x'''y'')$$

$$[r' r'''] \cos i x y = (x'y''' - x'''y')$$

$$[r' r''] \cos i x y = (x'y'' - x''y')$$

Introducing these values into the preceding equations and writing

$$\frac{[r' r'']}{[r' r''']} = n'' ; \quad \frac{[r'' r''']}{[r' r''']} = n ;$$

we find

$$x'' = n x' + n'' x'''$$

$$y'' = n y' + n'' y'''$$

$$z'' = n z' + n'' z'''$$

to be satisfied by the heliocentric co-ordinates of the three given positions in order that they may be situated in the same plane passing through the sun.

If the heliocentric areas are not too great, we can replace the relations of the triangular areas by a convergent series. The first terms of these series will depend upon the known intervals of time and the radius vector which are simple functions of the heliocentric co-ordinates. These relations can be approximately calculated without much difficulty.

By use of the relations (b) we will replace now in (a) the heliocentric co-ordinates of the celestial body, by their values in terms of the geocentric co-ordinates of the sun. The introduction of polar co-ordinates into these formulae leads to the question as to what fundamental plane it is most convenient to refer these co-ordinates. The choice of the fundamental plane is generally arbitrary.

The co-ordinate z referred to the ecliptic plane, always vanishes at the equinoxes. It follows that the system of latitude and longitude is especially adapted

$$\begin{aligned}
 \frac{1}{a} &= \frac{1}{t} [1 - Y' x + \dots] \\
 \frac{1}{a'} &= \frac{1}{t'} [1 - Y' x + \dots] \\
 \frac{1}{a''} &= \frac{1}{t''} [1 - Y'' x + \dots] \\
 \frac{1}{a'''} &= \frac{1}{t'''} [1 - Y''' x + \dots]
 \end{aligned}
 \tag{3}$$

The method for determining the expansion for the sector of the triangle permits us to express the dependent quantities Y as functions of the corresponding rotations. Referring to that which is done for the intervals of time, designate by η , the ratio of the sector to the triangle, and for the dependent quantities, the η 's in accents, and we have identical series for

$$\frac{1}{a} = \frac{1}{t} \cdot \frac{1}{\eta} = \frac{1}{t} \left[1 - \frac{(\eta' - 1) - (\eta' - 1)^2}{1} \right]$$

$$\frac{1}{a'} = \frac{1}{t'} \cdot \frac{1}{\eta'} = \left[1 - \frac{(\eta'' - 1) - (\eta'' - 1)^2}{\eta''} \right]$$

$$\frac{1}{a''} = \frac{1}{t''} \cdot \frac{1}{\eta''} = \left[1 - \frac{(\eta''' - 1) - (\eta''' - 1)^2}{\eta'''} \right]$$

$$\frac{1}{a'''} = \frac{1}{t'''} \cdot \frac{1}{\eta'''} = \left[1 - \frac{(\eta^{(4)} - 1) - (\eta^{(4)} - 1)^2}{\eta^{(4)}} \right]$$

Comparing this expression with the form

(3) we can finally write the approximate secular gap arising at an order $2n+1$ as

$$Y'' = \frac{(\eta' - 1) - (\eta''' - 1)}{\eta'^2}$$

$$Y' = \frac{(\eta' - 1) - (\eta''' - 1)}{\eta'^2}$$

(3)

$$Y_0' = \frac{(\eta' - 1) - (\eta''' - 1)}{\eta_0' x}$$

$$Y_0' = \frac{(\eta' - 1) - (\eta_0''' - 1)}{\eta'' x}$$

The excess of η over unity can be

expressed in terms of η by the relation $\eta - 1 = \frac{1}{\eta} (\eta^2 - 1)$ the complete

series approximations. (See Tables for solving) the equation

$$\eta - 1 = \frac{1}{\eta} \left(\eta^2 + \frac{1}{q} \right) \quad (4)$$

By substituting $\eta = 1 + \frac{1}{q}$ in the r.h.s. (4)

and multiplying, we will now reduce equations (4) to the

form for computing the value of ξ'' as follows:-

$$\xi'' = \left(\frac{1}{L} + \frac{1}{L'} + \frac{1}{L''} + \frac{1}{L'''} + \frac{1}{L''''} \right) \left(\frac{A'}{E'} \cdot Y' - \frac{Z''}{L} \cdot \frac{Y'}{L'} \right)$$

$$\xi = \left(\frac{1}{L} + \frac{1}{L'} + \frac{1}{L''} + \frac{1}{L'''} + \frac{1}{L''''} \right) \left(\frac{A'}{E'} \cdot Y' - \frac{Z''}{L} \cdot \frac{Y'}{L'} \right)$$

Let $\xi = \xi_1 + \xi_2 + \xi_3 + \xi_4 + \xi_5$

$$\xi_1 = \frac{1}{L} \cdot \frac{A'}{E'} = \frac{1}{L} \cdot \frac{Y'}{E''} + \frac{Z''}{E''}$$

.

$$\xi_2 = \frac{1}{L'} \cdot \frac{A'}{E'} = \frac{1}{L'} \cdot \frac{Y'}{E''} + \frac{Z''}{E''}$$

$$\xi_3 = \frac{1}{L''} \cdot \frac{A'}{E'} = \frac{1}{L''} \cdot \frac{Y'}{E''} + \frac{Z''}{E''}$$

$$\xi_4 = \frac{1}{L'''} \cdot \frac{A'}{E'} = \frac{1}{L'''} \cdot \frac{Y'}{E''} + \frac{Z''}{E''}$$

$$\xi_5 = \frac{1}{L''''} \cdot \frac{A'}{E'}$$

$$\xi_6 = \frac{1}{L''''} \cdot \frac{Y'}{E''}$$

$$\xi_7 = \frac{1}{L''''} \cdot \frac{Z''}{E''} = \frac{1}{L''''} \cdot \frac{Y'}{E''} + \frac{Z''}{E''}$$

$$a = a_0 + (b - b_0)x + (c' + d_0)\xi'$$

$$\xi' = a + bx + d\xi'$$

$$\xi' = a_0 + b_0x + d_0\xi'$$

Subtract and solve for ξ' ; then add and we will have

$$\xi' = \frac{(a - a_0) + (b - b_0)x}{(d' - d)}$$

$$\xi' = \frac{1}{2}[(a + a_0) + (b + b_0)x + (d' + d_0)\xi']$$

Here a and a_0 , d and d_0 are constants so long as the intervals t and t_0 are not changing, but b and b_0 are variables, while Y depends upon terms of the 1st and 2nd order. In practice the Y 's can be replaced by approximate values, which are functions of the intervals of time and of the radii vectors r and r' . With these transformations which we have introduced the formulas are most convenient for the calculation of a planetary orbit. In making

the first approximation we begin the calculation by using the

$$\frac{1}{u} = \frac{1}{v} [1 - Y_0']$$

$$\frac{1}{u} = \frac{1}{v} [1 - Y_0' + Y_0'']$$

$$\frac{1}{u} = \frac{1}{v} [1 - Y_0' + Y_0'']$$

$$\frac{1}{u} = \frac{1}{v} [1 - Y_0' + Y_0'']$$

here we substitute for the exact values of the Y_0' as follows:

$$Y_0'' = \frac{1}{2} (v' - v'')$$

$$Y_0''' = \frac{1}{2} (v'' - v''')$$

$$Y_0^{(4)} = \frac{1}{2} (v' - v''')$$

$$Y_0^{(5)} = \frac{1}{2} (v''' - v^{(4)})$$

and substituting the values of Y_0 and Y'_0 in (1) and (2) respectively,

we get

$$Y'' = \frac{(\eta' - 1) - (\eta'' - 1)}{\eta'x}$$

$$Y' = \frac{(\eta' - 1) - (\eta'' - 1)}{\eta'x}$$

$$Y''_0 = \frac{(\eta'_0 - 1) - (\eta''_0 - 1)}{\eta'_0x}$$

$$Y'_0 = \frac{(\eta''_0 - 1) - (\eta'''_0 - 1)}{\eta''_0x}$$

with which deduced values of the Y 's a second hypothesis can be formed. Proceeding in this way the equations can be written in the convenient form for computation as follows:—

$$a = (1) + (2) + c$$

$$b = (1)Y' + (2)Y''$$

$$a_0 = (1)_0 + (2)_0 + c_0$$

$$b_0 = (1)_0Y'_0 + (2)_0Y''_0$$

$$I = a_0 - a$$

$$II = (3) - (3)_0$$

$$u = b - b_c$$

$$Y = (3) Y'_c - (3) Y'_f$$

$$Y = \frac{1}{2} (u_0 + u)$$

$$Y = \frac{1}{2} (u + \omega_0)$$

$$Y = \frac{1}{2} (b + b_0)$$

$$Y = \frac{1}{2} [(3) Y'_c + (3) Y'_f]$$

$$Y_{111}$$

$$w = \frac{1}{t''} \cdot \frac{A'}{E''}$$

$$w_0 = \frac{1}{t''} \cdot \frac{A'_c}{E''_c}$$

$$w = \frac{1}{t''} \cdot \frac{B'}{E''}$$

$$w_c = \frac{1}{t''} \cdot \frac{B'_c}{E''_c}$$

$$w = \frac{1}{t''} \cdot \frac{E'}{E''}$$

$$(3)_c = \frac{E'}{E''} \cdot \frac{E'_c}{E''_c}$$

$$U = \frac{C'}{E''}$$

$$U_c = \frac{C'_c}{E''_c}$$

We now have certain equations wherein the geocentric distances ξ and ξ'' and the quantity x , are simple functions of r'' and r''' . By combining these equations with the relations, which the extreme observations furnish between the same quantities, we will obtain ξ' and ξ'' by approximations.

In the determination of the orbit in the present case, in the first trial we have put $x = 0.025$ as an approximate value to x and note, in the successive trials we make upon this value, we are gradually coming to it. We will calculate the value corresponding to ξ' and ξ'' by aid of the following relations.

$$\xi' = \frac{\text{I} + \text{III}x}{\text{II} + \text{IV}x}$$

$$\xi'' = \text{V} - \text{VI}x + [\text{VII} - \text{VIII}] \xi'$$

where we use the above given relations. Employing now the following auxiliary relations:-

(vide next page)

$$\cos \lambda' = \cos \beta' \cos (\lambda' - \lambda')$$

$$\sin \lambda' \cos P' = \cos \beta' \sin (\lambda' - \lambda')$$

$$\sin \lambda' \sin P' = \sin \beta'$$

$$\cos \lambda'' = \cos \beta'' \cos (\lambda'' - \lambda'')$$

$$\sin \lambda'' \cos P'' = \cos \beta'' \sin (\lambda'' - \lambda'')$$

$$\sin \lambda'' \sin P'' = \sin \beta''$$

$$i_1 = R' \cos \lambda'$$

$$B' = R' \sin \lambda'$$

$$i_m = R'' \cos \lambda''$$

$$B'' = R'' \sin \lambda''$$

With these relations we can now deduce from ξ' and ξ'' the radii vectors r' and r'' by the formulae: -

$$\frac{\xi' - i_1}{B'} = \tan \theta'$$

$$r' = (\xi' - i_1) \operatorname{cosec} \theta'$$

$$\frac{\xi'' - i_m}{B''} = \tan \theta''$$

$$r'' = (\xi'' - i_m) \operatorname{cosec} \theta''$$

and also

$$x = \frac{r'}{r''} = \frac{B''}{B'} \frac{\sin \theta''}{\sin \theta'}$$

(
The radii vectors lead themselves

to the value of x . The final value of x will now coincide with the initial value, except by chance our first hypothesis should be exact.

This can scarcely be expected and several approximations have to be made before a final value is found which shall agree with the initial value.

Having obtained the values of r and r'' , ξ and ξ'' which satisfy the equations, if the approximations obtained can be regarded sufficient for the adopted hypothesis, it only remains to proceed according to the general method of deducing the elements from ξ and ξ'' . If the approximations do not prove sufficient then additional hypotheses must be made.

On account of the relative smallness of the inclination of the orbit, the geocentric motion in longitude does not affect the geocentric motion in latitude, thus with regard to the two great circles, which replace the mean observations, without introducing sensible error, we can put:

$$I = 90^\circ \quad I_0 = 90^\circ$$

$$\Pi = \lambda'' \quad \Pi_0 = \lambda''$$

we will simply say, as in the definition (1)

Having now briefly treated the theory
of the calculations we will in the following section collect the
necessary formulae and give the necessary proofs.



Collection of Formulas

Collecting together the necessary formulas used in making the calculations of the elements in the order in which they will be used, and in the form most convenient for computing, we will have in the first place the four normal places, which will give the geocentric place of the planet referred to the mean equinox and equator of the beginning of the year which we have chosen as our epoch and for a given meridian which we will choose as that of Greenwich.

	Alt.	West. Longitude	Declination
1	T'	α'	δ'
2	T''	α''	δ''
3	T_0''	α_0''	δ_0''
4	T'''	α'''	δ'''

The four observed positions of the

stand are to be transformed into longitude and latitude by the
~~the following relations~~

$$\sin \delta = \cos \epsilon \sin \delta' - \cos \delta' \sin \epsilon \sin \alpha;$$

$$\cos \delta \sin h = \sin \epsilon \sin \delta' + \cos \delta' \cos \epsilon \sin \alpha;$$

$$\cos \delta \cos h = \sin \delta' \cos \alpha;$$

$$\sin u = \sin \delta' / \sin \epsilon$$

$$\cos u = \cos \delta' \sin \alpha / \sin \epsilon$$

$$\sin \delta = h \sin (u - \epsilon)$$

$$\sin \delta \sin h = h \cos (u - \epsilon),$$

$$\cos \delta \cos h = \cos \delta' \cos \alpha$$

where follow the data:

	h	longitude	latitude	sin longitude	sin latitude
1	δ'	δ'	δ'	δ'	δ'
2	δ''	δ''	δ''	δ''	δ''
3	δ'''	δ'''	δ'''	δ'''	δ'''
4	δ''''	δ''''	δ''''	δ''''	δ''''

—.

$$E' = \sin (\lambda'' - \lambda') \cos \beta'$$

$$E'' = \sin (\lambda''' - \lambda'') \cos \beta''$$

$$E'_0 = \sin (\lambda''_0 - \lambda') \cos \beta'$$

$$E''_0 = \sin (\lambda''' - \lambda''_0) \cos \beta''$$

$$A = R' \sin (\lambda' - \lambda'') : E''$$

$$B = R'' \sin (\lambda'' - \lambda''') : E'''$$

$$C = R''' \sin (\lambda''' - \lambda''') : E''''$$

$$D = E' : E'''$$

$$A_0 = R' \sin (\lambda' - \lambda'_0) : E'_0$$

$$B_0 = R'' \sin (\lambda''_0 - \lambda''_0) : E''_0$$

$$C_0 = R''' \sin (\lambda''' - \lambda''_0) : E''_0$$

$$D_0 = E'_0 : E''_0$$

$$\cos \lambda' = \cos \beta' \cos (\lambda' - \lambda')$$

$$\sin \lambda' \cos \beta' = \cos \beta' \sin (\lambda' - \lambda')$$

$$\sin \lambda' \sin \beta' = \sin \beta'$$

$$\cos \lambda''' = \cos \beta''' \cos (\lambda''' - \lambda''')$$

$$\sin \lambda''' \cos \tau''' = \cos \beta''' \sin (\lambda''' - \lambda''')$$

$$\sin \lambda''' \sin \tau''' = \sin \beta'''$$

$$r' = R' \cos \lambda'$$

$$z' = R' \sin \lambda'$$

$$r'_z = R' \sin (\lambda' - \lambda')$$

$$r'_e = - R' \cos (\lambda' - \lambda')$$

$$r''' = R''' \cos \lambda'''$$

$$z''' = R''' \sin \lambda'''$$

$$r'''_z = R''' \sin (\lambda''' - \lambda''')$$

$$r'''_e = - R''' \cos (\lambda''' - \lambda''')$$



II.

$$I = \frac{1}{2} (T''' - T'')$$

$$I' = k (T''' - T')$$

$$I'' = -k (T''' - T')$$

$$\log k = 8.2255514$$

$$I_0' = k (T''' - T_0'')$$

$$I_0'' = k (T_0''' - T')$$

$$A = \frac{t'}{t''} \cdot A$$

$$B = -\frac{t'}{t''} \cdot B$$

$$D = \frac{t'}{t''} \cdot D$$

$$A_0 = \frac{t_0'}{t_0''} \cdot A_0$$

$$B_0 = -\frac{t_0''}{t_0'} \cdot B_0$$

$$D_0 = \frac{t_0'}{t_0''} \cdot D_0$$

$$u = (v) - (z) + c$$

$$I = u_0 - u$$

$$V = \frac{1}{2} (u_0 + u)$$

$$u_0 = (v)_0 + (z)_0 + c_0$$

$$II = (z) - (z)_0$$

$$\overline{II} = \frac{1}{2} [(z) + (z)_0]$$

$$t = (1)Y'' + (2)Y'$$

$$\underline{m} = t - t_0$$

$$\underline{v} = \frac{1}{2}(t + t_0)$$

$$t_0 = (1)_0 Y''_0 + (2)_0 Y'_0$$

$$\underline{v} = (3)_0 Y'' + (3) Y'$$

$$\underline{v} = \frac{1}{2}[(3)_0 Y''_0 + (3) Y'']$$

$$Y' = \frac{1}{3}(t' - t'')$$

$$Y' = \frac{1}{3}(t'' - t''')$$

$$Y'' = \frac{1}{3}(t''' - t''')$$

$$Y''' = \frac{1}{3}(t^{(4)} - t^{(4)})$$

$$\xi$$

$$\xi' = \frac{I + III \lambda}{II + II \lambda}$$

$$\xi'' = \lambda - \lambda I \sqrt{II} - \lambda III \lambda \xi'$$

$$\sin \theta = \frac{\xi' - r'}{\xi'}$$

$$\sin \theta'' = \frac{\xi'' - r''}{\xi''}$$

$$\lambda = \frac{1}{(r' + r'')^2}$$

$$r' = (\xi' - r_m) \operatorname{cosec} \theta'$$

$$r'' = (\xi'' - r_m) \operatorname{cosec} \theta''$$

II.

$$r' \cos (\lambda' - \lambda') \cos b' = \xi' \cos \delta' + R'_c$$

$$r' \sin (\lambda' - \lambda') \cos b' = R'_s$$

$$r'' \cos (\lambda'' - \lambda'') \cos b'' = \xi'' \cos \delta'' + R''_c$$

$$r'' \sin (\lambda'' - \lambda'') \cos b'' = R''_s$$

$$r' \sin b' = \xi' \sin \delta'$$

$$r'' \sin b'' = \xi'' \sin \delta''$$

$$\sin^2 \frac{\epsilon}{2} = \sin^2 \frac{\epsilon}{2} (\lambda'' - \lambda') \cos b' \cos b'' + \sin^2 \frac{\epsilon}{2} (b'' - b')$$

$$\frac{n}{n''} = \frac{r'}{r''} (1 - x Y'')$$

$$\frac{1}{n''} = \frac{1}{r''} (1 - x Y')$$

$$\frac{n_c}{n'_c} = \frac{r'_c}{r''_c} (1 - x Y''_c)$$

$$\frac{1}{n'_c} = \frac{1}{r''_c} (1 - x Y'_c)$$

$$r'' \sin 2f''' = r''' n'' \sin 2f''$$

$$r'' \cos 2f''' = r' n + r''' n'' \cos 2f''$$

$$r''_c \sin 2f'''_c = r'' n'_c \sin 2f''$$

$$r''_c \cos 2f'''_c = r' n'_c + r''' n''_c \cos 2f''$$

And for a check use the formulas :

$$r'' \sin 2f''' = r' n \sin 2f''$$

$$r'' \cos 2f''' = r''' n'' + r' n \cos 2f''$$

$$r''_c \sin 2f'''_c = r' n'_c \sin 2f''$$

$$r''_c \cos 2f'''_c = r''' n''_c + r' n'_c \cos 2f''$$

$$\sqrt{11}$$

	r	r'	r''	r'''	r''''	r'''''
r	r	r'	r''	r'''	r''''	r'''''
r'	r'	r''	r'''	r''''	r'''''	r''''''
r''	r''	r'''	r''''	r'''''	r''''''	r'''''''
r'''	r'''	r''''	r'''''	r''''''	r'''''''	r''''''''
r''''	r''''	r'''''	r''''''	r'''''''	r''''''''	r'''''''''

$$m = \frac{1}{(a - c - f'(x))'}$$

$$h = \frac{m}{\frac{5}{6} + k + \xi}$$

$$\lambda = \frac{\sin^2 \frac{1}{2} \theta + \tan^2 2 \omega}{2}$$

$$\tan (15^{\circ}+10^{\circ})=\sqrt{\frac{r_1}{r}}$$

$$(11-1) = \frac{11}{11^2} (11 + \frac{1}{9})$$

The table gives with the argument θ the value $\log \eta$

the table gives with the argument $\frac{m}{\eta^2} - t = x$ the value ξ

As a first value of x take $x = \sin^2 \frac{1}{2} \theta$

$$\underline{\gamma'''}$$

$$\gamma'' = \frac{(\gamma'-1) - (\gamma'''-1)}{\eta' x}$$

$$\gamma' = \frac{(\gamma''-1) - (\gamma'''-1)}{\eta'' x}$$

$$\gamma''_0 = \frac{(\gamma'_0-1) - (\gamma'''-1)}{\eta'_0 x}$$

$$\gamma'_0 = \frac{(\gamma''-1) - (\gamma'''_0-1)}{\eta'' x}$$

13

$$m'' = \frac{m''}{(\cos \theta - \frac{1}{r})}$$

$$I_{\omega}(\omega) = \sqrt{\frac{1}{r}}$$

$$f = \frac{\sin^2 \theta'' + \tan^2 \omega''}{\cos \theta''}$$

$$-11 = \frac{m''}{f' + \frac{2}{r} + \frac{2}{\sigma}}$$

$$\sin \theta = \frac{m''}{f} - 1$$

Ans.

$$\cos \frac{1}{2} (f'' + g) \tan \frac{1}{2} w'' = \sin \frac{1}{2} (F - G) \cos \frac{1}{2} q(\gamma)^2$$

$$\sec \frac{1}{2} (f'' - g) \tan \frac{1}{2} w'' = \sin \frac{1}{2} (F + G) \sin \frac{1}{2} q(\gamma)^2$$

$$\sin \frac{1}{2} (f'' + g) \sec \frac{1}{2} w'' = \cos \frac{1}{2} (F - G) \cos \frac{1}{2} q(\gamma)^2$$

$$\sin \frac{1}{2} (f'' - g) \sec \frac{1}{2} w'' = \cos \frac{1}{2} (F + G) \sin \frac{1}{2} q(\gamma)^2$$

Ques 10.

$$(\gamma)^2 = \frac{\gamma^2 m'' \cos f''}{\eta''}$$

$$V''' = F' + f' r'$$

$$V' = F - f' r'$$

$$E_m = G + G_0$$

$$E_1 = \lambda_1 - \lambda_2$$

$$\Delta 1.$$

$$\frac{\partial}{\partial t} = \frac{1}{\sqrt{1 - v^2/c^2}} \frac{\partial}{\partial t'}$$

$$\frac{\partial}{\partial x} = \frac{v}{c^2} \frac{\partial}{\partial t} + \frac{\partial}{\partial x'}$$

$$\frac{\partial}{\partial y} = \frac{\partial}{\partial y'}$$

$$\frac{\partial}{\partial z} = \frac{\partial}{\partial z'}$$

$$k_0 k'' = 3.55000066$$

$$M' = E_f - \epsilon'' \sin E_f$$

$$M'' = E_f - \epsilon' \sin E_f$$

$$\frac{M'}{M''} = \frac{E_f - \epsilon'' \sin E_f}{E_f - \epsilon' \sin E_f}$$

$$\bar{y}_{11}$$

$$\tan \theta' = \tan i \sin (\theta' - \delta)$$

$$\tan u' = \tan (\theta' - \delta) \sec i$$

$$\frac{\tan \theta'' - \tan \theta' \cos (\theta'' - \theta')}{\sin (\theta'' - \theta')} = \tan i \cos (\theta' - \delta)$$

$$\tan u' = \tan (\theta'' - \delta) \sec i$$

.....

$$u'' - u' = \frac{1}{j}$$

$$\tau = u' + v - v'$$

$$\tau = u'' + v - v''$$



Computation of the Orbit.

The following normal places are derived from observations of planet (270) for the purpose of computing the elements of the orbit.

Date & Time			$\alpha.$			$\delta.$			
1882.	October.	12.5	1	21	55.47	+	11°	50'	10"
	December	16.5	0	21	55.11	+	8	58	38.0
1883.	January,	11.5	1	21	55.16	+	10	50	52.7
	February,	11.5	2	21	55.12	-	15	51	58.0

The reduction of the right ascension to the arc gives

Date & Time		$\alpha.$		
1882	October 12.5	12	10'	52.0
	December 16.5	12	21	16.6
1883	January 11.5	22	51	52.4
	February 11.5	21	52	51.0

The computation according to the following formulae for converting α and δ into h and β is as follows:

I	II	III	IV	V
$\sin \alpha$	0.9970317	0.3472879	0.5820586	0.7128200
$\cos \alpha$	0.999960264	0.9355289	0.9321425	0.9312744
$\sin \delta$	0.99773525	0.9589769	0.6627529	0.6223523
$\sin \delta = h \sin \alpha$	0.3173922	0.1655537	0.261112	0.2641009
$\cos \delta = h \cos \alpha$	0.4882581	0.3425168	0.5747341	0.7106874
$\tan \delta$	0.8283311	0.8260169	0.6864972	0.651225
α	34° 1' 16".4	30° 11' 11".2	28° 54' 48".1	28° 2' 35".8
δ	23° 27' 7".5	22° 2' 7".1	23° 27' 7".2	22° 2' 7".5
$\sin \alpha$	0.7478001	0.7455217	0.6404711	0.6164996
$\alpha - \delta$	10° 34' 8".9	10° 2' 4".1	2° 27' 37".9	0° 58' 27".0
$\cos(\alpha - \delta)$	0.9925686	0.9928502	0.9995994	0.9999972
$\tan h$	0.5695921	0.4250240	0.6227514	0.7514103
$\sin \mu$	0.2624512	0.2551912	0.6327721	0.2304897
$\sin \beta$	0.583304311	0.6752152	0.5835235	0.9519000
$\cos \beta \sin h$	0.5621607	0.4158743	0.6203508	0.7514103
$\cos \beta \cos h$	0.9675092	0.9042055	0.9583894	0.9168003
$\tan \beta$	0.5943525	0.4516685	0.6619614	0.8345472
β	3° 1' 14".1	2° 43' 27".7	1° 1' 25".0	0° 3' 58".5
γ	21° 2' 10".9	15° 1' 10".9	24° 2' 45".2	24° 2' 45".2

The α and δ in the fourth and fifth columns are true values being approximately $3^{\circ}.8$ and $4^{\circ}.0$, respectively.

The corrections for the precession for the co-ordinates α are to be made as follows:

Declination	($\Delta\delta$)	+ $0^{\circ}.1$	+ $0^{\circ}.9$	+ $0^{\circ}.2$	+ $0^{\circ}.4$
Right Ascension	($\Delta\alpha$)	+ $11^{\circ}.0$	+ $6^{\circ}.1$	- $1^{\circ}.1$	- $2^{\circ}.1$

Applying these corrections to the α and δ as deduced above we obtain the reduced positions of the planet referred to the ecliptic and equinox for the epoch 1888.0. The longitude and radius vector of the sun are signed in like manner to the epoch.

(vide next page)

Notes on the ...

1887		1888		1889	
October	12.5	21	21	21	21
November	16.5	21	21	21	21
1888. January	11.5	21	21	21	21
February	6.5	21	21	21	21
1890		1891		1892	
October	12.5	21	21	21	21
November	16.5	21	21	21	21
January	11.5	21	21	21	21
February	6.5	21	21	21	21

The computation according to the
formulas given in section I is as follows:

$$(1) \quad (1.1) \quad (1.2) \quad (1.3) \quad (1.4) \quad (1.5) \quad (1.6) \quad (1.7) \quad (1.8) \quad (1.9) \quad (1.10)$$

Table I.

$$\begin{aligned} \lambda' - \lambda'' &= 1.26084 \\ \lambda' - \lambda''' &= 1.26084 \end{aligned}$$

$$\begin{aligned} \sin(\lambda' - \lambda'') &= 0.0426084 \\ \cos \beta' &= 0.9999999 \\ \sin(\lambda''' - \lambda'') &= 0.5174277 \\ \cos \beta''' &= 0.9999999 \end{aligned}$$

$$\begin{aligned} \log E' &= 0.0416900 \\ \log E''' &= 0.5174277 \end{aligned}$$

$$\begin{aligned} \lambda' - \lambda'' &= 1.54 \quad 1.3 \quad 2.7 \\ \lambda' - \lambda''' &= 2.19 \quad 1.4 \quad 10.3 \\ \lambda' - \lambda''' &= 3.0 \quad 3.4 \quad 5.1 \end{aligned}$$

$$\begin{aligned} \log R' &= 0.4814179 \\ \log R''' &= 0.4814179 \end{aligned}$$

$$\begin{aligned} \log R' &= 0.4814179 \\ \log R''' &= 0.4814179 \end{aligned}$$

$$\begin{aligned} \sin(\lambda''' - \lambda'') &= 0.4256556 \\ \log R'' : E''' &= 0.47467015 \end{aligned}$$

$$\begin{aligned} \log A &= 0.3486654 \\ \log B &= 0.2785767 \\ \log C &= 0.4023251 \\ \log D &= 0.5242823 \end{aligned}$$

$$C = -2.525428$$

$$\begin{aligned} \lambda' - \lambda'' &= 1.26084 \\ \lambda' - \lambda''' &= 1.26084 \end{aligned}$$

$$\begin{aligned} \sin(\lambda' - \lambda'') &= 0.0426084 \\ \cos \beta' &= 0.9999999 \\ \sin(\lambda''' - \lambda'') &= 0.5174277 \\ \cos \beta''' &= 0.9999999 \end{aligned}$$

$$\begin{aligned} \log E' &= 0.0416900 \\ \log E''' &= 0.5174277 \end{aligned}$$

$$\begin{aligned} \lambda' - \lambda'' &= 1.54 \quad 1.3 \quad 2.7 \\ \lambda' - \lambda''' &= 2.19 \quad 1.4 \quad 10.3 \\ \lambda' - \lambda''' &= 3.0 \quad 3.4 \quad 5.1 \end{aligned}$$

$$\begin{aligned} \sin(\lambda' - \lambda'') &= 0.0426084 \\ \log R' : E''' &= 0.47467015 \end{aligned}$$

$$\begin{aligned} \sin(\lambda''' - \lambda'') &= 0.4256556 \\ \log R'' : E''' &= 0.47467015 \end{aligned}$$

$$\begin{aligned} \sin(\lambda''' - \lambda'') &= 0.4256556 \\ \log R'' : E''' &= 0.47467015 \end{aligned}$$

$$\begin{aligned} \log A &= 0.3486654 \\ \log B &= 0.2785767 \\ \log C &= 0.4023251 \\ \log D &= 0.5242823 \end{aligned}$$

$$C = -5.400755$$

Appendix 1

$k' - k''$	1 5 2 0 0 0 0
$\cos(\gamma' - \gamma'')$	0 0 0 0 0 0 0
$\cos \beta'$	0 0 0 0 0 0 0
$\sin(\gamma' - \gamma'')$	0 0 0 0 0 0 0
$\cos k'$	0 0 0 0 0 0 0
$\sin k'$	0 0 0 0 0 0 0
$\cos k' \sin \beta'$	0 0 0 0 0 0 0
$\sin k' \cos \beta'$	0 0 0 0 0 0 0
$\sin \beta'$	0 0 0 0 0 0 0
$\cos k'$	0 0 0 0 0 0 0
$\sin k'$	0 0 0 0 0 0 0
$\cos k' \sin \beta'$	0 0 0 0 0 0 0
$\sin k' \cos \beta'$	0 0 0 0 0 0 0
$\sin \beta'$	0 0 0 0 0 0 0

$k''' - k''''$	7 6 3 8 2 9 4
$\cos(\gamma''' - \gamma''')$	0 3 6 3 6 9 3 3
$\cos \delta'''$	0 0 0 0 0 0 0
$\sin(\gamma''' - \gamma''')$	0 0 0 0 0 0 0
$\cos k'''$	0 3 6 3 6 9 3 3
$\sin k'''$	0 0 0 0 0 0 0
$\sin k''' \sin \beta'''$	0 0 0 0 0 0 0
$\sin k''' \cos \beta'''$	0 0 0 0 0 0 0
$\sin \beta'''$	0 0 0 0 0 0 0
$\cos k'''$	0 3 6 3 6 9 3 3
$\sin k'''$	0 0 0 0 0 0 0
$\cos k''' \sin \beta'''$	0 0 0 0 0 0 0
$\sin k''' \cos \beta'''$	0 0 0 0 0 0 0
$\sin \beta'''$	0 0 0 0 0 0 0

11

Section III

The calculation according to the

formulas in section III is as follows: —

First Hypothesis

$\lambda_{01} I'$	0.2057906	$\lambda_{01} I''$	0.7011064
$\lambda_{02} I'$	0.5592088	$\lambda_{02} I''$	0.2814956
$\lambda_{03} I'$	1.6075346	$\lambda_{03} I''$	0.6025246
$\lambda_{04} Y'$	0.2114488	$\lambda_{04} Y''$	2.2021809 ₁₁
$\lambda_{05} Y'$	0.5668288	$\lambda_{05} Y''$	0.2001116
$\lambda_{06} Y'$	0.7343275	$\lambda_{06} Y''$	0.2751251 ₁₁
$\lambda_{07} Y'$	0.0897075	$\lambda_{07} Y''$	0.7210792
$\lambda_{08} Y'$	0.4527426 ₁₁	$\lambda_{08} Y''$	0.0712217 ₁₁
$\lambda_{09} Y'$	0.8924041	$\lambda_{09} Y''$	0.6025086
$(1) Y''$	-0.28262	$(1) Y''$	-0.11782
$(2) Y'$	+7.80856	$(2) Y''$	+4.00790
b	+7.52197 ₁	b	+3.83805
$\lambda_{10} Y''$	0.6282557	$\lambda_{10} Y''$	5.552146 ₁₁
$(3) Y'$	-0.41107	$(3) Y''$	-0.07117
$\overline{III}$	+3.62387	$\overline{II}$	+0.30280
$\overline{IV}$	+5.70501	$\overline{III}$	-0.20807 ₁
$\lambda_{11} \overline{I}$	0.5602720	$\lambda_{11} \overline{II}$	0.5925522
$\lambda_{12} \overline{I}$	0.7565271	$\lambda_{12} \overline{III}$	0.2945800 ₁₁

Section III. (continued).

Second Hypothesis.

$\sum_{i=1}^n Y_i''$	94282114 _n
$\sum_{i=1}^n Y_i'$	08847457
$\sum_{i=1}^n Y_i''$	-0.264979
$\sum_{i=1}^n Y_i'$	+7.66011
$\sum_{i=1}^n Y_i$	+7.404144
$\sum_{i=1}^n Y_i''$	0.708852 _n
$\sum_{i=1}^n Y_i'$	-0.71021
$\sum_{i=1}^n Y_i$	+2625651
$\sum_{i=1}^n Y_i$	+5501210 _n
$\sum_{i=1}^n Y_i$	0.5593860
$\sum_{i=1}^n Y_i$	0.7475142

$\sum_{i=1}^n Y_i''$	0.1082061 _n
$\sum_{i=1}^n Y_i'$	0.5818195
$\sum_{i=1}^n Y_i''$	-0.183811
$\sum_{i=1}^n Y_i'$	+3.906787
$\sum_{i=1}^n Y_i$	+7.178401
$\sum_{i=1}^n Y_i''$	8.889203 _n
$\sum_{i=1}^n Y_i'$	-0.07748
$\sum_{i=1}^n Y_i$	+0.10540 _n
$\sum_{i=1}^n Y_i$	-0.21258
$\sum_{i=1}^n Y_i$	0.7045214
$\sum_{i=1}^n Y_i$	0.717202 _n

Section III (continued)

Collection of Constants.

$\log \alpha$	0.3456684 _n
$\log \beta$	0.2755787 _n
$\log \gamma$	0.4023251 _n
$\log \delta$	0.5242523 _n
$\log \epsilon$	8.5573468
$\log \zeta$	0.0075221 _n
$\log \eta$	-0.994311
$\log \theta$	8.5645873 _n
$\log \iota$	0.005510
$\log \kappa$	0.1493453
$\log \lambda$	0.7706404
$\log \mu$	0.3037673
$\log (v)$	4.7184143 _n
$\log (z)$	0.8026966
$\log (e)$	4.5940282 _n
$\frac{I}{I}$	-1.034492
$\frac{I}{I}$	+2.752304
$\log III$	0.5543560.
$\log IV$	0.7475143

$\log A_0$	0.7402070
$\log B_0$	0.7664795 _n
$\log C_0$	0.7324557 _n
$\log D_0$	0.5212046
$\log E_0$	0.6521760
$\log F_0$	4.3577605
$\log G_0$	+0.227609
$\log H_0$	0.6521745
$\log I_0$	0.6505547
$\log J_0$	0.1946225
$\log (v)$	4.1461389
$\log (z)$	0.8026966
$\log (e)$	4.5940282
$\frac{II}{VI}$	-0.81885.
$\frac{II}{VI}$	-0.344304
$\log VII$	4.5045374
$\log VIII$	4.3752208 _n

Section III, continued

Grand Hypothesis

$\log_{10} Y'$	9.42194416 ₁₁
$\log_{10} Y$	0.8846947 ₁
$\log_{10} Y'$	-0.264206
$\log_{10} Y'$	+7.665155
$\log_{10} Y'$	+7.403982
$\log_{10} Y''$	9.5975558 ₁₁
$\log_{10} Y''$	-0.297877
$\log_{10} Y''$	+3.622145
$\log_{10} Y''$	+5.551108
$\log_{10} Y''$	0.5601627 ₁
$\log_{10} Y''$	0.7472192

$\log_{10} Y''$	9.1055715 ₁₁
$\log_{10} Y''$	0.50111007 ₁
$\log_{10} Y''$	-0.125491
$\log_{10} Y''$	+2.900224
$\log_{10} Y''$	+3.77187
$\log_{10} Y''$	8.8895694 ₁₁
$\log_{10} Y''$	-0.077601
$\log_{10} Y''$	-0.218271
$\log_{10} Y''$	-0.236737 ₁
$\log_{10} Y''$	9.5027954
$\log_{10} Y''$	9.6742781 ₁₁

Appendix III (continued)

Fourth set of hypotheses.

$\log_{10} Y''$	0.4217142 _n	$\log_{10} Y''$	0.1089289 _n
$\log_{10} Y'$	0.8846266	$\log_{10} Y'$	0.8909242
$\log_{10} Y$	-0.264067	$\log_{10} Y$	-0.108511
$\log_{10} Y'$	+7.667020	$\log_{10} Y'$	+3.898746
$\log_{10} Y$	+7.402952	$\log_{10} Y$	+3.770220
$\log_{10} Y$	0.8873885 _n	$\log_{10} Y$	8.8894365 _n
$\log_{10} Y$	-0.225106	$\log_{10} Y$	-0.077612
$\log_{10} Y$	+2.630123	$\log_{10} Y$	+0.318053
$\log_{10} Y$	+8.556092	$\log_{10} Y$	-0.236640
$\log_{10} Y$	0.7102222	$\log_{10} Y$	0.5024495
$\log_{10} Y$	0.7471358	$\log_{10} Y$	0.3740852 _n

Table II (continued)

	λ^1	λ^2	λ^3	λ^4
$\xi'(\Pi - \Pi')x$	-0.36603	-0.330526	-0.220506	-0.216363
ξ''	+2.273744	+2.173778	+2.145437	+2.134389
ξ'	+2.074551	+1.984351	+1.963994	+1.953441
$\xi' + \xi''$	+2.045835	+1.945869	+1.918025	+1.906480
$\log(\xi' - \xi'')$	0.31797	0.2987114	0.2931402	0.2908003
$\log B'$	8.88725	8.8873468	8.8873468	8.8873468
$\log \tan \theta'$	1.43062	1.4112646	1.4057934	1.4034535
$\log \sin \theta'$	0.40970	0.4096736	0.4096651	0.4096616
$\log(\xi''' - \xi''')$	0.31056	0.2891136	0.2828549	0.2802422
$\log B'''$	0.08218	0.0821760	0.0821760	0.0821760
$\log \tan \theta'''$	0.32863	0.3069376	0.3006789	0.2950562
$\log \sin \theta'''$	0.05680	0.0527137	0.0514747	0.0509470
$\log \lambda^1$	0.31827	0.2992378	0.2934751	0.2911387
$\log \lambda^2$	0.35406	0.3363999	0.3313502	0.3292552
λ^1	+2.0810	+1.990547	+1.965510	+1.954964
λ^2	+2.2597	+2.169701	+2.144767	+2.134446
$\lambda^1 + \lambda^2$	+4.3407	+4.160248	+4.110278	+4.089410
$\log(\lambda^1 + \lambda^2)$	0.63756	0.6191505	0.6138712	0.6116607
$\log(\lambda^1 + \lambda^2)'$	1.01268	1.8574515	1.8416133	1.8349821
$\log \lambda^3$	0.60206	0.6020600	0.6020600	0.6020600
$\log \lambda^4$	8.68935	8.7446185	8.7605467	8.7670714

Section II. (continued)

	5^H	6^H	7^H
$\log x$	8.767500	8.7677700	8.7677900
$\log \text{III} x$	4.3279400	4.3281300	4.3281500
$\log \text{IV} x$	8.3163400	8.3165300	8.3165500
$\log \text{V} x$	4.5238400 _n	4.5240300 _n	4.5240500 _n
$\log \text{VI} x$	8.162600	8.1627500	8.1627700
$\text{III} x$	+0.212754	+0.212778	+0.212777
$\text{IV} x$	+0.020718	+0.020727	+0.020728
$\text{V} x$	-0.33407-	-0.334218	-0.334234
$\text{VI} x$	+0.014526	+0.014533	+0.014534
$\text{I} + \text{III} x$	-0.821707	-0.821613	-0.821604
$\text{II} + \text{IV} x$	-0.857634	-0.857625	-0.857624
$\log (\text{I} + \text{III}) x$	4.9147170 _n	4.9146673 _n	4.9146625 _n
$\log (\text{II} + \text{IV}) x$	4.4333020 _n	4.4332975 _n	4.4332969 _n
$\log \xi'$	4.9514150	4.9513695	4.9513656
ξ'	+0.458105	+0.458100	+0.458100
$(\text{I} + \text{III}) x$	-0.8217778	-0.8217771	-0.8217770
$\log (\text{I} - \text{III}) x$	4.718227 _n	4.718217 _n	4.718217 _n
$\log \xi' (\text{I} - \text{III}) x$	4.449636 _n	4.4495822 _n	4.4495761 _n

Section II continued)

	δ'	δ''	δ'''
$\delta'(\bar{u} - \bar{u})\bar{x}$	-0.315963	-0.315920	-0.315910
δ'	+2.133209	+2.133102	+2.133100
$\delta' - \bar{\delta}'$	+1.952420	+1.952421	+1.952311
$\delta'' - \bar{\delta}''$	+1.905360	+1.905252	+1.905201
$\log(\delta' - \bar{\delta}')$	0.2905732	0.2905512	0.2905490
$\log \bar{\delta}'$	8.8873468	8.8873468	8.8873468
$\log \tan \theta'$	1.4032264	1.4032045	1.4032022
$\log \sin \theta'$	4.9996612	4.9996611	4.9996611
$\log(\delta'' - \bar{\delta}'')$	0.2799771	0.2799527	0.2799499
$\log \bar{\delta}''$	4.9821760	4.9821760	4.9821760
$\log \tan \theta''$	0.2978011	0.2977767	0.2977739
$\log \sin \theta''$	4.9508954	4.9508905	4.9508899
$\log \delta'$	0.2909120	0.2908902	0.2908879
$\log \delta''$	0.3290817	0.3290623	0.3290600
δ'	+1.953942	+1.953845	+1.953835
δ''	+2.133446	+2.133350	+2.133340
$\delta' + \delta''$	+4.087390	+4.087195	+4.087175
$\log(\delta' + \delta'')$	0.6114462	0.6114254	0.6114233
$\log(\delta' + \delta'')^2$	1.8343286	1.8342762	1.8342644
$\log 4$	0.6020600	0.6020600	0.6020600
$x = \log \frac{1}{(\delta' + \delta'')^2}$	8.7677214	8.7677838	8.7677901

Section IV. (continued).

Second Hypothesis.

	1st	2nd	3rd
$\log x$	8.7677701	8.7657720	8.7658070
$\log III x$	9.3271701	9.3251770	9.3251700
$\log IV x$	8.2723275	8.2703304	8.2703414
$\log VII x$	9.5153044 _n	9.5133073 _n	9.513383 _n
$\log VIII x$	5.43000	5.170138	5.170128
$II x$	+0.212711	+0.211436	-0.212711
$IV x$	+0.018721	+0.018035	+0.018636
$VI x$	-0.327570	-0.326067	-0.326076
$VIII x$	+0.013900	+0.013836	+0.013836
$I + III x$	-0.822081	-0.823056	-0.822081
$II + IV x$	-0.559631	-0.559717	-0.559717
$\log(I + III) x$	9.9149140 _n	9.9154274 _n	9.9154274 _n
$\log(I + IV) x$	9.9343121 _n	9.9343555 _n	9.9343555 _n
$\log p'$	9.9806025	9.9810739	9.9810739
ϵ	+0.050318	+0.057337	+0.057337
$(VI - VIII) x$	-0.330404	-0.330108	-0.330108
$\log(VI - VIII) x$	9.5190453 _n	9.5191275 _n	9.5191275 _n
$\log(p' - VIII) x$	9.4996478 _n	9.5002034 _n	9.5002034 _n

Section II (continued).Second Hypothesis.

	181	184	182
$\log(\epsilon - f_1)$	-0.31507	-0.310370	-0.310370
ϵ''	+2.34703	+2.140861	+2.140861
$\epsilon - f_1$	+0.50020	+1.951668	+1.951668
$\epsilon - f_2$	+0.11550	+1.912952	+1.912952
$\log(\epsilon - f_1)$	0.200547	0.2004060	0.2004060
$\log B'$	8.8873468	8.8873468	8.8873468
$\log \tan \theta'$	1.4030592	1.4030592	1.4030580
$\log \sin \theta'$	9.9996609	9.9996609	9.9996609
$\log(\epsilon' - f_1)$	0.2817578	0.2817011	0.2817025
$\log B''$	9.9821760	9.9821760	9.9821760
$\log \tan \theta''$	0.2995228	0.2995251	0.2995265
$\log \sin \theta''$	9.9511730	9.9512438	9.9512425
$\log r'$	0.2905141	0.2907051	0.2907051
$\log r''$	0.3305011	0.3304603	0.3304500
r'	+1.952150	+1.953193	+1.953187
r''	+2.132278	+2.140219	+2.140233
$r' + r''$	+4.084428	+4.093412	+4.093420
$\log(r' + r'')$	0.6111841	0.6120505	0.6120553
$\log(r' + r'')^3$	1.8353163	1.8362525	1.8362557
$\log 4$	0.6020600	0.6020600	0.6020600
$\log x$	3.7604437	3.7605005	3.7605005

Section I (continued)

Third Hypothesis.

	<u>I</u>	<u>II</u>	<u>III</u>
$\log I$	8.905041	8.9050050	8.9050200
$\log II$	9.323065	9.3230087	9.3230228
$\log III$	9.2060005	9.2059039	9.2059175
$\log IV$	9.5130525	9.5131542	9.5130708
$\log V$	8.1400502	8.1401717 _n	8.1400082 _n
$II - I$	+0.218020	+0.211870	+0.211910
$III - I$	+0.018561	+0.018565	+0.018569
$IV - I$	+0.325877	+0.325952	+0.325887
$V - I$	-0.013800	-0.013809	-0.013804
$I + III$	-0.822072	-0.822022	-0.822052
$II + IV$	-0.857691	-0.859787	-0.858797
$\log (I + III)$	9.0152006 _n	9.0152003 _n	9.0152011 _n
$\log (II + IV)$	9.9343929 _n	9.9343909 _n	9.9343909 _n
$\log e'$	9.9508338	9.9508094	9.9507523
E	+0.950828	+0.956774	+0.956714
$II - III$	-0.330498	-0.330495	-0.330500
$\log (V - IV)$	9.5191689 _n	9.5191649 _n	9.5191715
$\log (I - V)$	9.500027 _n	9.4999743 _n	9.5000258

Section IV (continued)

Third Hypothesis:

	1st	2nd	3rd
$\epsilon(1-\epsilon)k$	-0310220	-0310220	-0310220
ϵ	+2111197	+2111197	+2111197
$\epsilon - f_1$	+1051131	+1051131	+1051131
$\epsilon - f_2$	+1113255	+1113255	+1113255
$\log(\epsilon - f_1)$	0.0002882	0.0002882	0.0002882
$\log B$	88813408	88813408	88813408
$\log \tan \theta$	14027217	14027217	14027217
$\log \sin \theta'$	9.9996607	9.9996607	9.9996607
$\log(p'' - f_m)$	0.2817604	0.2817661	0.2817863
$\log B''$	9.9521760	9.9521760	9.9521760
$\log \tan \theta''$	0.2996044	0.2995921	0.2996103
$\log \sin \theta''$	9.9512591	9.9512566	9.9512603
$\log r'$	0.2906275	0.2906155	0.2906022
$\log r''$	0.3205913		
r	+1.955004	+1.52610	+1.052800
r'	+2.141530	+2.140482	+2.140553
$r' + r''$	+4.093107	+4.003082	+4.093103
$\log(r' + r'')$	0.6120624	0.6120515	0.6120551
$\log(r' + r'')^3$	1.8361572	1.8361545	1.8361581
$\log 4$	0.6020600	0.6020600	0.6020600
$\log 2$	0.3010300	0.3010300	0.3010300
$\log 3$	0.4771213	0.4771213	0.4771213
$\log 5$	0.6989700	0.6989700	0.6989700
$\log 7$	0.8450980	0.8450980	0.8450980
$\log 11$	1.0413927	1.0413927	1.0413927
$\log 13$	1.1139434	1.1139434	1.1139434
$\log 17$	1.2304489	1.2304489	1.2304489
$\log 19$	1.2791812	1.2791812	1.2791812
$\log 23$	1.3617278	1.3617278	1.3617278
$\log 29$	1.4623980	1.4623980	1.4623980
$\log 31$	1.4913616	1.4913616	1.4913616
$\log 37$	1.5682017	1.5682017	1.5682017
$\log 41$	1.6127839	1.6127839	1.6127839
$\log 43$	1.6334686	1.6334686	1.6334686
$\log 47$	1.6720979	1.6720979	1.6720979
$\log 53$	1.7242959	1.7242959	1.7242959
$\log 59$	1.7708520	1.7708520	1.7708520
$\log 61$	1.7853298	1.7853298	1.7853298
$\log 67$	1.8260748	1.8260748	1.8260748
$\log 71$	1.8512584	1.8512584	1.8512584
$\log 73$	1.8633229	1.8633229	1.8633229
$\log 79$	1.8970195	1.8970195	1.8970195
$\log 83$	1.9190781	1.9190781	1.9190781
$\log 89$	1.9493900	1.9493900	1.9493900
$\log 97$	1.9912268	1.9912268	1.9912268
$\log 101$	2.0043214	2.0043214	2.0043214
$\log 103$	2.0128335	2.0128335	2.0128335
$\log 107$	2.0293150	2.0293150	2.0293150
$\log 109$	2.0354243	2.0354243	2.0354243
$\log 113$	2.0530778	2.0530778	2.0530778
$\log 127$	2.1038034	2.1038034	2.1038034
$\log 131$	2.1156667	2.1156667	2.1156667
$\log 137$	2.1369196	2.1369196	2.1369196
$\log 139$	2.1412218	2.1412218	2.1412218
$\log 149$	2.1732194	2.1732194	2.1732194
$\log 151$	2.1780520	2.1780520	2.1780520
$\log 157$	2.1973260	2.1973260	2.1973260
$\log 163$	2.2132935	2.2132935	2.2132935
$\log 167$	2.2238719	2.2238719	2.2238719
$\log 173$	2.2385686	2.2385686	2.2385686
$\log 179$	2.2518884	2.2518884	2.2518884
$\log 181$	2.2552725	2.2552725	2.2552725
$\log 191$	2.2800415	2.2800415	2.2800415
$\log 193$	2.2835429	2.2835429	2.2835429
$\log 197$	2.2944393	2.2944393	2.2944393
$\log 199$	2.2983774	2.2983774	2.2983774
$\log 211$	2.3243750	2.3243750	2.3243750
$\log 223$	2.3483750	2.3483750	2.3483750
$\log 227$	2.3542425	2.3542425	2.3542425
$\log 229$	2.3576716	2.3576716	2.3576716
$\log 233$	2.3675905	2.3675905	2.3675905
$\log 239$	2.3783976	2.3783976	2.3783976
$\log 241$	2.3818267	2.3818267	2.3818267
$\log 251$	2.4013036	2.4013036	2.4013036
$\log 257$	2.4093294	2.4093294	2.4093294
$\log 263$	2.4201365	2.4201365	2.4201365
$\log 271$	2.4342965	2.4342965	2.4342965
$\log 277$	2.4432713	2.4432713	2.4432713
$\log 281$	2.4477004	2.4477004	2.4477004
$\log 283$	2.4493298	2.4493298	2.4493298
$\log 293$	2.4673298	2.4673298	2.4673298
$\log 307$	2.4893298	2.4893298	2.4893298
$\log 311$	2.4937589	2.4937589	2.4937589
$\log 313$	2.4961880	2.4961880	2.4961880
$\log 317$	2.5016171	2.5016171	2.5016171
$\log 331$	2.5216171	2.5216171	2.5216171
$\log 337$	2.5296462	2.5296462	2.5296462
$\log 347$	2.5437153	2.5437153	2.5437153
$\log 353$	2.5491444	2.5491444	2.5491444
$\log 359$	2.5545735	2.5545735	2.5545735
$\log 367$	2.5635426	2.5635426	2.5635426
$\log 373$	2.5715717	2.5715717	2.5715717
$\log 379$	2.5770008	2.5770008	2.5770008
$\log 383$	2.5814299	2.5814299	2.5814299
$\log 397$	2.6014299	2.6014299	2.6014299
$\log 401$	2.6058590	2.6058590	2.6058590
$\log 409$	2.6112881	2.6112881	2.6112881
$\log 419$	2.6232881	2.6232881	2.6232881
$\log 431$	2.6373267	2.6373267	2.6373267
$\log 433$	2.6397558	2.6397558	2.6397558
$\log 439$	2.6441849	2.6441849	2.6441849
$\log 443$	2.6466140	2.6466140	2.6466140
$\log 449$	2.6510431	2.6510431	2.6510431
$\log 457$	2.6579122	2.6579122	2.6579122
$\log 461$	2.6603413	2.6603413	2.6603413
$\log 463$	2.6619704	2.6619704	2.6619704
$\log 467$	2.6644000	2.6644000	2.6644000
$\log 479$	2.6784386	2.6784386	2.6784386
$\log 487$	2.6874077	2.6874077	2.6874077
$\log 491$	2.6918368	2.6918368	2.6918368
$\log 499$	2.6987059	2.6987059	2.6987059
$\log 503$	2.7011350	2.7011350	2.7011350
$\log 509$	2.7055641	2.7055641	2.7055641
$\log 517$	2.7119932	2.7119932	2.7119932
$\log 521$	2.7144223	2.7144223	2.7144223
$\log 523$	2.7160514	2.7160514	2.7160514
$\log 527$	2.7184805	2.7184805	2.7184805
$\log 539$	2.7325191	2.7325191	2.7325191
$\log 547$	2.7414882	2.7414882	2.7414882
$\log 557$	2.7479173	2.7479173	2.7479173
$\log 563$	2.7503464	2.7503464	2.7503464
$\log 569$	2.7527755	2.7527755	2.7527755
$\log 571$	2.7544046	2.7544046	2.7544046
$\log 577$	2.7588337	2.7588337	2.7588337
$\log 587$	2.7652628	2.7652628	2.7652628
$\log 593$	2.7676919	2.7676919	2.7676919
$\log 599$	2.7721210	2.7721210	2.7721210
$\log 601$	2.7737501	2.7737501	2.7737501
$\log 607$	2.7781792	2.7781792	2.7781792
$\log 613$	2.7806083	2.7806083	2.7806083
$\log 617$	2.7830374	2.7830374	2.7830374
$\log 619$	2.7846665	2.7846665	2.7846665
$\log 623$	2.7870956	2.7870956	2.7870956
$\log 629$	2.7915247	2.7915247	2.7915247
$\log 631$	2.7931538	2.7931538	2.7931538
$\log 637$	2.7975829	2.7975829	2.7975829
$\log 641$	2.8000120	2.8000120	2.8000120
$\log 643$	2.8016411	2.8016411	2.8016411
$\log 647$	2.8040702	2.8040702	2.8040702
$\log 653$	2.8085000	2.8085000	2.8085000
$\log 659$	2.8129291	2.8129291	2.8129291
$\log 661$	2.8145582	2.8145582	2.8145582
$\log 667$	2.8189873	2.8189873	2.8189873
$\log 671$	2.8214164	2.8214164	2.8214164
$\log 673$	2.8230455	2.8230455	2.8230455
$\log 677$	2.8254746	2.8254746	2.8254746
$\log 683$	2.8299037	2.8299037	2.8299037
$\log 689$	2.8343328	2.8343328	2.8343328
$\log 691$	2.8359619	2.8359619	2.8359619
$\log 697$	2.8403910	2.8403910	2.8403910
$\log 701$	2.8428201	2.8428201	2.8428201
$\log 709$	2.8482492	2.8482492	2.8482492
$\log 713$	2.8506783	2.8506783	2.8506783
$\log 719$	2.8551074	2.8551074	2.8551074
$\log 727$	2.8605365	2.8605365	2.8605365
$\log 733$	2.8649656	2.8649656	2.8649656
$\log 739$	2.8693947	2.8693947	2.8693947
$\log 743$	2.8718238	2.8718238	2.8718238
$\log 749$	2.8762529	2.8762529	2.8762529
$\log 751$	2.8778820	2.8778820	2.8778820
$\log 757$	2.8823111	2.8823111	2.8823111
$\log 761$	2.8847402	2.8847402	2.8847402
$\log 769$	2.8891693	2.8891693	2.8891693
$\log 773$	2.8915984	2.8915984	2.8915984
$\log 779$	2.8960275	2.8960275	2.8960275
$\log 787$	2.8984566	2.8984566	2.8984566
$\log 791$	2.9008857	2.9008857	2.9008857
$\log 797$	2.9053148	2.9053148	2.9053148
$\log 809$	2.9107439	2.9107439	2.9107439
$\log 811$	2.9123730	2.9123730	2.9123730
$\log 817$	2.9168021	2.9168021	2.9168021
$\log 821$	2.9192312	2.9192312	2.9192312
$\log 823$	2.9208603	2.9208603	2.9208603
$\log 827$	2.9232894	2.9232894	2.9232894
$\log 833$	2.9277185	2.9277185	2.9277185
$\log 839$	2.9321476	2.9321476	2.9321476
$\log 847$	2.9375767	2.9375767	2.9375767
$\log 853$	2.9420058	2.9420058	2.9420058
$\log 857$	2.9444349	2.9444349	2.9444349
$\log 859$	2.9460640	2.9460640	2.9460640
$\log 863$	2.9484931	2.9484931	2.9484931
$\log 869$	2.9529222	2.9529222	2.9529222
$\log 871$	2.9545513	2.9545513	2.9545513
$\log 877$	2.9589804	2.9589804	2.9589804
$\log 881$	2.9614095	2.9614095	2.9614095
$\log 883$	2.9630386	2.9630386	2.9630386
$\log 887$	2.9654677	2.9654677	2.9654677
$\log 893$	2.9698968	2.9698968	2.9698968
$\log 899$	2.9743259	2.9743259	2.9743259
$\log 901$	2.9759550	2.9759550	2.9759550
$\log 907$	2.9803841	2.9803841	2.9803841
$\log 911$	2.9828132	2.9828132	2.9828132
$\log 913$	2.9844423	2.9844423	2.9844423
$\log 917$	2.9868714	2.9868714	2.9868714
$\log 923$	2.9913005	2.9913005	2.9913005
$\log 929$	2.9957296	2.9957296	2.9957296
$\log 931$	2.9973587	2.9973587	2.9973587
$\log 937$	3.0017878	3.0017878	3.0017878

Section V.

the computation according to the

formulas in section V is as follows: -

Small irregular m.

Section I (continued)

continued

$\log \cos 3''$	9.9999911	$\log \cos 3'''$	9.9999800	$\frac{1}{2}(\lambda''' - \lambda')$	20 18 14.3
$\log \epsilon$	9.9810717	$\log \epsilon'''$	0.3305871	$\log \sin \frac{1}{2}(\epsilon''' - \epsilon')$	9.0306600
$\log \epsilon' \cos \beta'''$	9.9800628	$\log \epsilon'' \cos \beta'''$	0.3305671	$\log \cos b'$	9.99997580
$\log \pi_c'$	9.9955310	$\log \pi_c'''$	9.3577805 _n	$\log \cos b'''$	9.9999799
$\frac{1}{2}$	0.2918906	$\frac{1}{2}$	0.9238962	$\log \text{procl.}$	9.0803985
$\log [\epsilon' \cos \beta + \pi_c']$	0.2904216	$\log [\epsilon'' \cos \beta + \pi_c']$	0.2516767	$\frac{1}{2}$	0.0005096
$\log \pi_s'$	9.5648573 _n	$\log \pi_s'''$	9.9821748	$\frac{1}{2}$	
$\log \tan (\lambda - \lambda')$	8.277465 _n	$\log \tan (\lambda''' - \lambda'')$	1.004941	$\frac{1}{2}(\lambda - \lambda')$	-5 00 54
$\lambda' - \lambda''$	-1° 4' 40.1	$\lambda''' - \lambda''$	26 35 44.8	$\log \sin \frac{1}{2}(\lambda''' - \lambda')$	8.0749788
λ'	21 27 34.7	λ'''	34 20 38.3	$\log \sin \frac{1}{2}(\lambda''' - \lambda'')$	6.1499516
λ''	20 22 54.6	λ''	60 59 23.1	$\log \sin \frac{1}{2} \lambda''$	9.0827930
$\log \sin \lambda'$	8.8330449	$\log \sin \beta'''$	7.9824965	$\log \sin f'$	9.5413965
$\log \sin \lambda''$	8.8141166	$\log \sin \lambda'''$	8.3130836	f'	20 15 26.1
$\log \sin \lambda'''$	8.5233727	$\log \sin \lambda''$	7.9826246	$2f''$	40 37 12.2
$\frac{1}{2}$	1° 54 44.0	b'	3 52 1.8		
$\log \cos \lambda'$	9.99997580		9.9999799		
$\log \cos (\lambda - \lambda')$	8.2743889 _n	$\log \cos \lambda'''$	9.6517367		
$\log \pi$	0.2907439	$\log \cos \lambda''$	0.3304590		
$\log \pi_c'$	8.5648908	$\log \cos \lambda''$	9.9521756		

Table 1 continued

... ..

$\log \cos \beta'$	4.4459411	$\log \cos \beta''$	4.44494800	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \xi'$	4.4508094	$\log \xi''$	0.2206457	$\log \cos b'$	4.44494800
$\log \xi' \cos \beta'$	4.44494800	$\log \xi' \cos \beta''$	0.2206457	$\log \cos l''$	4.44494800
$\log R'_e$	4.4459411	$\log R''_e$	0.2206457	$\log (l'' - l')$	0.0505946
$\log [\xi' \cos \beta' + R'_e]$	4.44494800	$\log [\xi'' \cos \beta'' + R''_e]$	0.2206457	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log R'_s$	4.4459411	$\log R''_s$	0.2206457	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \tan (l' - l'')$	4.44494800	$\log \tan (l'' - l''')$	0.2206457	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$l' - l''$	2.1 2.1 2.1	$l'' - l'''$	2.6 3.8 3.2	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$l'' - l'''$	2.1 2.1 2.1	$l''' - l''''$	1.0 2.0 2.8	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$l''' - l''''$	2.0 2.0 2.0	$l'''' - l'''''$	1.0 2.0 2.8	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \sin \beta'$	8.8230411	$\log \sin \beta''$	7.9824467	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \sin b'$	8.8230411	$\log \sin b''$	8.8230411	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \sin l'$	8.8230411	$\log \sin l''$	7.9824467	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
l'	0 5 4 4	l''	0 5 4 4	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \cos b'$	4.44494800	$\log \cos b''$	4.44494800	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \sin (l' - l'')$	8.2745127	$\log \sin (l'' - l''')$	4.44494800	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log \xi'$	0.2206457	$\log \xi''$	0.2206457	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946
$\log R'_e$	8.8230411	$\log R''_e$	4.44494800	$\log \sin^2 \frac{1}{2} (l'' - l')$	0.0505946

Navigation (continued)

Navigation

$\log \cos \beta'$	9.94540911	$\log \cos \beta''$	9.94444500	$\log \cos \beta'''$	20 18 6.5
$\log \xi'$	9.9507888	$\log \xi''$	9.9507888	$\log \xi'''$	9.9507888
$\log (\xi' \cos \beta')$	9.94747742	$\log (\xi'' \cos \beta'')$	9.94747742	$\log (\xi''' \cos \beta''')$	9.94747742
$\log R'$	9.94882210	$\log R''$	9.94882210	$\log R'''$	9.94882210
$\log [\xi' \cos \beta' + R']$	0.2902462	$\log [\xi'' \cos \beta'' + R'']$	0.2817649	$\log [\xi''' \cos \beta''' + R''']$	0.2817649
$\log R'_c$	8.5648873	$\log R''_c$	8.5648873	$\log R'''_c$	8.5648873
$\log \tan (\beta' - \lambda')$	8.2746011	$\log \tan (\beta'' - \lambda'')$	8.2746011	$\log \tan (\beta''' - \lambda''')$	8.2746011
$\beta' - \lambda'$	-1° 4' 41.3	$\beta'' - \lambda''$	-26° 18' 15.0	$\beta''' - \lambda'''$	0° 46' 50.3
λ'	21 27 34.7	λ''	21 20 1.2	λ'''	20 56.2
β'	20 18 52.4	β''	20 18 52.4	β'''	20 18 52.4
$\log \sin \beta'$	8.8230440	$\log \sin \beta''$	8.8230440	$\log \sin \beta'''$	8.8230440
$\log \xi' \sin \beta'$	8.8138330	$\log \xi'' \sin \beta''$	8.8138330	$\log \xi''' \sin \beta'''$	8.8138330
$\log \sin \beta'$	8.8230440	$\log \sin \beta''$	8.8230440	$\log \sin \beta'''$	8.8230440
λ'	21 27 34.7	λ''	21 20 1.2	λ'''	20 56.2
$\log \sin (\beta' - \lambda')$	8.2746011	$\log \sin (\beta'' - \lambda'')$	8.2746011	$\log \sin (\beta''' - \lambda''')$	8.2746011
$\log \xi'$	9.9507888	$\log \xi''$	9.9507888	$\log \xi'''$	9.9507888
$\log R'$	9.94882210	$\log R''$	9.94882210	$\log R'''$	9.94882210

Section II

computation according to formulas

Section II -

$\log Y''$	8.5021176	$\log Y_0'$	8.5021176
$\log x$	8.5021176	$\log x$	8.5021176
$\log Y'$	0.0897075	$\log Y_0'$	0.0897075
$\log x Y''$	8.5021176	$\log x Y_0'$	8.5021176
$\log x Y'$	1.4835581	$\log x Y_0'$	1.4835581
$\log x Y''$	8.5021176	$\log x Y_0'$	8.5021176
$\log x Y'$	1.1100348	$\log x Y_0'$	1.1100348
$\log (1-xY'')$	9.9859757	$\log (1-xY_0'')$	9.9859757
$\log (1-xY')$	0.3694459	$\log (1-xY_0')$	0.3694459
$\log (1-xY'')$	9.9859757	$\log (1-xY_0'')$	9.9859757
$\log (1-xY')$	0.5241174	$\log (1-xY_0')$	0.5241174
$\log x + x''$	0.3557216	$\log x + x_0''$	0.3557216
$\log x + x'$	0.4016502	$\log x + x_0'$	0.4016502
$\log x''$	9.8640713	$\log x_0''$	9.8640713
$\log x'$	0.2008854	$\log x_0'$	0.2008854
$\log \sin 25''$	9.8144203	$\log \sin 25''$	9.8144203

For continuation see following page

... problem, consequently designate by λ ,
 ... latitude and geocentric distance ... the ecliptical
 ... by R the geocentric distance of the ... and let L be the
 solar longitude, and consider the sun's latitude to be zero. Then will
 we have the following relations:

$$\xi = r \cos(\lambda - \Pi) \cos \beta$$

$$\eta = r \sin(\lambda - \Pi) \cos \beta \quad (h)$$

$$\zeta = r \sin \beta$$

$$X = R \cos(L - \Pi)$$

$$Y = R \sin(L - \Pi) \quad (i)$$

$$Z = 0$$

In these formulas it is necessary to count the longitudes from
 ... whose longitude is Π . Designate by accents the different
 positions of the celestial body, which we are considering. By introducing
 into equations (g) the relations (h) and (i) we can write the following
 relations:

(vide next page.)

$$\begin{aligned}
 & n[\xi' \cos \lambda' \cos \beta' - R' \cos \lambda' \cos \beta'] \\
 & + n[\xi'' \cos \lambda'' \cos \beta'' - R'' \cos \lambda'' \cos \beta''] \\
 & = \xi' \sin (\lambda' - \pi) \cos \beta' - R' \sin (\lambda' - \pi) \\
 & n[\xi' \sin (\lambda' - \pi) \cos \beta' - R' \sin (\lambda' - \pi)] \\
 & + n[\xi'' \sin (\lambda'' - \pi) \cos \beta'' - R'' \sin (\lambda'' - \pi)] \\
 & = \xi' \sin (\lambda' - \pi) \cos \beta' - R' \sin (\lambda' - \pi) \\
 & + \xi'' \sin (\lambda'' - \pi) \cos \beta'' - R'' \sin (\lambda'' - \pi) \\
 & = \xi' \sin \beta' + n \xi'' \sin \beta'' \\
 & = \xi' \sin \beta'
 \end{aligned} \tag{k}$$

By in the equations (i) we do not put $Z = 0$, the co-ordinates of the sun will take the form

$$\begin{aligned}
 X &= R \cos B \cos (L - \pi) \\
 Y &= R \cos B \sin (L - \pi) \\
 Z &= R \sin B.
 \end{aligned} \tag{i}$$

where B represents the sun's latitude.

By putting $\pi = 0$ we will have in place of

equations (k)

$$\begin{aligned}
 & n[\xi' \cos \lambda' \cos \beta' - R' \cos \lambda' \cos \beta'] \\
 & + n[\xi'' \cos \lambda'' \cos \beta'' - R'' \cos \lambda'' \cos \beta''] \\
 & = \xi' \cos \lambda' \cos \beta' - R' \cos \lambda' \cos \beta' \\
 & n[\xi' \sin \lambda' \cos \beta' - R' \sin \lambda' \cos \beta'] \\
 & + n[\xi'' \sin \lambda'' \cos \beta'' - R'' \sin \lambda'' \cos \beta''] \\
 & = \xi' \sin \lambda' \cos \beta' - R' \sin \lambda' \cos \beta' \\
 & + \xi'' \sin \lambda'' \cos \beta'' - R'' \sin \lambda'' \cos \beta'' \\
 & = \xi' \sin \lambda' \cos \beta' - R' \sin \lambda' \cos \beta'
 \end{aligned} \tag{m}$$

In the first determination of an orbit, the last equations have an advantage over equations (k), which becomes appreciable in special cases. If, for example, one or more of the observations used in making the calculations, should have the observed latitude very small or even absolutely zero. The introduction of a "fictitious place" becomes impossible, and rigorously the latitude of the sun cannot be fully equal to zero. In such a case we can make use of equations (m) by introducing in the place of $L, B,$ and $R,$ the longitude, latitude and geocentric distance, L_0, B_0 and $R_0,$ of the sun measured or parallel according to the planet's position.

It is to be noted that four observations give eight elements, and since it is necessary to find only six elements we can consider two of the observations as incomplete. For an exact determination in the present case, we will take as incomplete the mean observations, i.e., the second and third, and replace them by two great circles which we will consider to have the property of passing through the two mean observations.

We will designate the dates of the four observations by $T', T'', T''',$ and T'''' , also the corresponding longitudes

by λ' , λ'' , λ'_0 and λ''_0 and the latitudes by β' , β'' , β'_0 and β''_0 (p. 1, l. 1),
 I and by I_0 the inclinations of the two great circles to the ecliptic,
 by Π and Π_0 the longitudes of their ascending nodes. We will have
 for the conditions which these four last quantities should satisfy

$$\begin{aligned} \tan I \sin (\lambda - \Pi) &= \tan \beta'' \\ \tan I_0 \sin (\lambda'_0 - \Pi_0) &= \tan \beta'_0 \end{aligned} \quad (n)$$

Also designate by the same accents as used in the case of the planet, the
 solar longitudes, latitudes and distances relative to the four observations,
 and count the longitude in the first place from Π , and in the second
 from Π_0 . For the solar longitudes λ , λ' , λ_0 , λ'' , for latitudes β , β' , β_0 , β'' , and
 distances R , R' , R_0 and R'' ; it is permissible in the most precise calculations
 to replace $\cos \beta$, the solar latitude affected by parallax, by unity, and
 the sine by the arc itself. By making these changes in equations (m)
 and then writing three additional equations by substituting in these
 same equations λ'_0 for λ' and Π_0 for Π , we will have six equations
 of the following form

(vide next page)

$$n[\xi' \cos(\lambda' - \pi) \cos \beta' - R' \cos(\mu' - \pi)]$$

$$+ n''[\xi'' \cos(\lambda'' - \pi) \cos \beta'' - R'' \cos(\mu'' - \pi)]$$

$$= \xi' \cos(\lambda' - \pi) \cos \beta' - R' \cos(\mu' - \pi)$$

$$n'[\xi' \sin(\lambda' - \pi) \cos \beta' - R' \sin(\mu' - \pi)]$$

$$+ n''[\xi'' \sin(\lambda'' - \pi) \cos \beta'' - R'' \sin(\mu'' - \pi)]$$

$$= \xi' \sin(\lambda' - \pi) \cos \beta' - R' \sin(\mu' - \pi)$$

$$n[\xi' \sin \beta' - R' B' \sin \mu']$$

$$+ n''[\xi'' \sin \beta'' - R'' B'' \sin \mu'']$$

$$= \xi' \sin \beta' - R' B' \sin \mu'$$

(c)

$$n_0[\xi' \cos(\lambda' - \pi_0) \cos \beta' - R' \cos(\mu' - \pi_0)]$$

$$+ n''_0[\xi'' \cos(\lambda'' - \pi_0) \cos \beta'' - R'' \cos(\mu'' - \pi_0)]$$

$$= \xi' \cos(\lambda' - \pi_0) \cos \beta' - R' \cos(\mu' - \pi_0)$$

$$n_c[\xi' \sin(\lambda' - \pi_0) \cos \beta' - R' \sin(\mu' - \pi_0)]$$

$$+ n''_c[\xi'' \sin(\lambda'' - \pi_0) \cos \beta'' - R'' \sin(\mu'' - \pi_0)]$$

$$= \xi' \sin(\lambda' - \pi_0) \cos \beta' - R' \sin(\mu' - \pi_0)$$

$$n_0[\xi' \sin \beta' - R' B' \sin \mu']$$

$$+ n''_0[\xi'' \sin \beta'' - R'' B'' \sin \mu'']$$

$$= \xi' \sin \beta' - R' B' \sin \mu'$$

(c')

But now

$$\cos(\lambda'' - \Pi) \cos \beta'' = \cos u$$

$$\sin(\lambda'' - \Pi) \cos \beta'' = \sin u \cos I$$

$$\sin \beta'' = \sin u \sin I$$

(7)

$$\cos(\lambda_0'' - \Pi_0) \cos \beta_0'' = \cos u_0$$

$$\sin(\lambda_0'' - \Pi_0) \cos \beta_0'' = \sin u_0 \cos I_0$$

$$\sin \beta_0'' = \sin u_0 \sin I_0$$

u and u_0 will be in these formulae angles purely arbitrary, I and I_0 ought to be deduced only from Π and Π_0 by the formulae (n). Imagine that we have placed in (p) and (q) the quantities constituting the first members of equations (1) by the values following from these relations; the resulting equations will include the arbitrary angles u and u_0 . To eliminate immediately the first of these angles we will add in equations (p) the product of the second by $\sin I$ to the product of the third by $-\cos I$. We can in the same way eliminate the u_0 from the last two equations of (q). We thus obtain between ξ' and ξ'' two relations of the form

$$-\xi' n E + \xi'' n'' E''' = n A' - B' + n'' C'$$

$$-\xi''' n_0 E'_c + \xi''' n'' E'_c = n_0 A'_c - B'_c + n''_c C'_c$$

(6')

where we have written for brevity

$$A' = R' [\sin (\lambda' - \pi) \sin I - B' \cos I \operatorname{arc} l']$$

$$B' = R'' [\sin (\lambda'' - \pi) \sin I - B'' \cos I \operatorname{arc} l']$$

$$C' = R''' [\sin (\lambda''' - \pi) \sin I - B''' \cos I \operatorname{arc} l']$$

$$A'_c = R'_c [\sin (\lambda'_c - \pi_c) \sin I_c - B'_c \cos I_c \operatorname{arc} l'_c]$$

$$B'_c = R''_c [\sin (\lambda''_c - \pi_c) \sin I_c - B''_c \cos I_c \operatorname{arc} l'_c]$$

$$C'_c = R'''_c [\sin (\lambda'''_c - \pi_c) \sin I_c - B'''_c \cos I_c \operatorname{arc} l'_c]$$

$$E' = \sin \beta' \cos I - \sin (\lambda' - \pi) \cos \beta' \sin I$$

$$E''' = \sin \beta''' \sin I \sin (\lambda''' - \pi) - \sin \beta''' \sin I$$

$$E'_c = \sin \beta'_c \cos I_c - \sin (\lambda'_c - \pi_c) \cos \beta'_c \sin I_c$$

$$E'''_c = \cos \beta'''_c \cos I_c \sin (\lambda'''_c - \pi_c) - \sin \beta'''_c \cos I_c$$

Solving equations (6) with respect to ξ' and then with respect to ξ'' , we will find the following equations for

Let us assume that the distance

$$\begin{aligned} \rho' &= \frac{\frac{[r' r'']}{[r' r'']} \cdot \frac{E'}{E} - \frac{[r' r'']}{[r' r'']} \cdot \frac{E'_0}{E'_0} + \frac{C'}{E'} - \frac{[r' r'']}{[r' r'']} \cdot \frac{A'}{E''} + \frac{[r' r'']}{[r' r'']} \cdot \frac{B'}{E''} - \frac{C'}{E''}}{\frac{[r' r'']}{[r' r'']} \cdot \frac{E'}{E''} - \frac{[r' r'']}{[r' r'']} \cdot \frac{E'_0}{E''}} \\ &= \frac{\frac{A'}{E} - \frac{[r' r'']}{[r' r'']} \cdot \frac{B'}{E'} + \frac{[r' r'']}{[r' r'']} \cdot \frac{C'}{E'} - \frac{A'_0}{E'_0} + \frac{[r' r'']}{[r' r'']} \cdot \frac{B'_0}{E'_0} - \frac{[r' r'']}{[r' r'']} \cdot \frac{C'_0}{E'_0}}{\frac{[r' r'']}{[r' r'']} \cdot \frac{E'}{E''} - \frac{[r' r'']}{[r' r'']} \cdot \frac{E'_0}{E''}} \end{aligned} \quad (1)$$

It is not difficult to see that the expression

which is calculated in order to find a supposed component by we imagine E', E'' and E'_0, E''_0 developed according to the powers of the intervals of time we can establish for these symbols a series of the form

$$E' = a(t''' - b t''^2 + \dots)$$

$$E'' = a(t' + b t'^2 + \dots)$$

$$E'_0 = a_0(t_0''' - b_0 t_0''^2 + \dots)$$

$$E''_0 = a_0(t_0' + b_0 t_0'^2 + \dots)$$

where

$$t' = k(T'' - T')$$

$$t'_0 = k(T''' - T'_0)$$

$$t'' = k(T''' - T')$$

$$t''_0 = k(T''_0 - T')$$

$$t''' = k(T''' - T')$$

$$k \approx k = 5.2355814$$

It is to be noted that the two sines

E'_c and E''_c are the sines of the perpendiculars cut off by the same points upon the great circle passing through the second observation, while E'_o and E''_o are the sines of the perpendiculars cut off by the same points upon the great circle passing through the third observation. We then have

$$\frac{E'_c}{E''_c} = \frac{t''}{t'} \cdot \frac{1 - b_1 t'' + \dots}{1 + b_1 t' + \dots}$$

$$\frac{E'_o}{E''_o} = \frac{t''_o}{t'_o} \cdot \frac{1 - b_o t''_o + \dots}{1 + b_o t'_o + \dots}$$

By replacing in the expressions the ratios

of the triangular areas by the sines, we have

$$\frac{[r' r'']}{[r'' r''']} = \frac{t''}{t'} \left[1 - \frac{1}{3} \cdot \frac{t''^2 - t'^2}{(r' + r'')^2} - \frac{1}{4} \frac{t'' t'}{t''} \cdot \frac{(r' - r'')}{(r' + r'')^2} + \dots \right]$$

$$\frac{[r' r''']}{[r'' r''']} = \frac{t''}{t'} \left[1 - \frac{1}{3} \cdot \frac{t''^2 - t'^2}{(r' + r'')^2} - \frac{1}{4} \frac{t'' t'}{t''} \cdot \frac{(r'' - r')}{(r' + r'')^2} + \dots \right] \quad (x)$$

$$\frac{[r' r'']}{[r' r''']} = \frac{t''}{t'} \left[1 - \frac{1}{3} \cdot \frac{t''^2 - t'^2}{(r' + r'')^2} + \frac{1}{4} \frac{t' t''}{t''} \cdot \frac{(r'' - r')}{(r' + r'')^2} + \dots \right]$$

$$\frac{[r'' r''']}{[r' r''']} = \frac{t'}{t''} \left[1 - \frac{1}{3} \cdot \frac{t''^2 - t'^2}{(r' + r'')^2} + \frac{1}{4} \frac{t' t''}{t''} \cdot \frac{(r'' - r')}{(r' + r'')^2} + \dots \right]$$

Replacing the terms multiplied by the squares of the products of t' by the denominator of the first relation of equation (1) becomes

$$t_0 = t_1$$

In general t_0 and t will be of the order zero, but their differences will evidently be of the order of the intervals of time. Then by supposing for an instant that the two mean observations are effected at dates infinitely close we should have for a limit

$$t = t_0.$$

As a first approximation, however, it will be necessary to take account of the terms of the third order in the equations of the triangular areas.

From the preceding considerations it has now been indicated how we can determine the geocentric distances. For the next step solve each of equations (s) with respect ξ' and we find

$$\xi'' = \frac{[r''r''']}{[r'r'']} \frac{A'}{E''} - \frac{[r'r''']}{[r'r'']} \cdot \frac{B'}{E''} + \frac{C'}{E''} + \frac{[r''r''']}{[r'r'']} \cdot \frac{E'}{E''} \cdot \xi'.$$

(ii)

$$\xi' = \frac{[r'r''']}{[r'r'']} \frac{A'}{E''} - \frac{[r'r''']}{[r'r'']} \cdot \frac{B'}{E''} + \frac{C'}{E''} + \frac{[r''r''']}{[r'r'']} \cdot \frac{E'}{E''} \cdot \xi''$$

For values of ξ' and ξ'' we have

the denominators of the gradients, which multiply the expressions for the triangular areas, do not include the symbol E which are of the first order. In general the relations of ξ''' to ξ' can be established more exactly by two orders than the geocentric distances. A form can be given to these equations permitting us to utilize this relation in our calculations of the geocentric distances.

We will put now for approximation,

$$Y = \frac{1}{3}(t - t_0)$$

$$Y' = \frac{1}{3}(t' - t_0')$$

$$Y_c' = \frac{1}{3}(t_c' - t_0')$$

$$Y_c'' = \frac{1}{3}(t_c'' - t_0'')$$

$$\lambda = \frac{4}{(2 - 0.5)}$$

and then transform the series (2) into the expression for approximation ξ' the form

$$(\xi' - \xi_0) = \lambda \xi_0'$$

Heber 11.1.

1890

$\log x''$	4.725 7011	$\log x''_0$	4.904 6451
$\log x'''$	0.120 0600	$\log x'''_0$	0.110 0600
$\log \cos 2\varphi''$	9.879 96665	$\log \cos 2\varphi'_0$	9.879 96665
$\log x'' n$	4.104 415	$\log x'''_0 n_0$	4.670 01410
$\log x'' n \cos 2\varphi''$	0.224 0060	$\log x'' n \cos 2\varphi'_0$	0.211 50000
$\log x'' n$	0.410 7419		0.905 60009
$\log x'' n$	0.740 97	$\log x'' n$	0.200 7001
$\log x'' n \cos 2\varphi''$	0.717 0765	$\log x'' n \cos 2\varphi'_0$	0.110 7001
	0.592 9644		0.576 8002
$\log x'' n$	0.154 0902	$\log x'' n$	0.670 01400
$\log x'' n \cos 2\varphi''$	0.651 8300	$\log x'' n \cos 2\varphi'_0$	0.048 1254
$\log x'' n \cos 2\varphi''$	0.290 0409	$\log x''_0 \cos 2\varphi'_0$	0.247 0000
$\log \tan 2\varphi''$	0.361 7891	$\log \tan 2\varphi'_0$	4.501 0000
	1.0 5 16.3		0.12 00.1
$\log \cos 2\varphi''$	9.958 8034	$\log \cos 2\varphi'_0$	9.926 9179
$\log x''$	0.301 2375	$\log x''_0$	0.201 1400
$\log x'' n$	4.969 3795	$\log x''_0 n_0$	4.984 5600
$\log x'' n \cos 2\varphi''$	4.245 1516	$\log x''_0 \cos 2\varphi'_0$	0.215 1200
$\log \tan 2\varphi''$	0.721 270	$\log \tan 2\varphi'_0$	4.169 1296
$\log x''$	2.0 40 27.1		8 00 00.0
$\log x'' n$	4.969 3795	$\log \cos 2\varphi'_0$	9.915 1100
$\log x''$	0.301 2375	$\log x''_0$	0.200 1100

Section II. (continued)

Logarithmic

$\log Y''$	9.7047971	$\log Y''$	9.9120672
$\log x$	8.7658041	$\log x$	8.7658041
$\log Y'$	0.0820491	$\log Y'$	9.7161955
$\log x Y'$	8.4706012	$\log x Y'$	8.6775713
$\log Y'$	1.5163699	$\log Y'$	1.3423336
$\log Y'$	8.8478222	$\log Y'$	8.6810796
$\log Y'$	1.1200767	$\log Y'$	1.5046190
$\log (1-Y)$	9.9369711	$\log (1-Y)$	0.0202009
$\log t^2 + t''$	0.3647459	$\log t^2 + t''$	9.4559319
$\log (1-xY)$	9.9652799	$\log (1-xY)$	9.9366156
$\log t^2 + t''$	0.5241179	$\log t^2 + t''$	0.1091475
$\log n + n''$	0.3567170	$\log n + n''$	9.4761368
$\log 1 + n''$	0.4923978	$\log 1 + n''$	0.0957631
$\log n$	9.8611192	$\log n$	9.3803737
$\log r$	0.2007429	$\log r$	0.2007429
$\log \sin 27''$	9.8136076	$\log \sin 27''$	9.8136076

Action 11 continued

Approximation

Arithmetical

Arithmetical

$\log X$	1.7020576	$\log Y''$	1.5170576
$\log x$	8.5659055	$\log x$	8.5659055
$\log Y$	0.0914461	$\log Y'$	0.0914461
x''	8.4644331	$\log x Y''$	8.6785386
$\log x Y'$	8.8477016	$\log x Y''$	8.8477016
$\log (1-x'')$	1.7587107	$\log (1-x Y')$	0.0202020
$\log (1-x')$	0.2647450	$\log t_0' x''$	1.7587107
$\log (1-x'')$	0.4908714	$\log (1-x Y')$	0.4908714
$\log (1-x')$	0.5241154	$\log t_0' \div t_0''$	0.1001100
$\log n \div n''$	0.3567531	$\log n_0 \div n''$	0.4761762
$\log 1 \div n''$	0.4923843	$\log 1 \div n''$	0.0927527
$\log n$	1.2642032	n_0	1.2500000
$\log x'$	0.2406155	$\log x'$	0.2406155
$\log \sin 27''$	4.5135724	$\log \sin 27''$	4.5135724

Section II (continued)

Logarithmic functions

$\log n$	.5076109	$\log n''$	9.9042162
$\log r$	0.2105115	$\log r'''$	0.2305115
$\log \cos 2f'$	9.8802409	$\log \cos 2f''$	9.8802409
$\log r' n$	0.1344740	$\log r' n_0$	9.6710060
$\log r' n \cos 2f''$	0.0352702	$\log r' n_0 \cos 2f''$	9.5710767
$\log r''' n''$	9.8381222	$\log r''' n''_0$	0.2347272
$\log r''' n'' \cos 2f''$	9.7184131	$\log r''' n''_0 \cos 2f''$	0.1120187
$\log r' n$	0.1549743	$\log r' n_0$	9.1710060
$\log r'' \sin 2f'''$	9.6516964	$\log r''_0 \sin 2f'''_0$	0.0483025
$\log r'' \cos 2f'''$	9.2704175	$\log r''_0 \cos 2f'''_0$	0.2484742
$\log r'' \tan 2f'''$	9.3612744	$\log \tan 2f'''_0$	9.7748230
$\log r''$	9.2562375	r''_0	32.14224
$\log \cos 2f'$	9.9888289	$\log \cos 2f''_0$	9.9272736
$\log r''$	0.3015556	$\log r''_0$	0.3211456
$\log r'' \sin 2f'_0$	9.9655540	$\log r'' \sin 2f'_0$	9.4845807
$\log r'' \cos 2f'_0$	0.2455155	$\log r'' \cos 2f'_0$	0.3165379
$\log r'' \tan 2f'_0$	9.7147255	$\log \tan 2f'_0$	9.1680428
r''	2.40253	r''_0	8.22344
$\log r'' \cos 2f'_0$	9.9472200	$\log \cos 2f'_0$	9.9472200
$\log r''$	0.3015555	$\log r''$	0.2211456

Computation according to the formulae in Section VIII.

$\log \sqrt{T_1}$	0 16 45 300	0 15 06 205	0 16 45300	0 16 00 570	0 16 45300
$\log \sqrt{T}$	0 15 06 205	0 14 54 440	0 16 00570	0 14 54 440	0 15 54 440
$\log \frac{T_1}{T}$	0 3 15 1505	0 3 00 45	0 3 15570	0 3 00 5010	0 3 00 45 40
$\log \cos f$	0 9 8 71322	0 9 9 72158	0 9 9 58330	0 9 8 24972	0 9 7 1 4934
$\log 2 \cos f$	0 2 8 8 1622	0 2 9 82455	0 2 9 98630	0 2 8 85272	0 2 7 3 0239
$\log 2 \cos f (\pi)$	0 6 0 3 3127	0 5 4 43133	0 6 2 44500	0 5 8 40252	0 5 5 2 4979
$\log t^2$	0 2 9 8 7406	0 5 5 42985	0 3 0 11094	0 3 5 42456	0 6 0 7 5346
$\log (2 \cos f (\pi))^3$	1 8 0 9 4381	1 7 8 29309	1 8 7 33500	1 7 6 70846	1 7 4 8 4937
$\log m$	5 4 8 5 8525	5 4 6 5 571	5 4 5 7 754	5 4 2 2 1610	5 5 5 5 204
$\sqrt{T}$	0 0 1 3 9095	0 0 0 5 1765	0 0 0 4 4730	0 0 1 4 6130	0 0 1 9 0860
$\log \sin (45^\circ + \omega)$	0 0 0 6 9548	0 0 0 2 5883	0 0 0 2 2365	0 0 0 7 3065	0 0 0 4 5430
$45^\circ + \omega$	45° 27' 31.5	45° 10' 11.6	45° 8' 51.1	45° 28' 55.0	45° 37' 46.0
2ω	0 55 3.0	0 20 24.2	0 17 42.2	0 57 50.0	1 15 32.0
$\log \tan 2\omega$	6 4 0 9 0412	5 5 5 0 4050	5 4 2 35700	6 4 5 18 906	6 6 8 3 4644
$\log \sin^2 \frac{f}{2}$	1 7 6 2 7468	1 9 5 5 4160	1 7 1 26276	1 8 4 8 644	1 8 1 7 3054
$\log \sin^2 \frac{f}{2}$	5 1 6 4 2726	7 5 0 4 0172	7 1 2 7 002	8 2 9 5 5718	8 4 9 4 5112
$\log (\sin^2 \omega + \sin^2 \frac{f}{2})$	5 1 7 1 8380	7 5 0 8 8210	7 1 3 6 1976	8 3 0 1 7550	8 5 0 1 1748
$\log \cos f$	9 9 8 7 1322	9 9 9 7 2158	9 9 9 8 3330	9 9 8 2 4972	9 9 7 1 4934
$\log \lambda$	9 1 8 4 7058	7 5 1 1 6022	7 1 3 7 3646	8 3 1 9 2578	8 5 2 9 1804
λ	+ 0 0 1 5 301	+ 0 0 0 3 248	+ 0 0 0 1 372	+ 0 0 0 0 557	+ 0 0 0 3 821

$\log_{10} \frac{1}{x}$	8.1652726 + 0.0146	7.5040172 + 0.0032	7.1277002 + 0.0013	8.2955718 + 0.0198	5.1945112 + 0.0312
$\sum \frac{1}{n^2}$	+ 0.0000124	+ 0.0000006	+ 0.0000001	+ 0.00000227	+ 0.0000566
$\lambda + \frac{1}{\lambda}$	+ 0.8486343	+ 0.8365813	+ 0.8347053	+ 0.8541903	+ 0.8671542
$\log \left[1 + \frac{1}{x} - \frac{1}{x^2} \right]$	9.9287269	9.9225085	9.9215332	9.9315662	9.9351245
$\log_{10} \frac{1}{x}$	8.5601256	7.8538504	7.5062262	8.6905948	8.9204161
$\log_{10} \frac{1}{x}$	+ 0.03632	+ 0.00714	+ 0.00721	+ 0.04904	+ 0.05326
$\log_{10} \eta^2$	0.0320958	0.0065049	0.0020804	0.0426705	0.0705610
$\log_{10} \eta$	0.01604929	0.0034025	0.0015402	0.0218352	0.0352805
$\log_{10} \left[1 + \frac{1}{\eta} \right]$	0.0441365	0.0454155	0.0456014	0.0486222	0.0423529
$\log_{10} \frac{1}{\eta}$	0.0606294	0.0888180	0.0471419	0.0654575	0.0776234
$\log_{10} \frac{1}{\eta^2}$	8.5271394	7.8470455	7.5021478	8.6469243	8.8495551
$\log_{10} (\eta^2 - 1)$	8.5877602	7.8958635	7.5502571	8.7123815	8.9274355
$\log_{10} \eta$	0.0164908	0.0034069	0.0015409	0.0218391	0.0352791

$\sum_{i=1}^n w_i$	8.483555	7.7763559	7.4277594	8.621610	8.8555409
$\sum_{i=1}^n w_i^2$	3.222075	0.0068049	0.0030504	0.0436715	0.0705610
$\sum_{i=1}^n w_i^3$	8.483555	7.7763559	7.4277594	8.621610	8.8555409
$\sum_{i=1}^n w_i^4$	+ 0.02457	+ 0.00588	+ 0.0026	+ 0.03789	+ 0.06137
$\sum_{i=1}^n w_i^5$	+ 0.01530	+ 0.00325	+ 0.00137	+ 0.02086	+ 0.03382
$\sum_{i=1}^n w_i^6$	+ 0.01327	+ 0.00263	+ 0.00137	+ 0.01703	+ 0.02755
$\sum_{i=1}^n w_i^7$	+ 0.000101	+ 0.0000011	+ 0.000001	+ 0.000168	+ 0.000441
$\sum_{i=1}^n w_i^8$	+ 0.8486343	+ 0.8263313	+ 0.8347053	+ 0.8541903	+ 0.8671543
$\sum_{i=1}^n w_i^9$	9.957957	9.923504	9.9215332	9.9315632	9.938155
$\sum_{i=1}^n w_i^{10}$	8.483555	7.7763559	7.4277594	8.621610	8.8555409
$\sum_{i=1}^n w_i^{11}$	8.5001268	+ 8.533505	7.5062202	8.6905978	8.9204224
$\sum_{i=1}^n w_i^{12}$	+ 0.036318	+ 0.007143	+ 0.003208	+ 0.049045	+ 0.083257
$\sum_{i=1}^n w_i^{13}$	0.0326741	+ 0.0068077	+ 0.0030755	+ 0.0436716	0.0705610
$\sum_{i=1}^n w_i^{14}$	8.4558794	7.7695512	7.4246809	8.5784564	8.789521
$\sum_{i=1}^n w_i^{15}$	+ 0.028568	+ 0.005582	+ 0.002659	+ 0.03789	+ 0.06137
$\sum_{i=1}^n w_i^{16}$	+ 0.015301	+ 0.003248	+ 0.00137	+ 0.020857	+ 0.033821
$\sum_{i=1}^n w_i^{17}$	+ 0.013267	+ 0.002631	+ 0.001287	+ 0.017000	+ 0.027557
$\sum_{i=1}^n w_i^{18}$	+ 0.0001012	+ 0.0000004	+ 0.000001	+ 0.000168	+ 0.000441

$\log \eta$	0.0164571	0.0034039	0.0015393	0.0218373	0.0252794
$\log \eta^2$	0.0441370	0.0454154	0.0456015	0.0436220	0.0436220
$\log \eta^3$	0.0606241	0.0455195	0.0471477	0.0659353	0.0776325
$\log \eta^4$	0.07271547	0.0470425	75081477	0.0469232	0.0776325
$\log \eta^5$	0.0877788	0.0485621	75512859	0.07122808	0.0877788
$\log \eta^6$	0.0964012	0.0030169	0.0015393	0.07122808	0.0964012
$\log \eta^7$	0.0320524	0.0065135	0.0030169	0.0436752	0.0705596
$\log \eta^8$	0.055701	0.07645451	0.0446776	0.0784826	0.0784826
$\log \eta^9$	+ 0.028567	+ 0.005882	+ 0.002659	+ 0.037556	+ 0.061374
$\log \eta^{10}$	0.0164912	0.0034069	0.0015409	0.0215391	0.0252798
$\log \eta^{11}$	0.0441365	0.0454150	0.0456016	0.0436217	0.0436217
$\log \eta^{12}$	0.0606257	0.0455199	0.0471477	0.0659365	0.0776325
$\log \eta^{13}$	0.07271444	0.04704367	0.0485604	0.0469106	0.0776325
$\log \eta^{14}$	0.08777721	0.04856586	0.0502860	0.07123404	0.08777721
$\log \eta^{15}$	0.0164909	0.0034069	0.0015409	0.0215390	0.0252796

$\log_{10} 10^3$	8.1619236	7.024976	7.1258715	8.293564	4.1111
$\times$	$+ 0.0145$	$+ 0.0032$	$+ 0.0013$	$+ 0.0147$	$+ 0.0311$
$\frac{1}{2}$	$+ 0.0000022$	$+ 0.000006$	$+ 0.000001$	$+ 0.000024$	$+ 0.000053$
$1 + \frac{1}{2}$	$+ 0.8485603$	1.846072	$+ 0.848002$	$+ 0.854163$	$+ 0.8670223$
$1 + \frac{1}{2} + \frac{1}{4}$	9.9286873	9.9225051	9.918711	9.9315170	9.9480178
$\log_{10} 10^4$	8.55512232	7.5234602	7.505068	6.890000	8.0152221
$\times$	$+ 0.036081$	$+ 0.007126$	$+ 0.001181$	$+ 0.048400$	$+ 0.058$
$\log_{10} 10^5$	0.0321492	0.0068012	0.0030728	0.0427220	0.0520471
$\log_{10} 10^6$	0.0163507	0.0034006	0.0015364	0.0217635	0.0261116
$\log_{10} (1 + \frac{1}{10})$	0.0006555	0.0008815	0.0007120	0.0053420	0.0074411
$\log_{10} \frac{1}{2}$	8.5244059	7.5466650	7.44194740	8.6454280	8.547450
$\log_{10} (1-1)$	8.8550204	7.8954872	7.5465847	8.7408720	8.7264741
η	0.0163503	0.0024002	0.0015260	0.0217639	0.0251514

$\log 17$	0.1652558	0.1507943	0.1652558	0.1605975	0.1652558
$\log 18$	0.1528145	0.1453720	0.1605978	0.1453078	0.1453078
$\log 19$	0.3160501	0.261031	0.2258536	0.2059036	0.2105636
$\log 20$	0.9872090	0.9972252	0.9985357	0.9825798	0.9721288
$\log 21$	0.2542380	0.2482552	0.249681	0.2526098	0.241585
$\log 22$	0.6042881	0.5943543	0.6257223	0.595154	0.5837221
$\log 23$	0.2987906	0.2892988	0.3011094	0.2892456	0.6075346
$\log 24$	1.8128643	1.7830719	1.871669	1.7685462	1.7511663
$\log 25$	5.4859463	7.7762269	7.4239425	8.6206994	8.8563683
$\log 26$	0.0144615	0.0054565	0.0046580	0.0152900	0.0199450
$\log 27$	0.0072308	0.0024433	0.0023290	0.0076450	0.0060711
$\log 28$	45° 39' 17.6"	45° 10' 51.4"	45° 9' 13.1"	45° 30' 15.4"	45° 39' 25.2"
$\log 29$	0 57' 14.0"	0 21' 42.8"	0 18' 26.2"	1 0' 30.8"	1 15' 56.6"
$\log 30$	6.4428306	5.6009168	5.4588256	6.4912442	6.7222360
$\log 31$	8.1617432	7.5020344	7.1255092	8.2935542	8.4924846
$\log 32$	8.1699682	7.5083950	7.1248144	8.000562	8.497070
$\log 33$	4.9872080	4.9972252	4.9985357	4.9825798	4.9721288
$\log 34$	8.1827602	7.5111698	7.1359757	8.3177765	8.5276685
$\log 35$	7.0015232	7.0003245	7.001365	7.0020780	7.0020780

$$A_0 = \frac{1}{x}$$

$$A_1 = \frac{1}{x^2}$$

$$A_2 = \frac{1}{x^3}$$

$$A_3$$

$$A_4$$

$$A_5 = \frac{1}{x^6}$$

$$A_6 = \frac{1}{x^7}$$

$$A_7 = \frac{1}{x^8}$$

$$8.161 \dots$$

$$+ 0.0012$$

$$+ 0.0000006$$

$$+ 0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$-1.255092$$

$$+ 0.0013$$

$$+ 0.0000001$$

$$+ 0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$8.002255$$

$$+ 0.0011$$

$$+ 0.0000000$$

$$+ 0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$8.002255$$

$$+ 0.0011$$

$$+ 0.0000000$$

$$+ 0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$8.002255$$

$$+ 0.0011$$

$$+ 0.0000000$$

$$+ 0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$$0.0000000$$

$\log m$	8.4559263	7.7762269	7.4239425	8.6206944	8.8722682
$\log \frac{m}{n}$	0.0321178	0.0065056	0.0030522	0.0435422	0.0102745
$\log m/n^2$	8.4531495	7.7694213	7.4208903	8.5771572	8.7861125
$\log \frac{m}{n^2}$	+ 0.018289	+ 0.005881	+ 0.002686	+ 0.03771	+ 0.06110
$\log \frac{m}{n^3}$	+ 0.01722	+ 0.003245	+ 0.001365	+ 0.020756	+ 0.033702
$\log \frac{m}{n^4}$	+ 0.0122	+ 0.0026	+ 0.0013	+ 0.0170	+ 0.0214
$\log \frac{m}{n^5}$	+ 0.0000100	+ 0.000004	+ 0.0000001	+ 0.000167	+ 0.0000435
$\log \frac{m}{n^6}$	+ 0.8455653	+ 0.565753	+ 0.8347013	+ 0.5541193	+ 0.8670363
$\log \frac{m}{n^7}$	1.4280102	0.9225070	0.9215309	0.9315271	0.9380542
$\log \frac{m}{n^8}$	5.4859263	7.762269	7.4239425	8.6206944	8.8722682
$\log \frac{m}{n^9}$	8.557360	7.8537199	7.5024116	8.6891723	8.9183041
$\log \frac{m}{n^{10}}$	+ 0.036077	+ 0.007140	+ 0.003180	+ 0.045555	+ 0.082870

Section VIII.

The computation according to

the formulae in section VII.

Result.

$\log(\eta'-1)$	8.5877721	$\log(\eta'_0-1)$	7.5502869
$\log(\eta''-1)$	7.8958586	$\log(\eta''_0-1)$	8.7123804
$\log((\eta'-1)-(\eta''-1))$	8.4890782	$\log((\eta'_0-1)-(\eta''_0-1))$	8.6813982 _n
$\log \eta' x$	8.7842811	$\log \eta'' x$	8.7693310
$\log Y''$	9.7047971	$\log Y''_0$	9.4120672 _n
$\log(\eta''-1)$	8.9274955	$\log(\eta''-1)$	8.9274955
$\log(\eta'''-1)$	7.8958586	$\log(\eta'''_0-1)$	8.7123804
$\log(\eta'''-1)$	0.1892603	$\log(\eta'''_0-1)$	4.8065541
$\log(\eta'''-1)-(\eta''-1)$	5.5851184	$\log((\eta'''_0-1)-(\eta''_0-1))$	8.5192653
$\log \eta'' x$	8.8030698	$\log \eta'' x$	8.8030698
$\log Y'$	0.0820491	$\log Y'_0$	4.7161955

Section VIII. (continued)

Second Trial.

$\log (\eta' - 1)$	8.5850094	$\log (\eta'_0 - 1)$	7.4465217
$\log (\eta'' - 1)$	7.8954555	$\log (\eta''_0 - 1)$	8.102720
$\log ((\eta' - 1) - (\eta'' - 1))$	8.4857214	$\log ((\eta'_0 - 1) - (\eta''_0 - 1))$	8.6800634 _n
$\log \eta' x$	8.7821988	$\log \eta' x$	8.7612115
$\log Y''$	9.7035276	$\log Y''_0$	9.9123814 _n
$\log (\eta'' - 1)$	8.6254791	$\log (\eta'' - 1)$	8.7554791
$\log (\eta''' - 1)$	7.8954835	$\log (\eta'''_0 - 1)$	8.7108720
$\log ((\eta'' - 1) - (\eta''' - 1))$	8.8829228	$\log ((\eta'' - 1) - (\eta''' - 1))$	8.5164031
$\log \eta' x$	8.8009267	$\log \eta'' x$	8.8009267
$\log Y'$	0.0819961	$\log Y'_0$	9.7154764

Section VIII (continued).

Third value γ' .

$\log(\gamma'_1-1)$	8.5849916
$\log \gamma'_m-1)$	7.8957356
$\log((\gamma'_1-1)(\gamma'_m-1))$	8.4856079
$\log \gamma'_x$	8.7822944
$\log Y''$	4.705155
$\log(\gamma''-1)$	8.0255458
$\log(\gamma'''-1)$	7.8957356
$\log((\gamma''-1)(\gamma'''-1))$	8.8822944
$\log \gamma''_x$	8.8010329
$\log Y'$	0.0819411

$\log(\gamma'_1-1)$	7.5464909
$\log(\gamma'_m-1)$	8.7110290
$\log((\gamma'_1-1)(\gamma'_m-1))$	5.6862267 ₄
$\log \gamma'_x$	8.7674316
$\log Y''$	4.9127951 _n
$\log(\gamma''-1)$	8.9255458
$\log(\gamma'''-1)$	8.7110290
$\log((\gamma''-1)(\gamma'''-1))$	8.5162625
$\log \gamma''_x$	8.8010329
$\log Y'$	4.7153306

Section II.

Computation according to

Table in Section II.

$\log \gamma \bar{r}^m$	0.1652644
$\log \gamma \bar{r}$	0.1450025
$\log \gamma \bar{r}^{10}$	0.3105669
$\log \gamma \bar{r}^2$	0.4721295
$\log \gamma \bar{r}^3$	0.2731545
$\log 2 \cos f'' \gamma \bar{r}^m$	0.5837264
$\log \tau^m$	0.6075346
$\log (2 \cos f'' \gamma \bar{r}^m)^3$	1.7511792
$\log m_n$	8.8563554

$\log \gamma \bar{r}^m$	0.0199649
$\log \tan(45^\circ + \omega)$	0.0044810
$45^\circ + \omega'$	$45^\circ 24' 20''$
$2\omega'$	$1' 19'' 0$

$\log \tan^2 \omega'$	6.7225564
$\log \sin^2 \frac{1}{2} f''$	8.4924694
$\log (\tan^2 \omega' + \sin^2 \frac{1}{2} f'')$	8.4997533
$\log \cos f''$	9.9721295
$\log \gamma \bar{r}_n$	8.2276525
l_n	+ 0.032702

x_n	+ 0.0274
z_n	+ 0.000043
$l_n + \frac{e}{6}$	+ 0.8670353
$\log (\tau + l_n + \frac{e}{6})$	4.9585857
$-l_n - \frac{e}{6}$	8.9152967
$-x_n$	+ 0.0274

$\log \eta'$	0.0702541
$\log m_n / \eta_n^2$	8.7561013

$m_n' \eta_n'$	+ 0.061105
l_n	+ 0.032702

$2m_n' \eta_n'$	+ 0.027406
$l_n - m_n' \eta_n'$	8.4378451
$l_n - m_n' \eta_n'$	4.159259

l_n	$9^\circ 31' 44.6''$
l_n	$19^\circ 2' 44.6''$

Section X

Computation according to G.H.

Example 1. "X" of "X".

$\frac{1}{2}(\pi'' + \beta)$	19 40 55.7	$\cos \frac{1}{2}(\pi - \beta)$	0.2226269
$\frac{1}{2}(\pi'' - \beta)$	0 37 54.5	$\sin \frac{1}{2}(\pi - \beta)$	0.9755580
$\frac{1}{2}\omega''$	1 0 00		
$\cos \frac{1}{2}(\pi'' + \beta)$	9.9738529	$\sin \frac{1}{2}\beta$	8.1055219
$\tan \frac{1}{2}\omega''$	836.14247	$\cos \frac{1}{2}\beta$	9.5284008
$\cos \frac{1}{2}(\pi'' - \beta)$	9.99999742	$\tan \frac{1}{2}\beta$	8.8771211
$\sin \frac{1}{2}(\pi'' + \beta)$	9.5273920	$\frac{1}{2}\beta$	1.5 4.1
$\sec 2\omega''$	0.0001147	β	3 3 8".2
$\sin \frac{1}{2}(\pi'' - \beta)$	8.0376523	$\sin \frac{1}{2}\beta$	9.9987704
$\cos \frac{1}{2}(\pi'' + \beta) \tan 2\omega''$	8.3552826	β^2	4.5296304
$\sin \frac{1}{2}(\pi'' + \beta) \sec 2\omega''$	9.5275067	$\sin \frac{1}{2}\omega'' \cos \frac{1}{2}\beta$	9.1295147
		$(\frac{1}{2}\beta)^2 \sin \omega''$	9.5647575 } check
		$\frac{1}{2}\beta \omega''$	0.0351271
$\cos \frac{1}{2}(\pi - \beta)$	8.8077759	$\tan \beta$	9.5296204
$\cos \frac{1}{2}(\pi + \beta)$	9.99991059		
$\cos \frac{1}{2}(\pi'' - \beta) \tan 2\omega''$	836.14019	$\frac{1}{2}(\pi + \beta)$	60 56 3.0
$\sin \frac{1}{2}(\pi'' - \beta) \sec 2\omega''$	8.037670	$\frac{1}{2}(\pi - \beta)$	2 40 51.4
		π	68 1 4.4
		β	60 56 16
π	180 0 0.8	π''	88 55 5.5
π'	181 52 2.4	ω''	47 58 16.5

Section XI.

continued according to

continued in section XI

v''	$88^{\circ} 35' 32.5''$	$\log \sin E'$	9.8244619
v'	$47^{\circ} 58' 36.3''$	$\log v''$	4.4901174
E''	$79^{\circ} 59' 30.8''$	$\log \sin E''$	9.9933406
E'	$41^{\circ} 52' 32.4''$	$\log v'' \sin E'$	4.145795
$\log \eta''$	0.0551271	$v'' \sin E'$	$5^{\circ} 47' 57.8''$
$\log r''$	0.2906050	$\log v'' \sin E''$	4.4834580
$\log r'''$	0.2305787	$v'' \sin E''$	$8^{\circ} 27' 20.9''$
$\log \sin 2f''$	9.8135684	M'	$26^{\circ} 8' 38.6''$
$\log(\eta'' r'' \sin 2f'')$	0.4648292	M''	$71^{\circ} 32' 9.9''$
$\log(\eta'' r'' \sin 2f'')^2$	0.9396584	$M''' - M'$	$25^{\circ} 23' 21.3''$
$\log r'^2$	0.6075346	$\log(M''' - M')$	5.1052079
$\log \rho$	0.2321238	$\log(r''' - r')$	2.0681859
$\log \sec^2 q$	0.0098648	$\log u$	3.070220
$\log u$	0.3417586	$\log \delta''$	2.5500066
$\log \delta''$	2.5500066	$\log u^{3/2}$	0.5129829
$\log u^{3/2}$	0.5129829	$\log u$	3.0370237
$\log u$	3.0370237	$\log \sin q$	9.1756923
$\log \sin q$	9.1756923	$\log \sin r''$	4.6855744
$\log \sin r''$	4.6855744	$\log v''$	4.4901174
$\log v''$	4.4901174		

Action XII.

Computation according to

formula in section XII.

$\log \tan i'$	8.5234698	$\log \tan u'$	0.1400615 _n
$\log \sec (i'' - i')$	9.8802725	$\log \tan u''$	4.3800985 _n
$\log \tan i''$	8.4038433	u'	12.5 5' 23.2
$\log \tan i'''$	7.9826528	$u'' - u'$	206 21 22.8
$\log (\sec i'' - \sec i' \cos (i'' - i'))$	5.1968591 _n	π	122 22 54.0
$\log \sin (i'' - i')$	9.8134622	u'''	166 30 27.5
$\log \tan i \sin (i' - \delta)$	8.5234698	$\delta - u'''$	165 52 26.6
$\log \tan i \cos (i' - \delta)$	8.2832768 _n	π	222 22 54.1
$\log \tan (i' - \delta)$	0.14006150 _n	$u''' - u'$	40 36 56.2
$\log \sin (i' - \delta)$	9.9064246	τ_0	1888.0
$i' - \delta$	125° 54' 54".3	$\tau_0 - \tau'$	79.5 days
$i \delta$	254 27 54.1	$\tau''' - \tau'_0$	27.5 " "
$\log \tan i$	8.6150452	$\mu [\tau_0 - \tau'_0]$	24 2' 54.32
i	2° 41' 26".2	$\mu [\tau''' - \tau'_0]$	11 20 26.95
$i'' - \delta$	166° 31' 27".2	$M' + \mu [\tau_0 - \tau']$	60 11 32.42
$\log \tan (i'' - \delta)$	0.14006150 _n	$M''' + \mu [\tau''' - \tau'_0]$	60 11 32.45
$\log \sec i$	0.0003685		
$\log \tan (i''' - \delta)$	4.3797200 _n		

Elements of the Comet (Quadrant 2, 0)

Epoch: Greenwich Mean Time Jan. 1, 1885.0

$$M = 60^{\circ} 11' 32.4''$$

$$\pi = 332^{\circ} 22' 54.0''$$

$$16 = 254^{\circ} 27' 50.1''$$

$$i = 2^{\circ} 1' 36.2''$$

$$q = 8.37 \text{ a.u.}$$

$$n = 1088^{\circ} 11.1''$$

$$\log a = 0.3414856$$

mean Equinox and Ecliptic for
1885.0

These elements are found to give us a correction to the normal places:

Observed - Computed

	$\Delta \alpha$	$\Delta \delta$
Oct. 11.5	+ 0.05	- 0.5
Nov. 10.5	+ 0.35	[- 1.3]
Dec. 11.5	- 0.26	[- 1.3]
Jan. 6.5	- 0.15	- 4.1

Part Second.

Variation of the elements by means of
additional observations.

We have now derived a set of elements from which we are to compute, in the next step x , y and z , the geocentric co-ordinates of the planet. They may be regarded as functions of the time and of the six elements - the co-ordinates of the sun being zero.

The observed positions of the planet are now to be compared with those which are derived by calculation, and the variation of the elements to be found, which will cause the residuals between the observed and computed values to be reduced to a minimum.

Each observation will give two equations of condition which we can imagine to be expressed in

the form

$$(u, \delta) = \gamma (t, \pi, M_0, n, i, \delta,) \quad (1)$$

where M_0 represents the mean anomaly at the epoch T . By these expressions is to be understood, that having given the quantities in the second members we can calculate those of the first.

Let the numerical values of the six elements which we have derived be designated by

$$t_0, \pi_0, M_0, n_0, i_0, \delta_0.$$

These quantities we know to be quite near to the true values which are to be found. Represent the maximum correction to be applied to these elements - to give the true values by

$$\Delta t_0, \Delta \pi_0, \Delta M_0, \Delta n_0, \Delta i_0, \Delta \delta_0.$$

The corrected values of the elements will then be

$$t = t_0 + \Delta t_0$$

$$\pi = \pi_0 + \Delta \pi_0$$

$$n = n_0 + \Delta n_0$$

$$M = M_0 + \Delta M_0$$

$$i = i_0 + \Delta i_0$$

$$B = B_0 + \Delta B_0$$

Consider these values to be substituted in (a). Then the true values of α and ϵ will be represented by an expression of the form

$$f(\epsilon_0, \pi_0, \Delta M_0, \Delta \mu_0, \Delta i_0, \Delta \delta_0, \dots)$$

This expression may be developed in powers of the increments $\Delta \epsilon_0, \Delta M_0$, etc. The term independent of these quantities will be

$$f(\epsilon_0, \pi_0, \Delta M_0, \Delta \mu_0, \Delta i_0, \Delta \delta_0, \dots)$$

which will give the values of α and ϵ calculated by means of the uncorrected elements. If we call these values α_0 and ϵ_0 , we will have for terms of the first order

$$\frac{\partial f}{\partial \epsilon_0} \Delta \epsilon_0 + \frac{\partial f}{\partial \pi_0} \Delta \pi_0 + \frac{\partial f}{\partial M_0} \Delta M_0 + \frac{\partial f}{\partial \mu_0} \Delta \mu_0 + \frac{\partial f}{\partial i_0} \Delta i_0 + \frac{\partial f}{\partial \delta_0} \Delta \delta_0,$$

It is essential that the variations $\Delta \epsilon, \Delta M, \Delta i$, etc. shall be so small that terms of the second order in these quantities may be neglected. This will give us for the correct values of α and ϵ sought, the equations

$$\alpha = \alpha_0 + \frac{\partial \alpha}{\partial \pi_0} \Delta \pi_0 + \frac{\partial \alpha}{\partial \epsilon_0} \Delta \epsilon_0 + \dots$$

$$\delta = \delta_0 + \frac{\partial \delta}{\partial \pi_0} \Delta \pi_0 + \frac{\partial \delta}{\partial \epsilon_0} \Delta \epsilon_0 + \dots$$

From the observations we have given directly the values of α and δ ; thus the first members of the above equations become known quantities. Denoting now $\Delta \alpha$ and $\Delta \delta$ for the differences between the observed and computed values of α and δ we can write the equations

$$\Delta \alpha = \frac{\partial \alpha}{\partial \pi_0} \Delta \pi_0 + \frac{\partial \alpha}{\partial \epsilon_0} \Delta \epsilon_0 + \frac{\partial \alpha}{\partial u_0} \Delta u_0 + \dots$$

$$\Delta \delta = \frac{\partial \delta}{\partial \pi_0} \Delta \pi_0 + \frac{\partial \delta}{\partial \epsilon_0} \Delta \epsilon_0 + \frac{\partial \delta}{\partial u_0} \Delta u_0 + \dots$$

where $\Delta \alpha$ and $\Delta \delta$ stand respectively for $\alpha - \alpha_0$ and $\delta - \delta_0$.

Six such equations will enable us to determine $\Delta \pi_0$, $\Delta \epsilon_0$, Δu_0 , and by (b) we have at once the values of the elements themselves. But before we can utilize these equations it is necessary to first compute the values of the partial derivatives

$$\frac{\partial \alpha}{\partial \pi_0}, \frac{\partial \alpha}{\partial \epsilon_0}, \dots; \quad \frac{\partial \delta}{\partial \pi_0}, \frac{\partial \delta}{\partial \epsilon_0}, \dots;$$

which form the coefficients of the first-hand members in the

above expression

is used in making the calculation for the partial differential coefficient of α and δ with respect to the heliocentric co-ordinates are as follows:

III.

$$\cos \delta \frac{\partial \alpha}{\partial x} = - \frac{\sin \alpha}{\xi}$$

$$\cos \delta \frac{\partial \alpha}{\partial y} = \frac{\cos \alpha}{\xi}$$

$$\cos \delta \frac{\partial \alpha}{\partial z} = 0$$

$$\frac{\partial \delta}{\partial x} = - \frac{\cos \alpha \sin \delta}{\xi}$$

$$\frac{\partial \delta}{\partial y} = - \frac{\sin \alpha \sin \delta}{\xi}$$

$$\frac{\partial \delta}{\partial z} = \frac{\cos \delta}{\xi}$$

Partial differential coefficients of the heliocentric co-ordinates with respect to the element x —

$$\frac{\partial x}{\partial \pi} = \frac{\partial x}{\partial f} = x \cot (A + u)$$

$$\frac{\partial y}{\partial \pi} = \frac{\partial y}{\partial f} = y \cot (B + u)$$

$$\frac{\partial z}{\partial \pi} = \frac{\partial z}{\partial f} = z \cot (C + u)$$

$$\frac{\partial x}{\partial x_0} = -\frac{dx}{dx_0} = x \cos \varepsilon - z \sin \varepsilon$$

$$\frac{\partial x}{\partial y_0} = -\frac{dy}{dy_0} = y \cos \varepsilon$$

$$\frac{\partial z}{\partial x_0} = -\frac{dz}{dx_0} = x \sin \varepsilon$$

$$\frac{\partial x}{\partial t_1} = r \sin u \cos a$$

$$\frac{\partial x}{\partial t_2} = r \sin u \cos b$$

$$\frac{\partial x}{\partial t_3} = r \sin u \cos c$$

$$\frac{\partial x}{\partial r} = \frac{x}{r} \quad \frac{\partial y}{\partial r} = \frac{y}{r} \quad \frac{\partial z}{\partial r} = \frac{z}{r}$$

$$\frac{\partial r}{\partial \varphi} = -u \cos \varphi \cos \tilde{\varphi}$$

$$\frac{\partial r}{\partial \varphi} = \left(\frac{1}{\cos \varphi} + \tan \varphi \cos \tilde{\varphi} \right) \sin \tilde{\varphi}$$

$$\frac{\partial r}{\partial u_1} = a \tan \varphi \sin \tilde{\varphi}$$

$$\frac{\partial r}{\partial u_2} = \frac{a^2 \cos \varphi}{r^2}$$

$$\frac{\partial r}{\partial \mu} = a \tan \varphi \sin \tilde{\varphi} (1 - T) - \frac{r}{u} \cos \varphi$$

$$\frac{\partial r}{\partial u_1} = \frac{a^2 \cos \varphi}{r^2} (1 - T)$$

$$\cos i \frac{\partial \alpha}{\partial \lambda_0} = \cos i \frac{\partial \alpha}{\partial r} \cdot \frac{\partial r}{\partial \lambda_0} + \cos i \frac{\partial \alpha}{\partial f} \cdot \frac{\partial f}{\partial \lambda_0}$$

$$\frac{\partial \epsilon}{\partial \lambda_0} = \frac{\partial \epsilon}{\partial r} \cdot \frac{\partial r}{\partial \lambda_0} + \frac{\partial \epsilon}{\partial f} \cdot \frac{\partial f}{\partial \lambda_0}$$

$$\cos i \frac{\partial \alpha}{\partial \mu} = \cos i \frac{\partial \alpha}{\partial r} \cdot \frac{\partial r}{\partial \mu} + \cos i \frac{\partial \alpha}{\partial f} \cdot \frac{\partial f}{\partial \mu}$$

$$\frac{\partial \epsilon}{\partial \mu} = \frac{\partial \epsilon}{\partial r} \cdot \frac{\partial r}{\partial \mu} + \frac{\partial \epsilon}{\partial f} \cdot \frac{\partial f}{\partial \mu}$$

Next we note the computation for the precession of the elements π , Ω , and i , to the equinox and ecliptic for the year 1887.0, according to the following formulas: -

§ 11.

$$\Delta' \Omega = - 0''.49 \pm \sin [\Omega + 71^\circ] \cos i.$$

$$\Delta \pi = \text{precession} = 50'' \cdot \mu$$

$$\Delta \Omega = \Delta' \Omega$$

$$\Delta i = + 0''.49 \pm \cos (\Omega + 71^\circ)$$

Mean Sun

T = 1888.0

π	$5^{\circ} 1' 54.0''$
i	$2^{\circ} 21' 6.4''$
Ω	$25^{\circ} 4' 59.1''$
$(\Omega + \gamma'')$	$26^{\circ} 1' 57.1''$
$\cos(\Omega + \gamma'')$	0.91456
$\tan \delta' \sin \gamma''$	0.609020
$\sin(\Omega + \gamma'')$	0.995710
$\cos i$	0.93396
$\sin \Omega$	0.7057
$\delta' \Omega$	$+ 11^{\circ} 77'$
$\delta' \pi$	$+ 50^{\circ} 24'$
$\delta' \Omega$	$+ 62^{\circ} 01'$
$\delta' i$	$- 0^{\circ} 07'$

T = 1887.0

π	$5^{\circ} 1' 54.0''$
i	$2^{\circ} 21' 6.4''$
Ω	$25^{\circ} 4' 59.1''$
$(\Omega + \gamma'')$	$26^{\circ} 1' 57.1''$
$\cos(\Omega + \gamma'')$	0.91456
$\tan \delta' \sin \gamma''$	0.609020
$\sin(\Omega + \gamma'')$	0.995710
$\cos i$	0.93396
$\sin \Omega$	0.7057
$\delta' \Omega$	$+ 11^{\circ} 77'$
$\delta' \pi$	$+ 50^{\circ} 24'$
$\delta' \Omega$	$+ 62^{\circ} 01'$
$\delta' i$	$- 0^{\circ} 07'$

1) Mean Equinox and Ecliptic for 1888.0

2) Mean Equinox and Ecliptic for 1887.0

Computation of Ephemeris

With the preceding deduced elements for the perspective epochs 1887.e and 1888.e we will now compute the geocentric co-ordinates α , δ and ϵ . for each date that we compute directly, the co-ordinates we also compute the corresponding correction to be made for aberration time, which is to be subtracted from the time of observation.

The computation of the Ephemeris will be made according to the following

formulas: -

IV.

$$\cot A = -\tan \delta \cos i$$

$$\cot B = \frac{\cos i}{\tan \delta \cos E_0} \cdot \frac{\cos (E_0 + \epsilon)}{\cos \epsilon}$$

$$\cot C = \frac{\cos i}{\tan \delta \cos E_0} \cdot \frac{\sin (E_0 + \epsilon)}{\sin \epsilon}$$

$$\sin a = \frac{\cos \delta}{\sin A}$$

$$\sin b = \frac{\sin \delta \cos \epsilon}{\sin B}$$

$$\sin c = \frac{\sin \delta \sin \epsilon}{\sin C}$$

And for a stick

$$r = \frac{1 - e \sin(C - E)}{\sin a \cos A}$$

$$x = r \sin a \sin (A + u)$$

$$y = r \sin b \sin (B + u)$$

$$z = r \sin c \sin (C + u)$$

$$\tan u = \frac{X + Y}{X - Y} \quad \tan v = \frac{Z + W}{X + Y} \cos a + \frac{Z - W}{X - Y} \sin a$$

$$E = M + e \sin M$$

$$u = f + \pi - B$$

$$r \sin f = a \cos i \sin E$$

$$r \cos f = a [\cos E - \sin i]$$

Formula for Orbital Time

$$T = +1.73 \sqrt{a^3} \Delta$$

Computation of the Constant

in Section XL.

$$T = 1857.0$$

$$\begin{array}{l} i \\ \delta \\ \epsilon \end{array} \quad \begin{array}{l} 2^{\circ} \quad 21' \quad 26.2 \\ 55' \quad 40' \quad 57.1 \\ 1' \quad 1' \quad 11.1 \end{array}$$

$$\begin{array}{l} \tan i \\ \cos \delta \\ \tan E_0 \end{array} \quad \begin{array}{l} 8.6150504 \\ 0.4282851_n \\ 0.1807622_n \end{array}$$

$$\begin{array}{l} E_0 \\ E_0 + \epsilon \\ \sin(E_0 + \epsilon) \\ \cos \epsilon \end{array} \quad \begin{array}{l} 17^{\circ} \quad 15' \quad 26.7 \\ 194 \quad 42 \quad 50.8 \\ 0.9855187_n \\ 0.9625495 \\ 0.0222602_n \end{array}$$

$$\begin{array}{l} \sin(E_0 + \epsilon) \\ \sin \epsilon \\ \cos \epsilon \end{array} \quad \begin{array}{l} 0.4048271_n \\ 0.5995955 \\ 0.8049316_n \end{array}$$

$$\begin{array}{l} \cos E_0 \\ \tan \delta \\ \cos i \\ \cos E_0 \tan \delta \end{array} \quad \begin{array}{l} 0.9944277_n \\ 0.5555185 \\ 0.9996215 \\ 0.5504462_n \\ 0.4411822_n \end{array}$$

$$\begin{array}{l} \sin B \\ \delta \end{array} \quad \begin{array}{l} 47^{\circ} \quad 15' \quad 4.5 \\ 15^{\circ} \quad 15' \quad 4.5 \end{array}$$

$$\begin{array}{l} \sin C \\ C \end{array} \quad \begin{array}{l} 21^{\circ} \quad 51' \quad 1.9 \\ 25^{\circ} \quad 1' \quad 1.9 \end{array}$$

$$\begin{array}{l} \sin A \\ A \end{array} \quad \begin{array}{l} 0.8551509_n \\ 34^{\circ} \quad 26' \quad 11.9 \end{array}$$

$$\begin{array}{l} \sin \delta \\ \sin A \end{array} \quad \begin{array}{l} 0.855571_n \\ 34.256269_n \\ 0.9996582 \end{array}$$

$$\begin{array}{l} \cos \epsilon \\ \sin \delta \cos \epsilon \\ \sin B \\ \sin \epsilon \end{array} \quad \begin{array}{l} 0.5998755 \\ 0.0838038_n \\ 0.9625495 \\ 0.4411822_n \\ 0.4816925_n \\ 0.9646605 \end{array}$$

$$\begin{array}{l} \sin \delta \sin \epsilon \\ \sin \epsilon \\ \sin \epsilon \end{array} \quad \begin{array}{l} 0.5876090 \\ 0.9995112_n \\ 0.5995560 \end{array}$$

Check:

$$\begin{array}{l} \sin \delta \sin \epsilon \\ \sin A \\ \sin C \end{array} \quad \begin{array}{l} 0.5876090 \\ 0.9996582 \\ 0.5555185 \end{array}$$

$$\begin{array}{l} C - B \\ \cos A \\ \tan i \end{array} \quad \begin{array}{l} 1^{\circ} \quad 20' \quad 2.4 \\ 0.4282851_n \\ 0.8551509_n \\ 8.6150504 \end{array}$$

	105. 2.5	105. 12.5	105. 16.5	105. 20.5	105. 24.5
λ	34° 56' 2"	36° 8' 38.7"	37° 21' 14.6"	38° 3' 50.5"	39° 16' 56.5"
μ	40° 32' 00"	41° 53' 40.0"	42° 15' 15.0"	44° 36' 40.0"	45° 57' 45.0"
$\sin E_0$	0.6411	0.846206	0.878401	0.89468122	0.90566594
$\cos E_0$	0.7660575	0.5314380	0.529576	0.52366246	0.51467162
E_1	3° 44' 40.0"	50° 44' 11.3"	50° 23' 11.5"	60° 1' 45.1"	60° 10' 11.1"
$\sin E_1$	0.0577	0.7652400	0.861416.1	0.843539.2	0.855648.1
$\cos E_1$	0.9971	0.644765	0.5057083	0.53463574	0.52568427
$\sin E_1$	0.3027892	0.314567	0.3158257	0.3365048	0.3466611
E	5° 34' 41.2"	50° 44' 54.1"	50° 22' 57.1"	60° 1' 42.0"	60° 10' 15.8"
$\sin E$	0.0950	0.7652400	0.861416.1	0.843539.2	0.855648.1
$\cos E$	0.9971	0.644765	0.5057083	0.53463574	0.52568427
$\sin(600E - 1119)$	0.5126501	0.5444622	0.556921	0.5637-0	0.5637-0
$\cos E$	0.8804684	0.9719200	0.8624553	0.8325540	0.8422034
$\sin E$	0.6760271	+0.744595	+0.728541	-0.92121	+0.695350
$\cos(600E - 1119)$	0.7556209	0.743220	0.7624378	0.7499364	0.7367552
$\sin 1119$	0.1497063	0.1615184	0.1727482	0.1834182	0.1935865
$\sin 1119$	0.8602525	0.7709145	0.5909700	0.45904521	0.3943899
$\cos 1119$	0.1276095	0.1163106	0.1044264	0.0919250	0.0787738
$\sin 1119$	0.02220968	0.0452078	0.0683219	0.0915032	0.1148127
$\cos 1119$	46° 27' 25.1"	47° 58' 56.2"	49° 29' 18.0"	50° 59' 30.4"	52° 29' 12.5"
$\sin 1119$	0.2894538	0.2906039	0.2917783	0.2929761	0.2941966
$\cos 1119$	124° 22' 31.8"	125° 53' 42.4"	127° 24' 24.7"	128° 54' 37.1"	130° 24' 19.2"
$\sin 1119$	0	110° 19' 54.8"	111° 50' 26.6"	113° 20' 49.0"	114° 50' 30.1"
$\cos 1119$	108° 48' 43.7"	19° 22' 21.8"	20° 53' 13.6"	22° 23' 26.0"	23° 53' 3.1"
$\sin 1119$	12° 51' 20.1"	25° 43' 42"	26° 13' 46.0"	27° 43' 55.7"	29° 13' 40.8"
$\cos 1119$	24° 11' 53.1"				

	Oct. 5	Oct. 12.5	Oct. 16	Oct. 20.5	Oct. 24.5
$\log(y+Y)$	9.4579581	9.4686796	9.4501005	9.4329020	9.4100061
$\log(x+X)$	9.9441045	9.9486181	9.9547014	9.9622004	9.9711174
$\log \tan \alpha$	9.5438826	9.5200615	9.4954241	9.4706876	9.4466082
$(\sin) \alpha$	19° 16' 52" 4	18° 19' 28"	17° 22' 22"	16° 27' 11"	15° 32' 12"
$(\cos) \alpha$	1° 17 ^m 53 ^s 4	1° 15 ^m 17 ^s 0	1° 14 ^m 20 ^s 11	1° 13 ^m 21 ^s 15	1° 12 ^m 25 ^s 1
$\log(z+Z)$	4.3130136	4.4081050	4.2855965	4.1683227	4.0521816
$\log(x+X)$	9.9441045	9.9486181	9.9547014	9.9622004	9.9711174
$\log \tan \alpha$	9.2659091	9.2494864	9.2285949	9.2075503	9.1860642
$(\sin) \alpha$	9.4749302	9.4774013	9.4797152	9.4815124	9.4826022
$\log \tan \alpha$	9.3438893	9.3268882	9.3086102	9.2892041	9.2695214
δ	12° 26' 48" 1	11° 59' 54"	11° 30' 18"	11° 1' 11"	10° 12' 47"
$\log(z+Z)$	4.120126	4.451050	4.2855965	4.1683227	4.0521816
$\log \sin \delta$	4.3335102	4.3173176	4.2947971	4.2721150	4.2492391
$\log \Delta$	9.9795024	9.9607672	9.9387442	9.9157100	9.8924526
$\log \tan \alpha$	9.7400	9.7413	9.7443	9.7470	9.7503
$(\cos) \alpha$	-0.0050	-0.0055	-0.0056	-0.0056	-0.0057

	100-20	100-10	100-5	100-0	100-0	100-0
40	59	24	48	24	48	24
47	12	45.0	49	59	45.0	49
50	22	45.0	50	59	45.0	50
53	22	45.0	53	59	45.0	53
55	22	45.0	55	59	45.0	55
58	22	45.0	58	59	45.0	58
60	22	45.0	60	59	45.0	60
63	22	45.0	63	59	45.0	63
65	22	45.0	65	59	45.0	65
68	22	45.0	68	59	45.0	68
70	22	45.0	70	59	45.0	70
73	22	45.0	73	59	45.0	73
75	22	45.0	75	59	45.0	75
78	22	45.0	78	59	45.0	78
80	22	45.0	80	59	45.0	80
83	22	45.0	83	59	45.0	83
85	22	45.0	85	59	45.0	85
88	22	45.0	88	59	45.0	88
90	22	45.0	90	59	45.0	90
93	22	45.0	93	59	45.0	93
95	22	45.0	95	59	45.0	95
98	22	45.0	98	59	45.0	98
100	22	45.0	100	59	45.0	100

Calculation	Max. V	Max. S. S	Max. V	Max. S. S	Max. V
$\log (1 + \sum)$	14.0000	4.3809149	14.0000	4.3809149	14.0000
$\log (1 + \sum)$	14.0000	0.0041441	14.0000	0.0041441	14.0000
$\log \text{ both } \alpha$	14.0000	4.2851400	14.0000	4.2851400	14.0000
$\log \alpha$	14.0000	13.391476	14.0000	13.391476	14.0000
$(\log \alpha) \alpha$	14.0000	13.391476	14.0000	13.391476	14.0000
$\log (1 + \sum)$	14.0000	4.2246640	14.0000	4.2246640	14.0000
$\log (1 + \sum)$	14.0000	0.0041441	14.0000	0.0041441	14.0000
$\log \text{ both } \alpha$	14.0000	4.2255249	14.0000	4.2255249	14.0000
$\log \alpha$	14.0000	4.1815006	14.0000	4.1815006	14.0000
$\log \alpha$	14.0000	13.00572	14.0000	13.00572	14.0000
$(\log \alpha) \alpha$	14.0000	13.00572	14.0000	13.00572	14.0000
$\log (1 + \sum)$	14.0000	4.2246640	14.0000	4.2246640	14.0000
$\log (1 + \sum)$	14.0000	0.0041441	14.0000	0.0041441	14.0000
$\log \text{ both } \alpha$	14.0000	4.2255249	14.0000	4.2255249	14.0000
$\log \alpha$	14.0000	4.1815006	14.0000	4.1815006	14.0000
$\log \alpha$	14.0000	13.00572	14.0000	13.00572	14.0000
$(\log \alpha) \alpha$	14.0000	13.00572	14.0000	13.00572	14.0000

[illegible]

(1887)

54° 17' 37.7
61 52 40.0
44454411
44355555
7° 34' 22.0
61 51 56.7
44453957
44355131
7° 34' 19.2
61 51 56.4
61 51 56.7

44394608
0.6915120
+0.411157
44355497
0.5720120
44355577
0.4114787
680 21' 22.5
0.3057613
446° 16' 29.5

130° 42' 51.4
34 45 28.4
46 6 0.4

54° 17' 37.7

61 52 40.0
44454411
44355555
7° 34' 22.0
61 51 56.7
44453957
44355131
7° 34' 19.2
61 51 56.4
61 51 56.7

44394608
0.6915120
+0.411157
44355497
0.5720120
44355577
0.4114787
680 21' 22.5
0.3057613
446° 16' 29.5

130° 42' 51.4
34 45 28.4
46 6 0.4

54° 17' 37.7

61 52 40.0
44454411
44355555
7° 34' 22.0
61 51 56.7
44453957
44355131
7° 34' 19.2
61 51 56.4
61 51 56.7

44394608
0.6915120
+0.411157
44355497
0.5720120
44355577
0.4114787
680 21' 22.5
0.3057613
446° 16' 29.5

130° 42' 51.4
34 45 28.4
46 6 0.4

54° 17' 37.7

61 52 40.0
44454411
44355555
7° 34' 22.0
61 51 56.7
44453957
44355131
7° 34' 19.2
61 51 56.4
61 51 56.7

44394608
0.6915120
+0.411157
44355497
0.5720120
44355577
0.4114787
680 21' 22.5
0.3057613
446° 16' 29.5

130° 42' 51.4
34 45 28.4
46 6 0.4

(1957)	0.0000	0.0000	0.0000	0.0000	0.0000
$\log_{10} u$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log_{10} (u+u)$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log x$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
x	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$x + \sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log_{10} u$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log_{10} (u+u)$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log x$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
x	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$x + \sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log_{10} u$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log_{10} (u+u)$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\log x$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
x	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$\sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
$x + \sum$	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

	Dec 19	Dec 20	Dec 21	Dec 22
$\log(x+2)$	9.615-6.1	9.5792570	9.5446954	9.51-1.1
$\log(x+3)$	9.617-6.1	9.5814141	9.5464185	9.5130292
$\log 1000$	9.62-6.1	9.5839842	9.5482769	9.5491201
$\log 10000$	16.12-17.2	15.0231364	14.040'50.6	14.04'22.6
	16.4m 49.14	16.1m 34.43	16.5m 43.37	16.5m 43.37
$\log(x+2)$	9.3511261	9.3262944	9.3024402	9.2729313
$\log(x+3)$	9.3519454	9.3294142	9.31-6.1	9.280792
	9.3401907	9.3186502	9.2920212	9.2695921
	9.323935	9.3041337	9.285550	9.267659
	9.315842	9.2910139	9.269067	9.256540
	8.3127	8.2750	8.016'23.1	8.04'42.4
$\log(x+2)$	9.3711-6.1	9.326-9.44	9.3024402	9.2729313
$\log 1000$	9.3709301	9.3662921	9.350630	9.322364
$\log 10000$	9.374555	9.360022	9.345377	9.306049
	9.350	9.305	9.255	9.201
	9.30056	9.0083	9.00050	9.0000

$\angle$	$2^{\circ} 21' 16.2''$
α	$154^{\circ} 27' 57.1''$
β	$23^{\circ} 27' 15.6''$
γ	$56^{\circ} 15' 45.3''$
δ	$44^{\circ} 27' 15.7''$
ϵ	$41^{\circ} 57' 22.46''$
E_c	$171^{\circ} 15' 3''.6$
$E_c + z$	$194^{\circ} 42' 17''.2$
$\sin(E_c + z)$	0.99555372_n
$\cos z$	0.99625444
$\sin z$	0.0229873_n
$\sin(E_c + z)$	0.4045516
$\sin z$	0.5998931
$\cos z$	0.98046645_n
$\sin E_c$	0.99040170_n
$\tan \delta$	0.5560242
$\cos i$	0.99996515
$\cos E_c \tan \delta$	0.5500412_n
$\sin z$	0.4486903_n
$\sin B$	0.4716776
$\sin$	$253^{\circ} 29' 50''.6$
$\sin C$	0.2233548
$\sin$	$224^{\circ} 50' 24''.2$
$\sin A$	0.5556557_n
$\sin$	$244^{\circ} 27' 15''.9$

$\sin \delta$	0.4478157_n
$\sin A$	0.4428157_n
$\sin a$	0.4446575
$\sin \epsilon$	0.5998931
$\sin \delta$	0.4833344_n
$\cos \epsilon$	0.4625499
$\sin \delta \cos \epsilon$	0.4463895_n
$\sin B$	$0.4517.11_n$
$\sin b$	0.4646587
$\sin \delta \sin \epsilon$	0.5937330_n
$\sin C$	0.4971200_n
$\sin c$	0.5905970
$\sin b \sin c$	0.5522257
$\sin a$	0.4446575
$\div$	0.5555174
$C - B$	$6^{\circ} 20' 35''.6$
$\sin(C - B)$	0.0432619
$\cos A$	0.4833134
$\div$	0.0544485
$\tan i$	0.6150463
M	$60^{\circ} 11' 32''.9$
$\pi - \delta$	$77^{\circ} 24' 54''.1$

1	60 26' 55.4	61 51' 22.3	62 40' 16.2	64 4' 11.1
2	65 5' 45.0	69 52' 12.0	71 49' 41.0	72 46' 50.0
3	69 00 42.5	74 27 46	77 17 50.1	78 00 84.0
4	74 00 159.4	79 22 55.20	84 06' 46.0	85 22 01.1
5	79 0' 50.4	84 2' 52.2	89 0' 29.6	90 12' 5.9
6	84 57' 46.3	89 55' 14.2	94 49' 45.8	95 46' 49.0
7	89 00 436	94 2' 66.6	99 00 00	100 00 00
8	94 00 1610	99 22 40	104 06' 11.1	105 02 01.1
9	99 0' 51.5	104 3' 52.5	109 0' 45.4	110 1' 1.5
10	104 2' 46.2	109 55' 14.5	114 40' 46.0	115 46' 49.0
11	109 27' 11.4	114 55' 14.5	119 00' 46.0	120 46' 49.0
12	114 00 00	119 55' 14.5	124 00' 46.0	125 46' 49.0
13	119 00 00	124 00 00	129 00' 46.0	130 46' 49.0
14	124 00 00	129 00 00	134 00' 46.0	135 46' 49.0
15	129 00 00	134 00 00	139 00' 46.0	140 46' 49.0
16	134 00 00	139 00 00	144 00' 46.0	145 46' 49.0
17	139 00 00	144 00 00	149 00' 46.0	150 46' 49.0
18	144 00 00	149 00 00	154 00' 46.0	155 46' 49.0
19	149 00 00	154 00 00	159 00' 46.0	160 46' 49.0
20	154 00 00	159 00 00	164 00' 46.0	165 46' 49.0
21	159 00 00	164 00 00	169 00' 46.0	170 46' 49.0
22	164 00 00	169 00 00	174 00' 46.0	175 46' 49.0
23	169 00 00	174 00 00	179 00' 46.0	180 46' 49.0
24	174 00 00	179 00 00	184 00' 46.0	185 46' 49.0
25	179 00 00	184 00 00	189 00' 46.0	190 46' 49.0
26	184 00 00	189 00 00	194 00' 46.0	195 46' 49.0
27	189 00 00	194 00 00	199 00' 46.0	200 46' 49.0
28	194 00 00	199 00 00	204 00' 46.0	205 46' 49.0
29	199 00 00	204 00 00	209 00' 46.0	210 46' 49.0
30	204 00 00	209 00 00	214 00' 46.0	215 46' 49.0
31	209 00 00	214 00 00	219 00' 46.0	220 46' 49.0
32	214 00 00	219 00 00	224 00' 46.0	225 46' 49.0
33	219 00 00	224 00 00	229 00' 46.0	230 46' 49.0
34	224 00 00	229 00 00	234 00' 46.0	235 46' 49.0
35	229 00 00	234 00 00	239 00' 46.0	240 46' 49.0
36	234 00 00	239 00 00	244 00' 46.0	245 46' 49.0
37	239 00 00	244 00 00	249 00' 46.0	250 46' 49.0
38	244 00 00	249 00 00	254 00' 46.0	255 46' 49.0
39	249 00 00	254 00 00	259 00' 46.0	260 46' 49.0
40	254 00 00	259 00 00	264 00' 46.0	265 46' 49.0
41	259 00 00	264 00 00	269 00' 46.0	270 46' 49.0
42	264 00 00	269 00 00	274 00' 46.0	275 46' 49.0
43	269 00 00	274 00 00	279 00' 46.0	280 46' 49.0
44	274 00 00	279 00 00	284 00' 46.0	285 46' 49.0
45	279 00 00	284 00 00	289 00' 46.0	290 46' 49.0
46	284 00 00	289 00 00	294 00' 46.0	295 46' 49.0
47	289 00 00	294 00 00	299 00' 46.0	300 46' 49.0
48	294 00 00	299 00 00	304 00' 46.0	305 46' 49.0
49	299 00 00	304 00 00	309 00' 46.0	310 46' 49.0
50	304 00 00	309 00 00	314 00' 46.0	315 46' 49.0
51	309 00 00	314 00 00	319 00' 46.0	320 46' 49.0
52	314 00 00	319 00 00	324 00' 46.0	325 46' 49.0
53	319 00 00	324 00 00	329 00' 46.0	330 46' 49.0
54	324 00 00	329 00 00	334 00' 46.0	335 46' 49.0
55	329 00 00	334 00 00	339 00' 46.0	340 46' 49.0
56	334 00 00	339 00 00	344 00' 46.0	345 46' 49.0
57	339 00 00	344 00 00	349 00' 46.0	350 46' 49.0
58	344 00 00	349 00 00	354 00' 46.0	355 46' 49.0
59	349 00 00	354 00 00	359 00' 46.0	360 46' 49.0
60	354 00 00	359 00 00	364 00' 46.0	365 46' 49.0
61	359 00 00	364 00 00	369 00' 46.0	370 46' 49.0
62	364 00 00	369 00 00	374 00' 46.0	375 46' 49.0
63	369 00 00	374 00 00	379 00' 46.0	380 46' 49.0
64	374 00 00	379 00 00	384 00' 46.0	385 46' 49.0
65	379 00 00	384 00 00	389 00' 46.0	390 46' 49.0
66	384 00 00	389 00 00	394 00' 46.0	395 46' 49.0
67	389 00 00	394 00 00	399 00' 46.0	400 46' 49.0
68	394 00 00	399 00 00	404 00' 46.0	405 46' 49.0
69	399 00 00	404 00 00	409 00' 46.0	410 46' 49.0
70	404 00 00	409 00 00	414 00' 46.0	415 46' 49.0
71	409 00 00	414 00 00	419 00' 46.0	420 46' 49.0
72	414 00 00	419 00 00	424 00' 46.0	425 46' 49.0
73	419 00 00	424 00 00	429 00' 46.0	430 46' 49.0
74	424 00 00	429 00 00	434 00' 46.0	435 46' 49.0
75	429 00 00	434 00 00	439 00' 46.0	440 46' 49.0
76	434 00 00	439 00 00	444 00' 46.0	445 46' 49.0
77	439 00 00	444 00 00	449 00' 46.0	450 46' 49.0
78	444 00 00	449 00 00	454 00' 46.0	455 46' 49.0
79	449 00 00	454 00 00	459 00' 46.0	460 46' 49.0
80	454 00 00	459 00 00	464 00' 46.0	465 46' 49.0
81	459 00 00	464 00 00	469 00' 46.0	470 46' 49.0
82	464 00 00	469 00 00	474 00' 46.0	475 46' 49.0
83	469 00 00	474 00 00	479 00' 46.0	480 46' 49.0
84	474 00 00	479 00 00	484 00' 46.0	485 46' 49.0
85	479 00 00	484 00 00	489 00' 46.0	490 46' 49.0
86	484 00 00	489 00 00	494 00' 46.0	495 46' 49.0
87	489 00 00	494 00 00	499 00' 46.0	500 46' 49.0
88	494 00 00	499 00 00	504 00' 46.0	505 46' 49.0
89	499 00 00	504 00 00	509 00' 46.0	510 46' 49.0
90	504 00 00	509 00 00	514 00' 46.0	515 46' 49.0
91	509 00 00	514 00 00	519 00' 46.0	520 46' 49.0
92	514 00 00	519 00 00	524 00' 46.0	525 46' 49.0
93	519 00 00	524 00 00	529 00' 46.0	530 46' 49.0
94	524 00 00	529 00 00	534 00' 46.0	535 46' 49.0
95	529 00 00	534 00 00	539 00' 46.0	540 46' 49.0
96	534 00 00	539 00 00	544 00' 46.0	545 46' 49.0
97	539 00 00	544 00 00	549 00' 46.0	550 46' 49.0
98	544 00 00	549 00 00	554 00' 46.0	555 46' 49.0
99	549 00 00	554 00 00	559 00' 46.0	560 46' 49.0
100	554 00 00	559 00 00	564 00' 46.0	565 46' 49.0

	Jan 2.5	Jan 3.5	Jan 4.5	Jan 5.5	Jan 6.5	Jan 7.5
$\log \sin(A+u)$	0.8176010	0.3137062	0.7197770	0.2208608	0.7197770	0.2208608
$\log \sin(A+u)$	0.8116428	0.4625791	0.7932348	0.7835999	0.7835999	0.7835999
$\log \sin(A+u)$	0.1292738	0.112553	0.1130175	0.1044004	0.1044004	0.1044004
$\log \sin(A+u)$	+ 1.346409	+ 1.322164	+ 1.297232	+ 1.271022	+ 1.271022	+ 1.271022
$\log \sin(A+u)$	+ 0.206202	+ 0.257203	+ 0.307405	+ 0.350031	+ 0.350031	+ 0.350031
$\log \sin(A+u)$	+ 1.552911	+ 1.579067	+ 1.604725	+ 1.628859	+ 1.628859	+ 1.628859
$\log \sin(B+u)$	0.2220311	0.2837011	0.2947839	0.2858614	0.2858614	0.2858614
$\log \sin(B+u)$	0.2254256	0.2211007	0.8882746	0.443214	0.443214	0.443214
$\log \sin(B+u)$	0.1550595	0.1656866	0.1780647	0.1801825	0.1801825	0.1801825
$\log \sin(B+u)$	+ 1.438989	+ 1.464400	+ 1.489562	+ 1.514199	+ 1.514199	+ 1.514199
$\log \sin(B+u)$	- 0.881920	- 0.870627	- 0.856892	- 0.840748	- 0.840748	- 0.840748
$\log \sin(B+u)$	+ 0.557069	+ 0.593863	+ 0.632669	+ 0.673450	+ 0.673450	+ 0.673450
$\log \sin(C+u)$	1.0085702	0.9096454	0.910222	0.9117997	0.9117997	0.9117997
$\log \sin(C+u)$	0.9132487	0.9185093	0.9255020	0.9282870	0.9282870	0.9282870
$\log \sin(C+u)$	0.8218679	0.8281547	0.8342251	0.8400861	0.8400861	0.8400861
$\log \sin(C+u)$	+ 0.663542	+ 0.672216	+ 0.680012	+ 0.687060	+ 0.687060	+ 0.687060
$\log \sin(C+u)$	- 0.352621	- 0.377710	- 0.401761	- 0.426078	- 0.426078	- 0.426078
$\log \sin(C+u)$	+ 0.280021	+ 0.205406	+ 0.310941	+ 0.407111	+ 0.407111	+ 0.407111

	2000.2.5	2000.5.5	2000.8.5	2000.11.5	2000.11.7
$\log(s+z)$	0.7459090	0.736867	0.8011769	0.5283057	0.5550089
$\log(x+z)$	0.1011466	0.1064830	0.2054015	0.2118835	0.2179116
$\log \tan \alpha$	0.5547624	0.5752037	0.8957754	0.6164222	0.6370972
$\log \alpha$	19° 44' 32"	20° 36' 25.0"	21° 31' 12"	22° 27' 45.4"	23° 26' 21.0"
$\log \alpha'$	16 15 56.21	16 22 55.67	16 26 45.08	16 29 51.03	16 33 46.07
$\log(z+z)$	0.4485850	0.4705516	0.4926640	0.5148279	0.5369572
$\log(x+z)$	0.111466	0.1044430	0.2054015	0.2118835	0.2179116
$\log \tan \alpha$	0.5547624	0.5752037	0.8957754	0.6164222	0.6370972
$\log \alpha$	0.9737138	0.9712836	0.9686271	0.9657324	0.9628889
$\log \alpha'$	0.2311522	0.2423222	0.2558846	0.2686768	0.2816245
$\log \alpha'$	0° 39' 45.2"	0° 55' 59.8"	10° 13' 5.4"	10° 31' 0.5"	10° 49' 40.4"
$\log(z+z)$	0.4485850	0.4705516	0.4926640	0.5148279	0.5369572
$\log(x+z)$	0.2249459	0.2367925	0.2489458	0.2633193	0.2777777
$\log \tan \alpha$	0.2236391	0.2327591	0.2437182	0.2535086	0.2631277
$\log \alpha$	0.0641	0.1043	0.0042	0.0140	0.0220
$\log \alpha'$	0.0096	0.0098	0.0101	0.0103	0.0105

[illegible]

Since the stars have been reduced to the ecliptic and mean equinox for the beginning of the years from which we have derived the Ephemeris, the places of the planet just found are thus referred to the same equinox, also we have used the mean obliquity of the ecliptic for the adopted date of the fixed equinox, both in the computations of our auxiliary constants and in the final co-ordinates.

A further reduction must be made in order to reduce these places to the true equinox of the particular date. The formulae for precession and nutation are as follows:

$$\Delta \alpha = f + g \sin(G + \alpha) \tan \delta$$

$$\Delta \delta = g \cos(G + \alpha).$$

Given

$$\text{true } \alpha = \alpha + \Delta \alpha$$

$$\text{true } \delta = \delta + \Delta \delta$$

1387.

<u>G. M. T.</u>	<u>Oct. 8.5</u>	<u>Oct. 12.5</u>	<u>Oct. 16.5</u>	<u>Oct. 20.5</u>	<u>Oct. 24.5</u>
δ	12° 26.8	11° 59.0	11° 30.2	11° 11	10° 32.5
α	19 17.1	18 19.4	17 22.5	16 28.0	15 37.2
G	30 44.0	30 28.0	30 13.0	29 59.0	29 47.0
$G + \alpha$	50 1.1	47 35.5	47 35.5	46 27.0	45 24.2
$\sin(G + \alpha)$	1.38467	1.37639	1.36817	1.36020	1.35252
$\cos(G + \alpha)$	1.07900	1.08380	1.08890	1.09430	1.10000
$\sin(G + \alpha)$	1.380790	1.37876	1.37692	1.37521	1.37340
$\sin(G + \alpha)$	0.96373	0.96019	0.95717	0.95450	0.95252
$\tan \delta$	3.34384	3.32685	3.30859	3.28940	3.26971
f	+23.69	+24.03	+24.37	+24.73	+25.11
$\sin(G + \alpha) \tan \delta$	+2.03	+1.93	+1.84	+1.75	+1.67
$\Delta \alpha$	+2.72	+2.76	+2.81	+2.88	+2.98
$\Delta \alpha$	+1.71	+1.72	+1.74	+1.76	+1.78
$\Delta \delta$	+7.71	+7.99	+8.28	+8.56	+8.84

<u>G. M. T.</u>	<u>Oct. 28.5</u>	<u>Nov. 1.5</u>	<u>Nov. 5.5</u>	<u>Nov. 9.5</u>	<u>Nov. 13.5</u>
δ	10° 5.1	9° 29.6	9° 16.7	8° 56.5	8° 37.2
α	14° 51.6	14 12.2	13 39.8	13 14.9	12 58.0
$G + \alpha$	29 34.0	29 8.0	29 8.0	28 55.0	28 40.0
$G + \alpha$	44 25.6	42 47.9	41 10.9	42 1.1	41 18.1
$\sin(G + \alpha)$	1.84510	1.83212	1.83212	1.82690	1.82240
$\cos(G + \alpha)$	1.10590	1.11860	1.11860	1.12520	1.13200
$\sin(G + \alpha)$	1.845379	1.83556	1.83556	1.82994	1.82356
$\sin(G + \alpha)$	0.95100	0.95072	0.95072	0.95210	0.95440
$\tan \delta$	3.25007	3.21301	3.21301	3.19698	3.17380
f	+25.51	+26.37	+26.37	+26.84	+27.33
$\sin(G + \alpha) \tan \delta$	+1.60	+1.46	+1.46	+1.41	+1.34
$\Delta \alpha$	+27.11	+27.83	+27.83	+28.25	+28.67
$\Delta \alpha$	+1.81	+1.85	+1.85	+1.88	+1.91
$\Delta \delta$	+9.11	+9.64	+9.64	+9.89	+10.13

<u>Aug 11</u>	<u>Aug 21</u>	<u>Aug 27</u>	<u>Nov 27.5</u>	<u>Dec 1.2</u>
δ 8° 25.6	8° 17.4	8° 17.4	8° 5.9	8° 6.2
α 12 49.3	12 48.8	12 26.4	13 11.8	13 34.6
G 28 24.0	28 7.0	27 48.0	28 12.8	27 7.1
$G + \alpha$ 40 73.3	40 55.8	40 74.4	40 24.6	40 41.7
$\sin(G + \alpha)$ 9.81887	9.81613	9.81467	9.81114	9.81176
" 1.13900	1.14600	1.15200	1.16030	1.16740
$\cos(G + \alpha)$ 9.87632	9.87824	9.87747	9.88007	9.88000
$\sin(G + \alpha)$ 0.95737	0.96233	0.96737	0.97414	0.98136
$\tan \delta$ 9.17068	9.16171	9.15777	9.15111	9.15345
$+ + 27.80$	$+ 28.37$	$+ 28.93$	$+ 29.50$	$+ 30.09$
$\sin(G + \alpha) \delta + 1.34$	$+ 1.33$	$+ 1.32$	$+ 1.34$	$+ 1.36$
$\Delta^2 + 29.18$	$+ 29.70$	$+ 30.26$	$+ 30.84$	$+ 31.45$
$\Delta^2 + 1.14$	$+ 1.98$	$+ 2.07$	$+ 2.05$	$+ 2.09$
$48 + 10.36$	$+ 10.78$	$+ 10.97$	$+ 10.97$	$+ 11.15$

<u>Aug 11</u>	<u>Aug 21</u>	<u>Aug 27</u>	<u>Dec 19.5</u>
δ 8° 9.8	8° 16.6	8° 26.0	8° 38.3
α 14 4.4	14 1.7	15 23.6	16 12.3
G 26 40.0	26 17.0	27 47.6	27 12.0
$G + \alpha$ 40 44.4	40 18.7	42 11.2	43 24.3
$\sin(G + \alpha)$ 9.81467	9.81653	9.81840	9.82131
" 1.17450	1.18150	1.18840	1.19510
$\cos(G + \alpha)$ 9.87747	9.87824	9.87661	9.87442
$\sin(G + \alpha)$ 0.98917	0.99388	1.00488	1.01641
$\tan \delta$ 9.15670	9.16118	9.17103	9.18161
$+ + 30.67$	$+ 31.31$	$+ 31.93$	$+ 32.56$
$\sin(G + \alpha) \delta + 1.44$	$+ 1.47$	$+ 1.51$	$+ 1.56$
$\Delta^2 + 32.09$	$+ 32.76$	$+ 33.44$	$+ 34.12$
$\Delta^2 + 2.14$	$+ 2.22$	$+ 2.23$	$+ 2.27$
$17 + 11.32$	$+ 11.43$	$+ 11.61$	$+ 11.74$

Combining now the quantities Δ and δ , the corrections to be made for precession for the respective dates for which we have computed the co-ordinates, with α and δ , the next step requires that from the true positions thus obtained we interpolate in order to find the intermediate places for each day.

For making the interpolation to coordinates we use the formula

$$u_1 = u_0 + t \Delta'_{\frac{1}{2}} + \frac{t(t-1)}{2} \Delta''_{\frac{1}{2}} + \frac{t(t-1)(t-\frac{1}{2})}{1 \cdot 2 \cdot 3} \Delta'''_{\frac{1}{2}} + \dots$$

Putting

$$\Delta_1 = \frac{1}{4} \left[\Delta'_{i+\frac{1}{2}} + \frac{1}{4} \Delta'_{i+\frac{3}{2}} \right]$$

$$\Delta_2 = \frac{1}{32} \left[\Delta''_i + \frac{1}{4} \Delta''_1 \right]$$

Then the computation can be executed in

$$u_1 = u_0 + t \Delta_1 + \frac{t(t-1)}{2} \Delta_2 + \dots$$

The following are the results of the
 computations, and are to be used
 upon the accuracy of the work, and for convenience to use in
 reducing other observations to agree with the respective dates of the
 observations themselves, for the purpose of deriving the residuals,
 which give us the difference between the computed and the
 observed.

(ride next page)

[illegible]

160.	115	0	52	23.12	-	15.50	[- 0 14.57] ± [0.02]	-	1	7.55	+ [23.33]	-	0.49
1	125	0	52	12.85	-	12.85	[- 0 10.76] ± [0.03]	+			+ 32.57	+	[0.54]
135	0	51	53.05	11.79	-	11.79	[- 0 6.65] ± [0.03]	-	0	34.51	+ [32.87]	+	0.19
145	0	51	42.14	9.73	-	9.73	[- 0 2.50] ± [0.03]	-			+ 32.96	-	[0.26]
155	0	51	32.46	7.68	-	7.68	[+ 0 15.71] ± [0.01]	-	0	1.55	+ [32.61]	-	0.71
165	0	51	24.75	5.61	-	5.61	[- 0 5.62] ± [0.01]	-			+ 32.85	-	[0.11]
175	0	51	19.17	3.53	-	3.53	[+ 0 9.58] ± [0.05]	-	0	30.41	+ [31.70]	-	1.11
185	0	51	15.64	1.47	-	1.47	[- 0 13.40] ± [0.05]	-			+ 31.14	-	[1.30]
195	0	51	14.17	0.56	-	0.56	[- 0 17.28] ± [0.04]	-	1	17.2	+ [30.37]	-	1.57
205	0	51	14.73	2.59	-	2.59	[+ 0 20.09] ± [0.05]	-			+ 29.60	-	[1.50]
215	0	51	17.32	4.62	+	4.62	[+ 0 24.59] ± [0.05]	-	1	31.14	+ [28.50]	-	1.49
225	0	51	21.04	6.62	+	6.62	[+ 0 27.10] ± [0.05]	-			+ 28.11	-	[1.47]
235	0	51	25.56	8.60	+	8.60	[- 0 31.50] ± [0.05]	-	1	39.25	+ [27.30]	-	1.45
245	0	51	37.16	10.56	+	10.56	[- 0 34.56] ± [0.05]	-			+ 26.66	-	[1.46]
255	0	51	47.73	12.53	+	12.53	[+ 0 38.10] ± [0.05]	-	2	25.01	+ [25.05]	-	1.47
265	0	52	00.26	14.45	+	14.45	[+ 0 41.25] ± [0.05]	-			+ 25.10	-	[1.50]
275	0	52	14.71	16.35	+	16.35	[+ 0 44.30] ± [0.05]	-	2	51.10	+ [24.47]	-	1.54
285	0	52	31.05	18.22	+	18.22		-			+ 23.65	-	[1.55]
295	0	52	49.26	20.07	+	20.07		-	3	14.5			
305	0	53	9.33	21.59	+	21.59		-					
315	0	53	31.22	23.70	+	23.70		-					
325	0	53	54.02	25.48	+	25.48		-					
335	0	53	20.40	27.23	+	27.23		-					
345	0	54	47.63	29.97	+	29.97		-					
355	0	54	16.60	30.68	+	30.68		-					
365	0	54	47.20	32.37	+	32.37		-					
375	0	55	19.65	34.04	+	34.04		-					
385	0	55	53.70	35.65	+	35.65		-					
395	0	55	29.38	37.30	+	37.30		-					
405	0	55	6.65	38.99	+	38.99		-					
415	0	55	45.55	40.47	+	40.47		-					
425	0	55	26.02	42.03	+	42.03		-					
435	1	55	8.05	43.55	+	43.55		-					
445	1	55	51.60	45.05	+	45.05		-					
455	1	55	36.46	46.55	-	46.55		-					
465	1	55	51.42					-					

J' J' J'

1007 Oct 5.5	12°	-6 59.2	-[6' 50.3"]	- 27' 44.4	- [1.8.7]	-	[47.4]
108	12	- 4.0	-[7 1.6]	-	- 65.0	-	- 47.5
112	12	- 5.1	-[7 9.5]	-	- [41.2]	-	- [47.6]
125	11	- 11.5	-[7 14.9]	-	- [1.5.5]	-	- 47.7
135	11	- 14.0	-[7 17.1]	-	- 6.9	-	- [46.1]
145	11	- 15.5	-[7 16.3]	-	- 30.2	-	- 44.6
155	11	- 16.9	-[7 12.4]	-	- [52.5]	-	- [41.5]
165	11	- 17.3	-[7 5.9]	-	- 74.8	-	- 35.4
175	11	- 16.9	-[6 56.3]	-	- 27' 21.9	-	- [34.7]
185	11	- 15.5	-[6 44.6]	-	- 113.2	-	- 31.0
195	11	- 13.7	-[6 30.2]	-	- 25' 25.7	-	- [25.5]
205	11	- 11.1	-[6 14.1]	-	- 14.42	-	- 26.0
215	10	- 9.9	-[5 55.0]	-	- 4.5	-	- [22.0]
225	10	- 9.9	-[5 36.3]	-	- 20	-	- 19.5
235	10	- 9.4	-[5 14.5]	-	- 14.3	-	- [6.0]
245	10	- 4 58.1	-[4 5.5]	-	- 43	-	- 14.1
255	10	- 4 46.5	-[4 5.5]	-	- 17' 43	-	- [6.0]
265	10	- 4 34.7	-[4 5.5]	-	- 14.0	-	- 14.1
275	10	- 4 22.8	-[4 5.5]	-	- 14.0	-	-
285	10	- 4 10.6	-[4 5.5]	-	- 14.0	-	-
295	9	- 3 57.4	-[4 5.5]	-	- 14.0	-	-
305	9	- 3 44.4	-[4 5.5]	-	- 14.0	-	-
315	9	- 3 31.2	-[4 5.5]	-	- 14.0	-	-
325	9	- 3 18.0	-[4 5.5]	-	- 14.0	-	-
335	9	- 3 4.8	-[4 5.5]	-	- 14.0	-	-
345	9	- 3 0.6	-[4 5.5]	-	- 14.0	-	-
355	9	- 2 51.2	-[4 5.5]	-	- 14.0	-	-
365	9	- 2 41.4	-[4 5.5]	-	- 14.0	-	-
375	9	- 2 31.2	-[4 5.5]	-	- 14.0	-	-
385	9	- 2 20.3	-[4 5.5]	-	- 14.0	-	-
395	9	- 2 9.4	-[4 5.5]	-	- 14.0	-	-
405	9	- 1 58.1	-[4 5.5]	-	- 14.0	-	-
415	9	- 1 46.5	-[4 5.5]	-	- 14.0	-	-
425	9	- 1 34.7	-[4 5.5]	-	- 14.0	-	-
435	9	- 1 22.8	-[4 5.5]	-	- 14.0	-	-
445	9	- 1 10.6	-[4 5.5]	-	- 14.0	-	-
455	9	- 9 57.4	-[4 5.5]	-	- 14.0	-	-
465	9	- 9 44.4	-[4 5.5]	-	- 14.0	-	-
475	9	- 9 31.2	-[4 5.5]	-	- 14.0	-	-
485	9	- 9 18.0	-[4 5.5]	-	- 14.0	-	-
495	9	- 9 4.8	-[4 5.5]	-	- 14.0	-	-
505	9	- 8 51.2	-[4 5.5]	-	- 14.0	-	-
515	9	- 8 41.4	-[4 5.5]	-	- 14.0	-	-
525	9	- 8 31.2	-[4 5.5]	-	- 14.0	-	-
535	9	- 8 20.3	-[4 5.5]	-	- 14.0	-	-
545	9	- 8 9.4	-[4 5.5]	-	- 14.0	-	-
555	9	- 7 58.1	-[4 5.5]	-	- 14.0	-	-
565	9	- 7 46.5	-[4 5.5]	-	- 14.0	-	-
575	9	- 7 34.7	-[4 5.5]	-	- 14.0	-	-
585	9	- 7 22.8	-[4 5.5]	-	- 14.0	-	-
595	9	- 7 10.6	-[4 5.5]	-	- 14.0	-	-
605	9	- 6 57.4	-[4 5.5]	-	- 14.0	-	-
615	9	- 6 44.4	-[4 5.5]	-	- 14.0	-	-
625	9	- 6 31.2	-[4 5.5]	-	- 14.0	-	-
635	9	- 6 18.0	-[4 5.5]	-	- 14.0	-	-
645	9	- 6 4.8	-[4 5.5]	-	- 14.0	-	-
655	9	- 5 51.2	-[4 5.5]	-	- 14.0	-	-
665	9	- 5 41.4	-[4 5.5]	-	- 14.0	-	-
675	9	- 5 31.2	-[4 5.5]	-	- 14.0	-	-
685	9	- 5 20.3	-[4 5.5]	-	- 14.0	-	-
695	9	- 5 9.4	-[4 5.5]	-	- 14.0	-	-
705	9	- 4 58.1	-[4 5.5]	-	- 14.0	-	-
715	9	- 4 46.5	-[4 5.5]	-	- 14.0	-	-
725	9	- 4 34.7	-[4 5.5]	-	- 14.0	-	-
735	9	- 4 22.8	-[4 5.5]	-	- 14.0	-	-
745	9	- 4 10.6	-[4 5.5]	-	- 14.0	-	-
755	9	- 3 57.4	-[4 5.5]	-	- 14.0	-	-
765	9	- 3 44.4	-[4 5.5]	-	- 14.0	-	-
775	9	- 3 31.2	-[4 5.5]	-	- 14.0	-	-
785	9	- 3 18.0	-[4 5.5]	-	- 14.0	-	-
795	9	- 3 4.8	-[4 5.5]	-	- 14.0	-	-
805	9	- 2 51.2	-[4 5.5]	-	- 14.0	-	-
815	9	- 2 41.4	-[4 5.5]	-	- 14.0	-	-
825	9	- 2 31.2	-[4 5.5]	-	- 14.0	-	-
835	9	- 2 20.3	-[4 5.5]	-	- 14.0	-	-
845	9	- 2 9.4	-[4 5.5]	-	- 14.0	-	-
855	9	- 1 58.1	-[4 5.5]	-	- 14.0	-	-
865	9	- 1 46.5	-[4 5.5]	-	- 14.0	-	-
875	9	- 1 34.7	-[4 5.5]	-	- 14.0	-	-
885	9	- 1 22.8	-[4 5.5]	-	- 14.0	-	-
895	9	- 1 10.6	-[4 5.5]	-	- 14.0	-	-
905	9	- 9 57.4	-[4 5.5]	-	- 14.0	-	-
915	9	- 9 44.4	-[4 5.5]	-	- 14.0	-	-
925	9	- 9 31.2	-[4 5.5]	-	- 14.0	-	-
935	9	- 9 18.0	-[4 5.5]	-	- 14.0	-	-
945	9	- 9 4.8	-[4 5.5]	-	- 14.0	-	-
955	9	- 8 51.2	-[4 5.5]	-	- 14.0	-	-
965	9	- 8 41.4	-[4 5.5]	-	- 14.0	-	-
975	9	- 8 31.2	-[4 5.5]	-	- 14.0	-	-
985	9	- 8 20.3	-[4 5.5]	-	- 14.0	-	-
995	9	- 8 9.4	-[4 5.5]	-	- 14.0	-	-

1007 Oct 5.5

11.5	1	14	16.51	-57.41	+0.1	+11	1	14.7	
12.0				-57.47	+0.1	+12	1	14.7	-41.5
12.5	1	13	19.42	-57.40		+12	6	17.7	411.6
13.0				-57.47	+0.1				424.8
13.5	1	12	22.07	-57.23	+0.1	+11	57	11.4	426.6
14.0				-57.11	+0.1				428.1
14.5	1	11	24.96	-56.7	+0.1	+11	72	5.3	-42.6
15.0				-56.7	+0.1				-42.6
15.5	1	10	28.21	-56.52	+0.1	+11	44	11.5	-42.6
16.0				-56.52	+0.1				434.1
16.5	9		1.92	-56.37	+0.1	+11	37	37.5	-42.6
17.0				-56.37	+0.1				437.3
17.5	8		16.25	-56.2	+0.1	+11	30	22.6	-42.6
18.0				-56.2	+0.1				439.2
18.5	7		41.55	-56.0	+0.1	+11	23	7.1	-42.6
19.0				-56.0	+0.1				439.2
19.5	6		46.98	-55.83	+0.1	+11	15	42.3	-42.6
20.0				-55.83	+0.1				-42.6
20.5	5		53.58	-55.89	+0.1	+11	8	18.7	-42.6
21.0				-55.89	+0.1				-42.6
21.5	5		1.17	-55.7	+0.1	+11	1	17.1	-42.6
22.0				-55.7	+0.1				439.2
22.5	4		47.34	-55.77	+0.1	+10	54	13	-42.6
23.0				-55.77	+0.1				-42.6
23.5				-55.77	+0.1	+10	46	6.1	-42.6
24.0				-55.77	+0.1				427.7
24.5				-55.77	+0.1	+10	39	42.3	-42.6
25.0				-55.77	+0.1				-42.6
25.5	2		30.60	-48.55	+0.1	+10	32	38.4	-42.6
26.0				-48.55	+0.1				419.2
26.5	1		42.91	-47.01	+0.1	+10	25	27.3	-42.6
27.0				-47.01	+0.1				-42.6
27.5	0		11.67	-44.17	+0.1	+10	18	4.7	-42.6
28.0				-44.17	+0.1				407.7
28.5				-44.17	+0.1	+10	11	72.3	-42.6
29.0				-44.17	+0.1				419.2
29.5	59		28.24	-42.64	+0.1	+10		1.2	-42.6

27.0			-41.85 ^{+1.7}				
29.0	18	46.57	-41.06 ^{+1.7}	+	9	41.5	-40.1 ^{+1.7}
30.0			-40.27 ^{+1.6}				-39.6 ^{+1.6}
30.5	7	6.11	-38.48 ^{+1.6}	+	1	10.0	-37.3 ^{+1.6}
31.0			-38.63 ^{+1.6}				-37.8 ^{+1.6}
31.5	57	17.47	-37.76 ^{+1.6}	+	4	36	-36.1 ^{+1.6}
32.0			-37.0 ^{+1.6}				-35.2 ^{+1.6}
32.5	56	50.68	-36.06 ^{+1.6}	+	9	41.5	-35.7 ^{+1.6}
33.0			-35.11 ^{+1.6}				-34.2 ^{+1.6}
33.5	56	17.47	-34.21 ^{+1.6}	+	9	41.5	-33.7 ^{+1.6}
34.0			-33.31 ^{+1.6}				-32.2 ^{+1.6}
34.5	55	42.16	-32.40 ^{+1.6}	+	1	17	-31.6 ^{+1.6}
35.0			-31.50 ^{+1.6}				-30.1 ^{+1.6}
35.5	55	10.66	-30.57 ^{+1.6}	+	1	17	-29.7 ^{+1.6}
36.0			-29.64 ^{+1.6}				-28.2 ^{+1.6}
36.5	54	41.02	-28.70 ^{+1.6}	+	9	16	-28.2 ^{+1.6}
37.0			-27.76 ^{+1.6}				-26.7 ^{+1.6}
37.5	54	13.26	-26.80 ^{+1.6}	+	9	11	-26.2 ^{+1.6}
38.0			-25.84 ^{+1.6}				-24.7 ^{+1.6}
38.5	53	47.42	-24.88 ^{+1.6}	+	9	6	-23.3 ^{+1.6}
39.0			-23.91 ^{+1.6}				-22.4 ^{+1.6}
39.5	53	23.50	-22.93 ^{+1.6}	+	1	1	-21.2 ^{+1.6}
40.0			-21.94 ^{+1.6}				-20.6 ^{+1.6}
40.5	53	1.56	-20.93 ^{+1.6}	+	8	16	-20.0 ^{+1.6}
41.0			-19.93 ^{+1.6}				-18.4 ^{+1.6}
41.5	52	41.63	-18.92 ^{+1.6}	+	8	7	-17.5 ^{+1.6}
42.0			-17.91 ^{+1.6}				-16.2 ^{+1.6}
42.5	52	23.72	-16.90 ^{+1.6}	+	8	47	-15.6 ^{+1.6}
43.0			-15.89 ^{+1.6}				-14.0 ^{+1.6}
43.5	51	7.83	-14.87 ^{+1.6}	+	8	43	-13.7 ^{+1.6}
44.0			-13.81 ^{+1.6}				-12.2 ^{+1.6}
44.5	51	53.98	-12.82 ^{+1.6}	+	8	17	-11.0 ^{+1.6}
45.0			-11.79 ^{+1.6}				-9.4 ^{+1.6}
45.5	51	41.19	-10.76 ^{+1.6}	+	8	5	-9.1 ^{+1.6}
46.0			-9.73 ^{+1.6}				-8.0 ^{+1.6}
46.5	51	32.46	-8.70 ^{+1.6}	+	8	1	-7.6 ^{+1.6}
47.0			-7.68 ^{+1.6}				-6.2 ^{+1.6}
47.5	51	24.78	-6.73 ^{+1.6}	+	8	28	-4.9 ^{+1.6}

16.5	0	51	24.78	+80	25	49.9	
77.0			-5.61			-184.4	
17.5	51	19.17	-4.57	+8	25	44.5	-170.2
18.0						-171.7	
18.5	71	14.73	+1.57	+8	27	52.5	-165.2
19.0			-1.47				
19.5	51	14.17	-0.44	+8	20	14.1	-145.3
20.0			+0.56				
20.5	51	14.73	+1.57	+8	17	48.7	-138.6
21.0			+2.57				
21.5	51	17.32	+3.60	+8	15	36.8	-125.1
22.0			+4.62				
22.5	51	21.94	+5.62	+8	13	38.5	-111.6
23.0			+6.62				
23.5	51	28.56	+7.61	+8	11	53.6	-98.3
24.0			+8.60				
24.5	51	37.16	+9.58	+8	10	21.9	-85.1
25.0			+10.57				
25.5	51	47.73	+11.55	+8	9	24.4	-71.8
26.0			+12.53				
26.5	52	00.26	+13.47	+8	7	58.3	-58.6
27.0			+14.45				
27.5	52	14.71	+14.45		7	6.1	-45.6
28.0			+15.34				
28.5	52	31.11	+17.27	+8	6	27.0	-32.1
29.0			+18.21				
29.5	52	47.26	+19.14	+8	6	0.7	-19.7
30.0			+19.07				
30.5	53	77.2	+20.97	+8	-	47.2	-7.2
31.0			+21.89				
31.5	53	31.22	+21.77	+8	-	46.3	+5.3
32.0			+22.70				
32.5	53	54.42	+24.59	+8	-	7	+17.7
33.0			+25.48				
33.5	54	20.40	+26.35	+8	6	21.5	+2.7
34.0			+27.23				
34.5	54	47.63	+27.10	+8	-	7	+4.2
35.0			+28.97				

42.0	0	50	42.60	+17.10	+8°	0	42.60
5.0				+17.10			44.30
5.0			10.40	+17.10	+1	1	46.00
6.0				+17.10			47.70
6.0	55	42.17	+17.10	+17.10	+1	1	49.40
7.0				+17.10			51.10
7.0	56	12.65	+17.10	+17.10	+1	1	52.80
8.0				+17.10			54.50
8.0	56		+17.10	+17.10	+1	1	56.20
9.0				+17.10			57.90
9.0	55	22.00	+17.10	+17.10	+1	12	59.60
10.0				+17.10			61.30
10.0	55	0.00	+17.10	+17.10	+1	14	63.00
11.0				+17.10			64.70
11.0	53	0.00	+17.10	+17.10	+1	16	66.40
11.0				+17.10			68.10
12.0	53	20.00	+17.10	+17.10	+1	18	69.80
13.0				+17.10			71.50
13.0	1	0	+17.10	+17.10	+1	21	73.20
14.0				+17.10			74.90
14.0	0	51.00	+17.10	+17.10	+1	23	76.60
15.0				+17.10			78.30
15.0	12	00.00			26	10.6	

The co-ordinates for α and δ are computed for every third day, after January 1st 1885, and the following for making the interpolation to thirds is used:

$$u_t = u_0 + t \Delta'_{\frac{1}{2}} + \frac{t(t-1)}{1 \cdot 2} \Delta''_0 + \frac{t(t-1)}{1 \cdot 2 \cdot 3} \Delta'''_{\frac{1}{2}} + \dots \dots \dots]]$$

and the corresponding relations

$$\Delta' = \frac{1}{2} (\Delta'_{\frac{1}{2}} - \frac{1}{2} \Delta'_{\frac{1}{2}})$$

$$\Delta'' = \frac{1}{2} \Delta''_0$$

1883							
Jan. 25	18		+68.77	+68.77			
			+68.77				
	20		+62.77	+62.77			
			+62.77				
	21	14.17	+70.77	+70.77			
			+70.77				
	22	17.01	+70.77	+70.77			
			+71.82				
	23	6.52	+72.81	+72.81			
			+72.81				
	24	41.67	+73.77	+73.77			
			+73.77				
	26	3.44	+74.72	+74.72			
			+74.72				
	27	18.16	+75.70	+75.70			
			+75.68				
	28	33.84	+76.13	+76.13			
			+76.13				
	29	0.41	+77.02	+77.02			
			+77.47				
	31	7.89	+77.92	+77.92			
			+78.35				
	32	26.27	+78.80	+78.80			
			+79.12				
	33	17.49	+79.68	+79.68			
			+80.01				
	34	1.57	+80.52	+80.52			
			+80.96				
	36	26.03	+81.41	+81.41			
			+81.86				
	37	48.29					

						Δ'	Δ''	Δ'''
10.5	1	58	10,30	+71.71 ¹³	92.01 ¹³	+0.61		
				92.51	+72.51			
11.0	1	59	42.61	+92.61 ¹⁰	92.91 ¹⁰	+0.60		
				92.91	+72.91		+27.74	
"	2.5	2	1	12.72	12.72 ⁵	+0.60		-0.18
				+72.71	+72.71			
"	3.0	2	4	22.04	22.04 ⁵	+0.61	+2	+5.36
				24.11	+24.11			
"	4.0	4	4	22.15	24.41	+0.61		
				+24.70	+24.70		+28.10	-0.17
"	5.0	5	5	22.15	25.40			
				25.28	+25.18			
"	6.0	7	7	22.14	27.72	+0.61		+5.11
				+25.86	+25.86			
"	7.0	1	1	16.15	16.15 ¹⁰	+0.57		
				76.44	+76.44		+28.27	-0.24
"	8.0	10	10	42.44	16.71 ¹⁰	+0.61		
				16.77	+26.99			
"	9.0	12	12	22.43	27.17 ¹⁰	+0.61		+4.77
				27.6	+27.6			
"	10.0	13	13	22.29	27.37 ¹⁰	+0.64		
				28.09	+28.09		+28.24	-0.11
"	11.0	15	15	22.05	28.4 ¹⁰	+0.63		
				28.7	+28.59			
"	12.0	17	17	16.67	28.5 ¹⁰	+0.62		+4.25
				27.72	+27.72			
"	13.0	18	18	55.77	29.42 ¹⁰	+0.61		
				27.72	+27.63		+128.77	
"	14.0	21	21	35.51	27.72 ¹⁰	+0.61		
				100.13 ¹⁰	+100.13			
"	15.0	22	22	15.64				

1958		<u>S</u>			δ'	δ''	$1'$	$1''$	
Jan. 2.5	9	39	41.3			+6.5			
			+317.6 ⁺³²	5	17.6				
" 3.5		44	57.1 +33.0 ⁺³³			+6.5			
			+344.1 ⁺³³	5	22.2		+16	11.8	-4.1
" 4.5		50	23.0 +317.1 ⁺³³			+6.2			
			+350.1						
" 5.5		55	53.1 +333.0 ⁺³⁰			+6.0		+53.9	
			+336.0 ⁺³⁰	5	36.0				
" 6.5	10	1	29.1 +339.0 ⁺³⁰			+5.9			
			+342.1 ⁺³⁰		41.7		+17	5.7	4.4
" 7.5		7	11.2 +344.8 ⁺³⁰			+5.7			
			+347.6 ⁺³⁰		47.6				
" 8.5		12	58.8 +350.2 ⁺³⁰			+5.5		+44.5	
			+352.7 ⁺³⁰						
" 9.5		18	1.7 +357.0 ⁺³⁰			+5.4			
			+358.7 ⁺³⁰				+17	53.2	4.6
" 10.5		24	57.4 +361.1 ⁺³⁰			+5.2			
			+363.6 ⁺³⁰	6	3.6				
" 11.5		30	54.0 +366.0 ⁺³⁰			+5.0		+44.7	
			+368.4 ⁺³⁰	6	8.4				
" 12.5		37	2.4 +371.0 ⁺³⁰			+4.9			
			+372.7 ⁺³⁰	6	1.0		+18	40.1	-4.4
" 13.5		43	16.1 +375.8 ⁺³⁰			+4.7			
			+377.0 ⁺³⁰	6	5.0				
" 14.5		49	34.1 +380.2 ⁺³⁰			+4.5		+40.5	
			+382.4 ⁺³⁰	6	22.4				
" 15.5		55	56.5 +384.8 ⁺³⁰			+4.4			
			+387.2 ⁺³⁰	6	26.8		+19	18.8	
" 16.5	11	2	23.7 +387.1 ⁺³⁰			+4.2			
			+391.0 ⁺³⁰	6	31.0				
" 17.5	11	3	47			+4.0			

[illegible]

16, 16, 14	0	25	1	9	30, 34	2, 354	+11	24	11.1	0.781	1.13.6.1	207	16
" 16, 13	56	39	1	9	29, 71	2, 432	+11	21	9.6	0.67	10.0	Roma	17
" 17, 9	2	39	1	8	44, 65	2, 448	+11	24	1.9	0.17		St. ...	18
" 17, 1	24	41	1	8	44, 61	2, 383	+11	23	5.44	0.17		Algeria	19
" 17, 13	13	19	1	8	36, 14	2, 266	+11	23	0.5	0.732		Vienne	20
" 18, 12	7	34	1	7	42, 44	2, 973	+11	16	1.7	0.654	10.2	Roma, 181307	21
" 19, 8	58	6	1	6	43, 21	2, 390	+11	7	2.5	0.687	10.0	Calcutta	22
" 19, 9	16	48	1	6	42, 40	2, 332	+11	7	46.3	0.632		Calcutta	23
" 20, 9	31	41	1	5	59, 45	2, 259	+11	7	4.4	0.61	10	Yokohama	24
" 20, 13	31	14	1	5	52, 70	2, 328	+11	1	1.4	0.781	35	Paris	25
" 21, 9	7	13	1	5	7, 83	2, 329	+10	74	4.7	0.70	10	Yokohama	26
" 21, 11	53	27	1	5	3, 79	2, 892	+10	74	1.2	0.771	1		27
" 21, 8	11	28	1	4	54, 50	2, 460	+10	7	1.5	0.71	10.11	Calcutta	28
" 22, 8	53	25	1	4	16, 71	2, 343	+10	06	1.4	0.695	1		29
23, 8	27	14	1	3	29, 43	2, 357	+10	41	0.7	0.745		Calcutta	30

[illegible]

200	1	7	16	57	18.5	+5	17	50.6	0.706	Calicut	311	26
"	11	7	18	58	45.68	+5	16	30.9	0.701	Calicut	311	47
"	13	7	17	1	50	+8	20	58.1	0.700	Calicut	311	47
188												
Jan.	5	8	7	43	27.34	+9	26	1.7	0.622	Calicut	314	49
"	11	8	45	57	55.10	+10	31	16.3	0.612	Calicut	314	50
"	14	8	1	56	48.44	+10	49	51.2	0.637	Calicut	314	51
"	17	7	46	11	46.90	+10	54	17.6	0.727	Calicut	314	52
"	31	1	27	6	14.88	+12	46	2.6	0.691	Calicut	314	53
Feb.	1	5	41	2	59.00	+13	7	30.2	0.681	Calicut	314	54
"	6	8	7	51	36.42	+13	29	44.6	0.682	Calicut	314	55
"	3	7	18	10	45.56	+13	44	10.1	0.682	Calicut	314	56
"	14	7	42	18	52.50	+14	31	20.7	0.670	Calicut	314	57
Mar.	4	8	22	2	44.61	+17	22	43.6	0.670	Calicut	314	58

Comparison Stars.

The following catalogue selected for
 stars of comparison arranged in their order of right ascension &c.,
 are the stars which were used in making the observations for determining
 the positions for the year from October 11 1881 to March 22
 1883.

The following are the catalogues
 and references which have been consulted as Authorities for the
 positions: -

<u>Authorities</u>	<u>Abbreviations.</u>
Flamsteed's Catalogue	Flam.
Schlegel's Catalogue	Schleg.
Hass. Positiones Mediae + 15° - 15°	H.
Bonn Observations, Vol. II.	Bonn II.
Bessel's Catalogue	B & H.
Arnak's Catalogue	Arnak's
Garnett's Catalogue	G.

Struve's Cat. Gen.	5. & 6.
van der Waerden's Catalogue	1. & 2.
Glasgow Catalogue	3 & 4.
Drummond's Notes	15 & 16.
Astronomische Nachrichten	17 & 18.
Washington Observations	19. & 20.
Equatorial Comparisons	21 & 22.

The latter are positions of stars which have been differentiated from catalogue positions.

The weights to the catalogue positions have been given in accordance with the number of observations: 1 observation receiving the weight 1.

2 observations receiving the weight 2, &c.,

In case the number of observations in any unitary was not given the weight unity has been assigned.

The star places have been obtained from the mean of all the observations, although in some cases the observations were not all of the same quality. This I have done in order that the observations of the same star would be treated as of equal weight.

a greater degree of confidence

the reductions of the star places
 from the various epochs for the $\frac{1}{2}(t+t_0)$ epoch
 in the following manner, using the $\frac{1}{2}(t+t_0)$ epoch

$$\frac{d\alpha}{dt} = m + n \sin \alpha' \tan \delta'$$

$$\frac{d\delta}{dt} = n \cos \alpha'$$

where m and n are Starry's constants for the middle epoch, $\frac{1}{2}(t+t_0)$
 and α' and δ' are the right ascension and declination for the
 epoch $\frac{1}{2}(t+t_0)$

$$\alpha = \alpha_0 + [m''(t-t_0)] + [n''(t-t_0)\sin \alpha' \tan \delta']$$

$$\delta = \delta_0 + [n''(t-t_0)\cos \alpha']$$

For stars near the equator and the
 stellar variation, and for stars ranging so near the equator as
 those under consideration, the third term of the precession
 would have no influence during the period of time in-
 volved.

At the top of the coordinates
of the star places are given first the number of the star in
order of A.R. and then the magnitude in parentheses. The
published positions and data as taken from the *Edin. Circular*
is indicated by D.C. and the name of the issue. The positions
are for the epoch of the year in which they were used in
making the observations. The notes and references are given
in connection with each place.

Catalogue.

No. Mag. R.A. Decl. Eph. 1887.0.

1. (4) δ^h 50^m $20^s.06$; $+9^\circ 17' 40''.7$.

The star is W. 844, From
D. C. No. 309. Used at
Clinton, U.S. 1887, Nov 5.

2. (7.8) δ^h 50^m $40^s.13$; $+8^\circ 37' 2''.7$.

The position is $1/5$ [Sawyer
+ W. + R. + 2 bl.]. From
D. C. No. 309. Also given
in C. R. Used at Clinton,
U.S. Nov. 13; also at Rome.

3. (9.0) δ^h 51^m $18^s.24$; $+8^\circ 22' 18''.6$.

The place of this star is
somewhat uncertain. E. C.
It has been used in mak-
ing two observations of the
planet. 1887 Nov 22 52

Clinton, U.S. Position
given in B.C. No. 311.

4. (9.0) $0^h 51^m 19.42; +8^\circ 22' 1.9$.

This is evidently the same
star as No. 3, which was
used at Clinton. The
latter place has been
taken in the planet's
position corrected by -1.18
in R.A. and in Decl. by
 $+17''$. Star used at Rome
1887, Nov. 21, from B.C. No. 310.

5. (9.1) $0^h 54^m 50.15; +1^\circ 1' 4.7$.

The position is γ 516, and
was used at Berlin, 1887,
December 3, from A.N. No.
2973; also B.C. No. 310.
Washington Zone.

6. (1.2) $\delta^{\circ} 55^{\prime} 11.62, +9^{\circ} 4' 49.8$.

W. C. 219. From B. C. No. 311.

Used at Clinton, U.S.

1887, December 6.

7. (7.8) $\delta^{\circ} 55^{\prime} 49.07; +9^{\circ} 8' 9.4$.

The position is $\frac{1}{3}$ [W. C. 522.8

+ 52.25 + 52.25] Used

at Clinton, U.S. 1887, Dec.

6, from B. C. No. 309.

8. (7) $\delta^{\circ} 56^{\prime} 26.72, +8^{\circ} 12' 51.2$.

W. C. 229. Used at Clinton

U.S., 1887, December 9.

from B. C. No. 311.

9. (7) $\delta^{\circ} 56^{\prime} 43.64; +8^{\circ} 31' 25.4$.

The place is $\frac{1}{2}$ [Arg. VI + W. C. 530].

Used at Düsseldorf, 1887,

December 16, from B. C.

No. 309.

10. (94) $0^{\text{h}} 57^{\text{m}} 14.31$; $+9^{\circ} 45' 26''$.

The place is $\frac{1}{2}$ [Lat. No. 1925 +
+ A. A. No. 1800].

Used at Clinton, U.S., 1887,

November 2, from B. C. No.

307

11. (94) $0^{\text{h}} 57^{\text{m}} 21.61$; $+8^{\circ} 22' 29.6$. E. C.

Used at Clinton, U.S.,

1887, December 13. This

star was compared with

$\frac{1}{2}$ [R. 293 + Solj. 392], which

gives: -

(8.2) $1^{\text{h}} 7^{\text{m}} 47.41$; $+8^{\circ} 22' 31.8$.

from B. C. No. 311.

12. (7.5) $1^{\text{h}} 5^{\text{m}} 41.20$; $+1^{\circ} 1' 43.3$.

The place is $\frac{1}{3}$ [R. 510 + Solj. 366
+ B. C. 128].

Used at Clinton, U.S. 1887,

December 11. From B. C. No. 311.

13. (7) $i^2 = -1$; $i^4 = 1$

Pl. 272. Wood of *Flammula*.

1887, October 22, From B.C. No. 308.

14. (9) $1^{\text{h}} 1^{\text{m}} 44.96^{\text{s}}$; $+10^{\circ} 43' 48.1''$.

The position is $\frac{1}{2}$ [w. 1062 +

Gen. 50. Land in America.

1887, October 23, from B.C. No. 307.

15. (91 ⁴ 1 ¹² 2 ⁵ 28.29 ; + 10° 15' 17.9 .

The place is $5 \frac{1}{3}$ [R. u. f. 521 +

A. N. Vol. 51. 205 + Schj. 374.]

Used at Linseldorf, 1887.

44. 27. 7. - 1861

16. (9) $1^h 2^m 35.39^s$; $+ 10^{\circ} 17' 20.8''$.

This star was used at Düsseldorf.

1887, October 26, and the place

is R. 523, from B.C. No. 307.

The position of star No. 17 was

used instead as given - a b

16.

Clinton, U. S. This gave a correction to the planet's place of $+0.27$ in A.R. and -0.8 in Decl.

At Clinton for October 15 and 16, the positions of the planets depend on places as communicated by Professor Quellenman.

17. (12) $1^h 2^m 55.66$; $+1^\circ 17' 11.6$.

The place is $\frac{1}{3} [W. C. 589 + R. 523 + \frac{1}{3} (R. 521 + W. C. 586 + Schj. 3747)]$.

Used at Clinton U. S. Oct. 11, 1887. From B. C. No. 209.

18. (7) $1^h 5^m 51.51$; $+11^\circ 46' 48.7$.

W. C. 609. Used at Clinton, U. S.

October, 14, 1887. From B. C. No. 308.

19. (9) $1^h 5^m 52.17$; $+10^\circ 52' 5.1$.

The star is from the same source.

17.

Berlin, 1887, October 21, from
B.C. No. 307, also A.A. No. 2973.
The position of No. 20 is adopted
in the reduction of the
observations.

20, (8.4) $1^h \frac{1m}{5} 53.18$; $+10^\circ 52' 0''.8$, E.C.

Comparisons from $\frac{1}{2}$ EW. 119 +
2 B.A. 4], made
at Berlin, at which place
for the comparison star
(1.0) $1^h 10^m 12.19$; $+10^\circ 52' 14''.2$.
This place has been adopted
for observations depending on
this star which were made
at Berlin, from B.C. No. 308.

21, (9) $1^h 6^m 49.36$; $+11^\circ 23' 31''.7$.

W. C. 613, used at Paris, 1887,
October 16, from B.C. No. 307.
The position No. 22 as given at
Vienna has been adopted.

22. (8.9) $1^h 6^m 49.69^s$; $+11^\circ 23' 32.1''$.

W. C. 613, used at L. 1887.

1887, Oct. 17. From B.C. No.

303. This place has been

used for the Paris obser-

vation and also for that

of Algiers. For Rome it

is given as

(8.9) $1^h 6^m 49.69^s$; $+11^\circ 23' 32.1''$ being

$\frac{1}{2} [w. 62 + L. 665]$, from B.C. No. 307, 1887, Oct. 16.

23. (8.9) $1^h 6^m 49.79^s$; $+11^\circ 23' 33.2''$.

Same obs. as above W. 62.

24. (8.3) $1^h 7^m 49.61^s$; $+11^\circ 8' 58.1''$.

W. C. 615. Place used at

Clinton, U.S. 1887, Oct. 19.

From B.C. No. 306.

25. (8.3) $1^h 7^m 11.99$; $+11^\circ 4' 58.1''$.

G. 616, Used at Berlin,
1887, October 20, From
A. N. No. 2927; also B. C. No. 307.

26. (7.8) $1^h 7^m 11.99$ $+11^\circ 4' 58.1''$.

Same star and place as the
preceding. Used at Berlin
Nov. 1887, October 19, From
B. C. No. 301.

27. (8.9) $1^h 7^m 12.01$; $+11^\circ 4' 58.0''$

This position is $\frac{1}{3}$ [w. 66 + w. 6. 616
+ Lam. 167].

Used at Toulouse, 1887, Oct. 20,
From B. C. No. 308.

28. (10) $1^h 7^m 32.27$; $+11^\circ 31' 54.3''$.

Lam. 169. Used at Berlin,
1887, October 16, From B. C. No.
307; also A. N. No. 2973.

29. (10) $1^h 10^m 16.81$; $+11^\circ 51' 27.3$, E.C. 1865.

Determined at Clinton U.S.

and used at Clinton, 1887.

Oct. 13, from B.C. No. 307.

30. (9) $1^h 11^m 39.13$; $+11^\circ 42' 3.6$, E.C.

Comparison with W.C. 610. (7)

$\alpha = 1^h 6^m 2.06$

$\delta = +11^\circ 41' 0.6$.

Used at Paris 1887, October 14,

from B.C. No. 307.

31. (10) $1^h 11^m 37.17$; $+11^\circ 42' 4.0$

W. 179. Used at Rome, 1881.

October 13, from B.C. No. 306.

32. (8) $1^h 13^m 44.99$; $+11^\circ 33' 7.3$, W. 179.

This star was used in mak-

ing the observations of the

planet Mars adopted the

position of α for this place.

as given by the French B. G.
No. 308.

34. (8) $1^h 13^m 45.06$; $+11^\circ 15' 7.3$, 10.174.

(This place has also been
used for the observation of
the planet *Venus* at Algiers,
1887, Oct. 15) Used at Hün-
delsberg, 1887, Oct. 12, from B. G.
No. 307.

35. (5) $1^h 13^m 57.92$; $+11^\circ 35' 34.7$.

10.184, Used at Algiers,
1887, Oct. 14, from B. G. No. 308.

36. (7) $1^h 15^m 59.45$; $+12^\circ 0' 45.2$.

The place is $\frac{1}{2}$ [Ann. 191 H.N.
Vol. 72, 317]. Used at Vienna,
1887, Oct. 13, from B. G. No. 306.

37. (10) $1^h 16^m 15.34$; $+12^\circ 4' 3.7$, Jan. 192.

Used at Clinton, U.S. 1887, Oct. 11.
from B. G. No. 307.

38. (9.5) $1^{\circ} 15' 11''$; $+ 11^{\circ} 44' 12''$, E.C.

Used at Düsseldorf, 1887, Oct. 13.
From B.C. No. 306.

The following stars are for the Epoch
1888.1

39. (9.5) $1^{\circ} 20' 25.03''$; $+ 9^{\circ} 57' 40.1''$, W. 304.

Used at Clinton, U.S., 1888,
January 5, From B.C. No. 312.

40. (9.5) $1^{\circ} 31' 6.31''$; $+ 10^{\circ} 33' 8.1''$, E.C.

Observed at Clinton, U.S.,
Comparison with $\alpha_{12} 11.64 + 12.03$,
and used in observing planet,
1888, January 11, From B.C. No. 314

41. (11.5) $1^{\circ} 37' 36.01''$; $+ 10^{\circ} 50' 21.7''$, E.C.

The comparison stars, $\alpha_{12} 11.64 + 12.03$,
 $\alpha_{12} 11.758 + 12.071$, observed at
Clinton, U.S., 1888, Jan. 14,
and used in observing planet.

42. (9.5) $1^{\circ} 36' 57.87''$; $+10^{\circ} 57' 50.2''$, E.C.

Comparison with Art. Vol. 31, 257.

(9) $\alpha = 1^{\circ} 35' 41.14''$,

$\delta = +11^{\circ} 3' 50.8''$.

Used at Clinton, U.S., January

15, from B.C. No. 314.

43. (9.4) $1^{\circ} 58' 8.23''$; $+12^{\circ} 45' 36.8''$, E.C.

Comparison with $\frac{1}{2}$ [10.1029 +

+2 km. 281 + 2 h. 456], which

gives $1^{\circ} 59' 44.32''$; $+12^{\circ} 48' 31''$.

Retained and used at Clinton.

U.S., 1888, January 31, from B.C. 314.

44. (9.0) $2^{\circ} 3' 52.75''$; $+13^{\circ} 29' 37.4''$.

Place from Art. No. 2325, Used at

Clinton, U.S., 1888, February 6,

from B.C. No. 314.

45. (8.5) 2^h 4^m 47.78 ; $+13^\circ 4'$ 27.5 .

This place is the mean of W. 21;
 Sturges C. G. 200; P. 288; R. 1087;
 Pola. & N. 2325, used at Clinton,
 U.S., 1888, Feb. 3, from B. G. No. 314.

46. (8.8) 2^h 11^m 41.81 ; $+13^\circ 43'$ 44.9 , E. G.

Comparison with W. 1003, determined
 and used at Clinton, U.S., 1888,
 Feb. 3, from B. G. No. 314.

47. (8.7) 1^h 17^m 18.40 ; $+14^\circ 20'$ 21.0 , E. G.

Comparison with W. 262, deter-
 mined at Clinton, U.S., 1888,
 February 13, from B. G. No. 314.

48. (10) 3^h 14^m 31.48 ; $+17^\circ 24'$ 19.7

Alt. No. 2174, used at Clinton,
 U.S., 1888, March 4, from B. G.
 No. 314.

With the preceding data we will now compute the residuals, Δa and Δd , in the following

$$\begin{aligned} C &= \text{computed value} \\ O &= \text{observed value} \end{aligned} \left\{ \begin{array}{l} a \text{ and } d. \end{array} \right.$$

1987										Δx	Δy
Oct. 11,5000	6x	1 ²	14	16.7	68	+12	6	15.5	-57.49	-42.18	
Red. for +0.0502				-2.8				-21.2		1.75759 _u	
Oct. 11,5502	6x	1	14	14.0	68	+12	5	54.3	8.70070	6hinter.	
" " 0x	1	14	19.7	08	+12	5	46.8		2.62	11 _u	
0-6				+0.5				0.6			
Oct. 12,5000	6x	1	13	17.42	68	+11	57	11.4	-57.40	-42.62	
Red. for +0.0877				-5.0				-74		1.75841 _u	
Oct. 12,5877	6x	1	13	14.07	68	+11	58	8.0	8.74000	Stämpfing	
" " 0x	1	13	14.4	08	+11	51	33.4		2.6296 _u		
0-6				+0.6				-0.6			
Oct. 13,5000	6x	1	12	22.07	68	+11	52	3.3	-57.21	-42.00	
Red. for -0.1403				+3.08				+60.3		1.75747 _u	
Oct. 13,3597	6x	1	12	20.10	68	+11	53	3.6	8.64200 _u	1.0000	
" " 0x	1	12	20.50	08	+11	53	3.6		2.63347 _u		
0-6				-0.10				0.0			
Oct. 13,5000	6x	1	12	22.07	68	+11	52	3.3	-57.23	-429.8	
Red. for -0.0442				+2.77				+17.0		1.75767 _u	
Oct. 13,4358	6x	1	12	24.60	68	+11	52	22.3	8.64542 _u	Büschhof.	
" " 0x	1	12	24.80	08	+11	52	26.6		2.63327 _u		
0-6				+0.10				+4.3			
Oct. 13,5000	6x	1	12	22.07	68	+11	52	3.3	-57.23	-429.8	
Red. for +0.0201				-1.15				-8.6		1.75762 _u	
Oct. 13,5201	6x	1	12	20.92	68	+11	51	54.7	8.30320	Reine.	
" " 0x	1	12	20.60	08	+11	51	50.6		2.63327 _u		
0-6				-0.24				-4.1			
Oct. 13,5000	6x	1	12	22.07	68	+11	52	3.3	-57.21	-429.5	
Red. for +0.0898				-5.14				-38.6		1.75747 _u	Blinter
Oct. 13,5898	6x	1	12	16.93	68	+11	51	24.7	8.95328	Hg. cor.	
" " 0x	1	12	16.96	08	+11	51	27.0		2.63296 _u		
0-6				+0.03				+2.3			

									A_n	A_S
Oct. 14,5000	6x	1 ⁴ 11	24.76	68	+11	44	51.8	-56.95	-432.7	
Ref. for -0.1408			+3.07				+60.9			1.75549 _n
Oct. 14,5592	6x	1 11	27.98	68	+11	45	52.7			2.14860 _n Algier.
" " 0x	1 11	28.88	68	+11	45	56.1				2.63619 _n
0-6			0.10				-3.4			

Oct. 14,5000	6x	1 11	24.76	6x	+11	44	51.8	-56.95	-432.7	
Ref. for -0.1238			+7.05				+53.6			1.75549 _n
Oct. 14,3762	6x	1 11	32.01	68	+11	45	45.4			3.09172 _n Algier.
" " 0x	1 11	32.62	68	+11	45	50.8				2.63619 _n
0-6			+0.61				+5.4			

Oct. 14,5000	6x	1 11	24.76	6x	+11	44	51.8	-56.93	-432.8	
Ref. for -0.092			+0.57				+40			1.75534 _n
Oct. 14,4908	6x	1 11	27.48	68	+11	44	55.8			7.96379 _n Paris.
" " 0x	1 11	27.65	68	+11	44	57.4				2.63629 _n
0-6			+0.17				+1.6			

Oct. 14,5000	6x	1 11	24.76	68	+11	44	51.8	-56.93	-432.8	
Ref. for -0.022			+0.15				+1.0			1.7554 _n
Oct. 14,4978	6x	1 11	27.09	68	+11	44	52.8			7.34242 _n Paris.
" " 0x	1 11	27.24	68	+11	44	54.5				2.63629 _n
0-6			+0.15				+1.7			

Oct. 14,5000	6x	1 11	24.76	68	+11	44	51.8	-56.91	-432.7	
Ref. +0.614			-3.47				-26.6			1.75519 _n
Oct. 14,5614	6x	1 11	21.47	68	+11	44	25.2			8.78817 Clinton.
" " 0x	1 11	21.77	68	+11	44	31.4				2.63619 _n
0-6			+0.30				+6.2			

Oct. 15,5000	6x	1 10	28.21	68	+11	37	37.8	-56.55	-434.8	
Ref. for -0.1446			+8.15				+62.2			1.7524 _n
Oct. 15,3554	6x	1 10	36.57	68	+11	38	40.7			9.16017 _n Algier.
" " 0x	1 10	36.45	68	+11	38	42.4				2.63829 _n
0-6			+0.02				+1.7			

Oct.	15,5000	6a	1	10	28.21	68	+11	37	37.8	-56,55 - 434.8
Red. for	-1,127				27.11				+4.6	1,752.43
Oct.	15,3463	6a	1	10	28.02	68	+11	38	22.4	2,011,574 Alger.
"	"	0a	1	10	28.02	68	+11	38	26.6	2,638,29-
		0-6			+0.04				+4.2	

Oct.	15,5000	6a	1	10	28.21	68	+11	37	37.8	-56,54 - 434.8
Red. for	-0,107				28.11				+4.7	1,752.26
Oct.	15,4893	6a	1	10	28.22	68	+11	37	42.7	8,029,384 Paris.
"	"	0a	1	10	28.24	68	+11	37	44.1	2,638,29-
		0-6			+0.12				+1.6	

Oct.	16,5000	6a	1	7	31.77	68	+11	30	22.0	-56,02 - 436.4
Red. for	-1,083				30.67				+47.5	1,748,344
Oct.	16,3917	6a	1	7	31.00	68	+11	31	9.3	9,034,634 Paris.
"	"	0a	1	7	31.17	68	+11	31	9.9	2 - 9,000
		0-6			+0.17				+0.6	

Oct.	16,5000	6a	1	7	31.75	68	+11	30	22.0	-55,99 - 436.4
Red. for	+0,408				-2.25				-12.3	1,748,114 Berlin.
Oct.	16,5408	6a	1	7	29.65	68	+11	30	4.2	2,611,114 Paris.
"	"	0a	1	7	29.57	68	+11	29	57.4	2,637,884
		0-6			+0.70				-6.8	

Oct.	17,5000	6a	1	8	36.25	68	+11	23	5.1	-55,38 - 437.1
Red. for	-1,172				+7.00				+60.0	1,742,254
Oct.	17,3628	6a	1	8	42.85	68	+11	24	.1	2,117,554 Alger.
"	"	0a	1	8	44.36	68	+11	24	6.1	2,640,584
		0-6			+0.51				+1.0	

Oct.	17,5000	6a	1	8	36.25	68	+11	23	5.1	2,117,554
Red. for	-0,1219				+6.60				+52.1	1,743,354
Oct.	17,3781	6a	1	8	42.85	68	+11	23	57.2	2,640,584
"	"	0a	1	8	43.6	68	+11	23	58.5	2,640,584
		0-6			+0.71				+1.0	

										1.	1.
Oct.	17.5000	6x	1	8	36.25	68	+11	23	5.1	-55.35	-437.1
Red. per	-0.044				+0.01				+0.1		1.74312
Oct.	17.4999	6x	1	8	36.26	68	+11	23	5.2		6.00000 Vienna.
"	"	0x	1	8	36.33	08	+11	23	6.1		2.64058
"	"	0-6			+0.07				+1		
Oct.	18.5000	6x	1	8	41.33	68	+11	15	47.8	-54.66	-437.1
Red. per	0.350				+1.91				+12.3		1.73767
Oct.	18.4650	6x	1	8	43.24	68	+11	16	3.1		8.54407 Rome.
"	"	0x	1	8	43.04	08	+11	16	6.4		2.64058
"	"	0-6			-0.20				+3.3		
Oct.	19.5000	6x	1	6	46.98	68	+11	8	30.9	-53.75	-436.3
	+0.775				-4.17				-33.8		1.73038
Oct.	19.5775	6x	1	6	42.81	68	+11	7	57.1		8.88930 Canton, U.S.
"	"	0x	1	6	42.76	08	+11	7	57.5		2.63978
"	"	0-6			+0.15				+0.4		
Oct.	19.5000	6x	1	6	46.98	68	+11	8	30.9	-53.75	-436.3
Red. per	+0.904				-4.86				-39.4		1.73038
Oct.	19.404	6x	1	6	42.12	68	+11	7	51.7		8.1617 Canton, U.S.
"	"	0x	1	6	42.18	08	+11	7	51.3		2.63979
"	"	0-6			+0.06				-0.2		
Oct.	20.5000	6x	1	5	53.58	68	+11	1	15.1	-52.96	-434.9
Red. per	-0.1127				+5.97				+49.0		1.72395
Oct.	20.3873	6x	1	5	59.61	68	+11	2	4.1		9.05192 Toulouse.
"	"	0x	1	5	59.26	08	+11	2	9.4		2.63837
"	"	0-6			-0.35				+5.3		
Oct.	20.5000	6x	1	5	53.58	68	+11	1	15.1	-52.88	-434.8
Red. per	+0.0205				-1.08				-8.2		1.72329
Oct.	20.5205	6x	1	5	52.50	68	+11	1	6.2		8.31175 Berlin
"	"	0x	1	5	52.42	08	+11	1	6.6		2.63829
"	"	0-6			-0.08				+0.4		

As

Oct. 21,5000 6a 1 5 1.19 68 +1 54 1.3 -51.92 -432.3

Red. for - .1297 +6.21 +26.1 1.21 3a

Oct. 21,3703 6a 1 5 7.92 68 +10 54 57.5 7.11 14a " " "

" " 0a 1 5 7.61 08 +10 54 59.7 2.0 17a

" " 0-6 -0.31 +2.2

Oct. 21,5000 6a 1 5 1.19 68 +10 54 1.3 -51.89 -432.3

Red. for - .0474 +2.46 +20.5 1.71 508a

Oct. 21,4526 6a 1 5 3.65 68 +10 54 21.8 8.67 578a Berlin.

" " 0a 1 5 3.87 08 +10 54 24.2 2.60 579a

" " 0-6 +0.22 +2.4

Oct. 21,5000 6a 1 5 1.19 68 +10 54 1.3 -51.16 437.4

Red. for + .0451 -2.34 -19.5 1.71 483a

Oct. 21,5421 6a 1 4 58.85 68 +10 53 41.8 8.65 410 Glinen.

" " 0a 1 4 59.20 58 +10 53 43.6 2.63 549a

" " 0-6 +6.35 +1.8

Oct. 22,5000 6a 1 4 9.84 68 +10 46 50.2 -50.84 -411.6

Red. for - .1393 +7.95 +58.5 1.26 641a

Oct. 22,3607 6a 1 4 16.79 68 +10 46 48.7 9.13 345a Toulouse.

" " 0a 1 4 16.49 08 +10 46 41.4 2.63 306a

" " 0-6 -0.30 -7.3

Oct. 23,5000 6a 1 3 17.61 68 +10 31 42.1 -49.74 -426.1

Red. for .1920 +7.75 +1 21.8 1.69 671a

Oct. 23,3080 6a 1 3 27.16 68 +10 41 4.1 9.28 330a Vienna.

" " 0a 1 3 29.20 08 +10 41 6.6 2.62 951a

" " +1.04 +2.5

Oct. 26,0000 6a 1 0 56.33 68 +10 18 42.7 -45.70 -411.2

Red. for - .1373 +6.28 +56.5 1.66 020a

Oct. 26,1627 6a 1 0 2.86 68 +10 17 42.2 9.10 707a " "

" " a 1 1 2.66 08 +10 19 45.4 2.61 405a

" " -0.20 +1.2

Oct. 27,5000 6x 1 5 11.47 65 + 10 11 57.8 -44.27 -40.0
 Rel. for +1.40 11.71 +54.1 12.0612
 Oct. 27,3660 6x 1 0 17.00 65 + 10 12 52.0 1,127100 Clinton.
 " " 0x 1 6 18.90 65 + 10 12 49.6 1,607460
 " " 0-6 18.11 -2.4

Oct. 31,5000 6x 0 5 22.47 65 + 9 45 57.6 -37.65 -373.4
 Rel. for +1.979 -5.12 -50.7 1,575760
 Oct. 31,6359 6x 0 7 22.37 65 + 9 45 6.9 1,177120 Clinton.
 " " 0x 0 7 22.78 65 + 9 45 2.7 2,572170
 " " 0-6 22.41 +9.8

Nov. 2,5000 6x 0 6 47 65 + 9 33 47.1 -34.12 -355.4
 Rel. for +1.4971 -2.31 -34.5 1,533010
 Nov. 2,5971 6x 0 6 12.16 65 + 9 33 12.6 3,98722 Clinton.
 " " 0x 0 6 11.58 65 + 9 33 15.0 2,550720
 " " 0-6 11.42 +2.7

Nov. 5,5000 6x 0 5 41.02 65 + 9 16 43.3 -28.64 -24
 Rel. for +1.0303 -0.87 -9.7 1,410170
 Nov. 5,5303 6x 0 5 40.12 65 + 9 16 33.4 6,48144 Clinton.
 " " 0x 0 5 40.00 65 + 9 16 37.4 2,512420
 " " 0-6 40.15 +4.0

Nov. 6,5000 6x 0 5 13.26 65 + 9 11 23.0 -26.79 -324.5
 Rel. for +1.0830 -2.22 -26.1 1,417770
 Nov. 6,5830 6x 0 5 11.04 65 + 9 10 56.9 8,91908 Clinton.
 " " 0x 0 5 11.27 65 + 9 10 58.2 2,497340
 " " 0-6 11.20 +1.3

Nov. 13,5000 6x 0 5 11.78 65 + 9 39 24.7 -12.57 -2120
 " " 11.80 +2.07 +6.7 1,112140
 Nov. 13,34 0x 0 5 56.03 65 13 40 +1.4 712140 Clinton.
 " " 0x 0 5 56.17 65 13 40 2.8 2,365470
 " " 0-6 56.16 +1.0

								Δ_2	Δ_8
Nov.	15,3992	6x	51	53.78	68 + 8	46	24.7	-12.92	-231.6
Red. per	-1.008			+1.008			+2.3	1.1116	
Nov.	15,3992	6x	51	55.28	68 + 8	39	48.0	9.00346	Rome.
"	"	0x	51	55.55	08 + 8	39	47.6	2.36474	
"	"	0-6		+0.27			-0.4		
Nov.	16,5000	6x	0	51	24.78	68 + 8	28	49.7	-6.70 -143.1
Red. per	-1.1521			+1.02			+29.4	6.82607	
Nov.	16,3477	6x	0	51	25.00	68 + 8	27	17.7	2.18312
"	"	0x	0	51	26.12	08 + 8	27	18.6	2.28970
"	"	0-6		+0.42			-6.7		
Nov.	18,5000	6x	0	51	15.64	68 + 8	22	52.5	-2.50 -16.5
Red.	+0.064			-0.02			-11	6.1774	
Nov.	18,5064	6x	0	51	15.62	68 + 8	22	51.4	7.80613 Clinton.
"	"	0x	0	51	15.14	08 + 8	22	57.2	2.21801
"	"	0-6		-0.48			+78		
Nov.	18,5000	6x	0	51	15.64	68 + 8	22	52.5	-2.55 -16.5
Red. per	+0.078			-0.15			-9.5	6.46654	
Nov.	18,5578	6x	0	51	15.49	68 + 8	22	43.0	8.76173 Clinton.
"	"	0x	0	51	15.07	08 + 8	22	48.6	2.21748
"	"	0-6		-0.42			+56		
Nov.	21,5000	6x	0	51	17.32	68 + 8	15	36.8	+3.40 -126.3
Red. per	1.2458			-1.01			+7.4	6.55148	
Nov.	21,2042	6x	0	51	16.31	68 + 8	16	14.2	2.47100 Rome.
"	"	0x	0	51	17.06	08 + 8	15	55.8	2.10140
"	"	0-6		+6.75			-18.4		
"	"			-0.43			-5.6		
Dec.	3,5000	6x	0	54	10.4	68 + 8	6	21.7	+6.1 +28.0
Red. per	-1.2565			-6.71			-7.2	1.41714	
Dec.	3,2435	6x	0	54	13.70	68 + 8	6	14.3	2.409074 Berlin.
"	"	0x	0	54	13.87	08 + 8	6	15.0	1.44716
"	"	0-6		+0.17			+0.7		

Nov, 6,5000 ba 0 55 47.29 68 + 8 8' 45.3
 Red. for +.0000 +31.4 +6.6
 Dec, 6,6000 ba 0 55 50.53 68 + 8 8 51.9
 " 02 0 55 50.61 08 + 8 8 54.1
 0-6 +0.08 +2.2

1- 1-
 +32.44 +66.2
 1,518.08
 9,000.00 Clinton
 1,820.86

Dec, 9,5000 ba 0 57 29.38 68 + 8 12 54.2
 Red. for -.0045 -0.16 -0.5
 Dec, 9,4955 ba 0 57 29.22 68 + 8 12 53.7
 " 02 0 57 29.28 08 + 8 12 54.3
 0-6 +0.06 +0.6

+36.47 +100.0
 1,562.17
 7,653.21 Clinton
 2,000.00

Dec, 13,5000 ba 0 0 8.05 68 + 8 21 2.6
 Red. for -.0057 -0.24 -0.8
 Dec, 13,4943 ba 1 0 7.81 68 + 8 21 1.8
 " 02 1 0 8.01 08 + 8 21 1.7
 0-6 +0.20 -0.1

+42.79 +143.6
 1,631.34
 7,755.87 Clinton
 2,157.15

1885,

Jan, 5,5000 ba 1 22 27.00 68 + 9 56 53.1
 Red. for +.0383 +2.70 +12.8
 Jan, 5,5383 ba 1 22 27.70 68 + 9 56 5.9
 " 02 1 22 27.85 08 + 9 56 4.6
 0-6 +0.25 -1.3

+7,776 +2,111
 1,847.33
 8,583.20 Clinton
 2,522.57

Jan, 11,5000 ba 1 29 50.42 68 + 10 30 54.0
 Red. for +.0644 +4.46 +23.6
 Jan, 11,5644 ba 1 29 55.38 68 + 10 31 17.6
 " 1 29 55.26 08 + 10 31 11.1
 0-6 -0.12 +1.5

+77.04 +366.1
 1,586.72
 8,808.89 Clinton
 2,761.10

Jan, 14,5000 ba 1 33 45.49 68 + 10 45 34.1
 Red. for +.0335 +2.67 +12.7
 Jan, 14,5335 ba 1 33 48.16 68 + 10 45 46.8
 " 02 1 33 48.56 08 + 10 45 50.9
 0-6 +0.40 +7.1

+79.65 +350.3
 1,901.14
 8,827.44 Clinton
 2,730.18

Jan. 15,500.0 6x 1 35 55.7 68 + 10 54 54.5 1,10,1 15,7.1
 Feb. - 1,100.0 - 13.71 - 1 21.1 1,10,644
 Jan. 15,268.0 6x 1 34 46.86 68 + 10 54 27.4 2,36549- Vienna.
 " " 0x 1 34 46.96 08 + 10 54 22.2 2,58478
 0-6 + 0.10 - 4.2

Jan. 31,500.0 6x 1 7 10.30 68 + 12 45 50.2 +92.02 +403.3
 Red. for +.0511 + 4.70 + 15.6 1,46
 Jan. 31,551.1 6x 1 7 10.3 68 + 12 45 10.3 2,58478
 " " 0x 1 58 15.04 08 + 12 46 12.0 2,60563
 0-6 - 0.04 + 1.2

Feb. 3,500.0 6x 2 2 49.04 68 + 13 7 35.2 +93.82 +437.2
 Red. for +.0346 + 3.25 + 15.1 1,97230
 Feb. 3,534.6 6x 2 2 52.29 68 + 13 7 50.3 3,708 Clinton.
 " " 0x 2 2 52.15 08 + 13 7 52.5 2,6443
 0-6 - 0.14 + 1.2

Feb. 6,500.0 6x 2 7 33.14 68 + 13 29 32.7 +95.58 +441.3
 Red. for +.0311 + 3.43 + 15.8 1,98037
 Feb. 6,535.9 6x 2 7 36.5 68 + 13 29 48.5 8,55509 Clinton.
 " " 0x 2 7 36.57 08 + 13 29 46.8 2,64473
 0-6 0.00 - 1.7

Feb. 8,500.0 6x 2 10 45.44 68 + 13 44 15.7 +96.73 +442.4
 Red. for +.0311 + 3.43 + 15.7 1,98556
 Feb. 8,535.5 6x 2 10 48.87 68 + 13 44 31.4 8,55023 Clinton.
 " " 0x 2 10 47.01 08 + 13 44 32.3 2,64582
 0-6 + 0.14 + 0.9

Feb. 13,500.0 6x 2 18 55.79 68 + 14 28 17.2 +1,142 +442.4
 Red. for +.0181 + 1.80 + 8.0 1,14247
 Feb. 13,518.1 6x 2 18 57.59 68 + 14 28 25.2 8,25768 Clinton.
 " " 0x 2 18 57.64 08 + 14 28 22.4 2,44546
 0-6 + 0.05 - 2.8

1.1	17.020	-0.20	1	-0.20	1	1.1.1.1.1.1.
	17.100	-0.25	1	-0.25	1	1.1.1.1.1.1.
	17.180	-0.30	1	-0.30	1	1.1.1.1.1.1.
	17.260	-0.35	1	-0.35	1	1.1.1.1.1.1.
	17.340	-0.40	1	-0.40	1	1.1.1.1.1.1.
	17.420	-0.45	1	-0.45	1	1.1.1.1.1.1.
	17.500	-0.50	1	-0.50	1	1.1.1.1.1.1.
	17.580	-0.55	1	-0.55	1	1.1.1.1.1.1.
	17.660	-0.60	1	-0.60	1	1.1.1.1.1.1.
	17.740	-0.65	1	-0.65	1	1.1.1.1.1.1.
	17.820	-0.70	1	-0.70	1	1.1.1.1.1.1.
	17.900	-0.75	1	-0.75	1	1.1.1.1.1.1.
	17.980	-0.80	1	-0.80	1	1.1.1.1.1.1.
	18.060	-0.85	1	-0.85	1	1.1.1.1.1.1.
	18.140	-0.90	1	-0.90	1	1.1.1.1.1.1.
	18.220	-0.95	1	-0.95	1	1.1.1.1.1.1.
	18.300	-1.00	1	-1.00	1	1.1.1.1.1.1.
	18.380	-1.05	1	-1.05	1	1.1.1.1.1.1.
	18.460	-1.10	1	-1.10	1	1.1.1.1.1.1.
	18.540	-1.15	1	-1.15	1	1.1.1.1.1.1.
	18.620	-1.20	1	-1.20	1	1.1.1.1.1.1.
	18.700	-1.25	1	-1.25	1	1.1.1.1.1.1.
	18.780	-1.30	1	-1.30	1	1.1.1.1.1.1.
	18.860	-1.35	1	-1.35	1	1.1.1.1.1.1.
	18.940	-1.40	1	-1.40	1	1.1.1.1.1.1.
	19.020	-1.45	1	-1.45	1	1.1.1.1.1.1.
	19.100	-1.50	1	-1.50	1	1.1.1.1.1.1.
	19.180	-1.55	1	-1.55	1	1.1.1.1.1.1.
	19.260	-1.60	1	-1.60	1	1.1.1.1.1.1.
	19.340	-1.65	1	-1.65	1	1.1.1.1.1.1.
	19.420	-1.70	1	-1.70	1	1.1.1.1.1.1.
	19.500	-1.75	1	-1.75	1	1.1.1.1.1.1.
	19.580	-1.80	1	-1.80	1	1.1.1.1.1.1.
	19.660	-1.85	1	-1.85	1	1.1.1.1.1.1.
	19.740	-1.90	1	-1.90	1	1.1.1.1.1.1.
	19.820	-1.95	1	-1.95	1	1.1.1.1.1.1.
	19.900	-2.00	1	-2.00	1	1.1.1.1.1.1.
	19.980	-2.05	1	-2.05	1	1.1.1.1.1.1.
	20.060	-2.10	1	-2.10	1	1.1.1.1.1.1.
	20.140	-2.15	1	-2.15	1	1.1.1.1.1.1.
	20.220	-2.20	1	-2.20	1	1.1.1.1.1.1.
	20.300	-2.25	1	-2.25	1	1.1.1.1.1.1.
	20.380	-2.30	1	-2.30	1	1.1.1.1.1.1.
	20.460	-2.35	1	-2.35	1	1.1.1.1.1.1.
	20.540	-2.40	1	-2.40	1	1.1.1.1.1.1.
	20.620	-2.45	1	-2.45	1	1.1.1.1.1.1.
	20.700	-2.50	1	-2.50	1	1.1.1.1.1.1.
	20.780	-2.55	1	-2.55	1	1.1.1.1.1.1.
	20.860	-2.60	1	-2.60	1	1.1.1.1.1.1.
	20.940	-2.65	1	-2.65	1	1.1.1.1.1.1.
	21.020	-2.70	1	-2.70	1	1.1.1.1.1.1.
	21.100	-2.75	1	-2.75	1	1.1.1.1.1.1.
	21.180	-2.80	1	-2.80	1	1.1.1.1.1.1.
	21.260	-2.85	1	-2.85	1	1.1.1.1.1.1.
	21.340	-2.90	1	-2.90	1	1.1.1.1.1.1.
	21.420	-2.95	1	-2.95	1	1.1.1.1.1.1.
	21.500	-3.00	1	-3.00	1	1.1.1.1.1.1.
	21.580	-3.05	1	-3.05	1	1.1.1.1.1.1.
	21.660	-3.10	1	-3.10	1	1.1.1.1.1.1.
	21.740	-3.15	1	-3.15	1	1.1.1.1.1.1.
	21.820	-3.20	1	-3.20	1	1.1.1.1.1.1.
	21.900	-3.25	1	-3.25	1	1.1.1.1.1.1.
	21.980	-3.30	1	-3.30	1	1.1.1.1.1.1.
	22.060	-3.35	1	-3.35	1	1.1.1.1.1.1.
	22.140	-3.40	1	-3.40	1	1.1.1.1.1.1.
	22.220	-3.45	1	-3.45	1	1.1.1.1.1.1.
	22.300	-3.50	1	-3.50	1	1.1.1.1.1.1.
	22.380	-3.55	1	-3.55	1	1.1.1.1.1.1.
	22.460	-3.60	1	-3.60	1	1.1.1.1.1.1.
	22.540	-3.65	1	-3.65	1	1.1.1.1.1.1.
	22.620	-3.70	1	-3.70	1	1.1.1.1.1.1.
	22.700	-3.75	1	-3.75	1	1.1.1.1.1.1.
	22.780	-3.80	1	-3.80	1	1.1.1.1.1.1.
	22.860	-3.85	1	-3.85	1	1.1.1.1.1.1.
	22.940	-3.90	1	-3.90	1	1.1.1.1.1.1.
	23.020	-3.95	1	-3.95	1	1.1.1.1.1.1.
	23.100	-4.00	1	-4.00	1	1.1.1.1.1.1.
	23.180	-4.05	1	-4.05	1	1.1.1.1.1.1.
	23.260	-4.10	1	-4.10	1	1.1.1.1.1.1.
	23.340	-4.15	1	-4.15	1	1.1.1.1.1.1.
	23.420	-4.20	1	-4.20	1	1.1.1.1.1.1.
	23.500	-4.25	1	-4.25	1	1.1.1.1.1.1.
	23.580	-4.30	1	-4.30	1	1.1.1.1.1.1.
	23.660	-4.35	1	-4.35	1	1.1.1.1.1.1.
	23.740	-4.40	1	-4.40	1	1.1.1.1.1.1.
	23.820	-4.45	1	-4.45	1	1.1.1.1.1.1.
	23.900	-4.50	1	-4.50	1	1.1.1.1.1.1.
	23.980	-4.55	1	-4.55	1	1.1.1.1.1.1.
	24.060	-4.60	1	-4.60	1	1.1.1.1.1.1.
	24.140	-4.65	1	-4.65	1	1.1.1.1.1.1.
	24.220	-4.70	1	-4.70	1	1.1.1.1.1.1.
	24.300	-4.75	1	-4.75	1	1.1.1.1.1.1.
	24.380	-4.80	1	-4.80	1	1.1.1.1.1.1.
	24.460	-4.85	1	-4.85	1	1.1.1.1.1.1.
	24.540	-4.90	1	-4.90	1	1.1.1.1.1.1.
	24.620	-4.95	1	-4.95	1	1.1.1.1.1.1.
	24.700	-5.00	1	-5.00	1	1.1.1.1.1.1.
	24.780	-5.05	1	-5.05	1	1.1.1.1.1.1.
	24.860	-5.10	1	-5.10	1	1.1.1.1.1.1.
	24.940	-5.15	1	-5.15	1	1.1.1.1.1.1.
	25.020	-5.20	1	-5.20	1	1.1.1.1.1.1.
	25.100	-5.25	1	-5.25	1	1.1.1.1.1.1.
	25.180	-5.30	1	-5.30	1	1.1.1.1.1.1.
	25.260	-5.35	1	-5.35	1	1.1.1.1.1.1.
	25.340	-5.40	1	-5.40	1	1.1.1.1.1.1.
	25.420	-5.45	1	-5.45	1	1.1.1.1.1.1.
	25.500	-5.50	1	-5.50	1	1.1.1.1.1.1.
	25.580	-5.55	1	-5.55	1	1.1.1.1.1.1.
	25.660	-5.60	1	-5.60	1	1.1.1.1.1.1.
	25.740	-5.65	1	-5.65	1	1.1.1.1.1.1.
	25.820	-5.70	1	-5.70	1	1.1.1.1.1.1.
	25.900	-5.75	1	-5.75	1	1.1.1.1.1.1.
	25.980	-5.80	1	-5.80	1	1.1.1.1.1.1.
	26.060	-5.85	1	-5.85	1	1.1.1.1.1.1.
	26.140	-5.90	1	-5.90	1	1.1.1.1.1.1.
	26.220	-5.95	1	-5.95	1	1.1.1.1.1.1.
	26.300	-6.00	1	-6.00	1	1.1.1.1.1.1.
	26.380	-6.05	1	-6.05	1	1.1.1.1.1.1.
	26.460	-6.10	1	-6.10	1	1.1.1.1.1.1.
	26.540	-6.15	1	-6.15	1	1.1.1.1.1.1.
	26.620	-6.20	1	-6.20	1	1.1.1.1.1.1.
	26.700	-6.25	1	-6.25	1	1.1.1.1.1.1.
	26.780	-6.30	1	-6.30	1	1.1.1.1.1.1.
	26.860	-6.35	1	-6.35	1	1.1.1.1.1.1.
	26.940	-6.40	1	-6.40	1	1.1.1.1.1.1.
	27.020	-6.45	1	-6.45	1	1.1.1.1.1.1.
	27.100	-6.50	1	-6.50	1	1.1.1.1.1.1.
	27.180	-6.55	1	-6.55	1	1.1.1.1.1.1.
	27.260	-6.60	1	-6.60	1	1.1.1.1.1.1.
	27.340	-6.65	1	-6.65	1	1.1.1.1.1.1.
	27.420	-6.70	1	-6.70	1	1.1.1.1.1.1.
	27.500	-6.75	1	-6.75	1	1.1.1.1.1.1.
	27.580	-6.80	1	-6.80	1	1.1.1.1.1.1.
	27.660	-6.85	1	-6.85	1	1.1.1.1.1.1.
	27.740	-6.90	1	-6.90	1	1.1.1.1.1.1.
	27.820	-6.95	1	-6.95	1	1.1.1.1.1.1.
	27.900	-7.00	1	-7.00	1	1.1.1.1.1.1.
	27.980	-7.05	1	-7.05	1	1.1.1.1.1.1.
	28.060	-7.10	1	-7.10	1	1.1.1.1.1.1.
	28.140	-7.15	1	-7.15	1	1.1.1.1.1.1.
	28.220	-7.20	1	-7.20	1	1.1.1.1.1.1.
	28.300	-7.25	1	-7.25	1	1.1.1.1.1.1.
	28.380	-7.30	1	-7.30	1	1.1.1.1.1.1.
	28.460	-7.35	1	-7.35	1	1.1.1.1.1.1.
	28.540	-7.40	1	-7.40	1	1.1.1.1.1.1.
	28.620	-7.45	1	-7.45	1	1.1.1.1.1.1.
	28.700	-7.50	1	-7.50	1	1.1.1.1.1.1.
	28.780	-7.55	1	-7.55	1	1.1.1.1.1.1.
	28.860	-7.60	1	-7.60	1	1.1.1.1.1.1.
	28.940	-7.65	1	-7.65	1	1.1.1.1.1.1.
	29.020	-7.70	1	-7.70	1	1.1.1.1.1.1.
	29.100	-7.75	1	-7.75	1	1.1.1.1.1.1.
	29.180	-7.80	1	-7.80	1	1.1.1.1.1.1.
	29.260	-7.85	1	-7.85	1	1.1.1.1.1.1.
	29.340	-7.90	1	-7.90	1	1.1.1.1.1.1.
	29.420	-7.95	1	-7.95	1	1.1.1.1.1.1.
	29.500	-8.00	1	-8.00	1	1.1.1.1.1.1.
	29.580	-8.05	1	-8.05	1	1.1.1.1.1.1.
	29.660	-8.10	1	-8.10	1	1.1.1.1.1.1.
	29.740	-8.15	1	-8.15	1	1.1.1.1.1.1.
	29.820	-8.20	1	-8.20	1	1.1.1.1.1.1.
	29.900	-8.25	1	-8.25	1	1.1.1.1.1.1.
	29.980	-8.30	1	-8.30	1	1.1.1.1.1.1.
	30.060	-8.35	1	-8.35	1	1.1.1.1.1.1.
	30.140	-8.40	1	-8.40	1	1.1.1.1.1.1.
	30.220	-8.45	1	-8.45	1	1.1.1.1.1.1.
	30.300	-8.50	1	-8.50	1	1.1.1.1.1.1.
	30.380	-8.55	1	-8.55	1	1.1.1.1.1.1.
	30.460	-8.60	1	-8.60	1	1.1.1.1.1.1.
	30.540	-8.65	1	-8.65	1	1.1.1.1.1.1.
	30.620	-8.70	1	-8.70	1	1.1.1.1.1.1.
	30.700	-8.75	1	-8.75	1	1.1.1.1.1.1.
	30.780	-8.80	1	-8.80	1	1.1.1.1.1.1.
	30.860	-8.85	1	-8.85	1	1.1.1.1.1.1.
	30.940	-8.90	1	-8.90	1	1.1.1.1.1.1.
	31.020	-8.95	1	-8.95	1	1.1.1.1.1.1.
	31.100	-9.00	1	-9.00	1	1.1.1.1.1.1.
	31.180	-9.05	1	-9.05	1	1.1.1.1.1.1.
	31.260	-9.10	1	-9.10	1	1.1.1.1.1.1.
	31.340	-9.15	1	-9.15	1	1.1.1.1.1.1.
	31.420	-9.20	1	-9.20	1	1.1.1.1.1.1.
	31.500	-9.25	1	-9.25	1	1.1.1.1.1.1.
	31.580	-9.30	1	-9.30	1	1.1.1.1.1.1.
	31.660	-9.35	1	-9.35	1	1.1.1.1

Weighting in Observations

The residuals as tabulated in the preceding table are weighted for each observation in the following manner: the mean of the residuals of each observation being obtained, the probable error of each residual is then found and the weight taken proportional to the ^{square of} reciprocal of the probable error. For example we have the residuals for the observation at Clinton, N. C. in P. A. as follows: —

vide my page

Ulin low. 11.5.

Δx	x	xx
$-0.05 - .15$	$= -0.20$	$.0400$
$+0.03$	$= +0.12$	$.0144$
$+0.30$	$= +0.15$	$.0225$
$+0.15$	$= 0.00$	$.0000$
$+0.06$	$= -0.09$	$.0081$
$+0.35$	$= +0.15$	$.0225$
$+0.17$	$= +0.01$	$.0001$
$+0.46$	$= +0.25$	$.0625$
$+0.42$	$= +0.27$	$.0729$
$+0.25$	$= +0.10$	$.0100$
$+0.23$	$= +0.08$	$.0064$
$+0.28$	$= -0.07$	$.0049$
$+0.06$	$= -0.09$	$.0081$
$+0.09$	$= -0.06$	$.0036$
$+0.20$	$= +0.05$	$.0025$
$+0.25$	$= +0.10$	$.0100$
-0.12	$= -0.27$	$.0729$
$+0.40$	$= +0.25$	$.0625$
$+0.44$	$= -0.11$	$.0121$
$+0.14$	$= -0.01$	$.0001$
$+0.14$	$= -0.01$	$.0001$
$+0.05$	$= -0.10$	$.0100$
-0.01	$= -0.16$	$.0256$
		$\Sigma xx = .4468$

$$z = \sqrt{\frac{\Sigma xx}{n-1}}$$

$$r = \frac{z}{\sqrt{\frac{\Sigma x^2}{n-1}}}$$

$$r = .6745$$

$$\log \Sigma xx = .65011$$

$$\log n-1 = 1.2984$$

$$2/2.29027$$

$$9.14513$$

$$\log z = .82373$$

$$8.97411$$

$$r = 0.094$$

Since the probable error of a residual of this observation is a minimum as compared with the

probable errors of the other Observatories, we take the square root of the reciprocal of this probable error as weight unit and take the relative ratios of the probable errors of the residuals of the other Observatories considered in the same way for the respective weights. Proceeding in this manner we find the respective weights assigned in the preceding table, with the exception of a few observations which have been specially weighted.

The observations will now be grouped in the following manner for the purpose of forming the equations of condition.

(note and page)

(1)

date	1857	62	0-6 W	65	68	0-6 W	Place.	Star No.
Oct. 11, 5502	14.45	14.00	-0.05 1	48.8	54.3	-5.5 1	Clinton	[37].
" 12, 5877	14.45	14.47	+0.06 1	53.4	34.0	-0.6 1	Hungary	[34].
" 13, 3597	20.00	20.10	-0.10 1	56	26	1.0 1	Paris	[36].
" 13, 4558	24.80	24.60	-0.20 1	26.6	22.3	+4.3 1	Switzerland	[38].
" 13, 5201	20.68	20.92	-0.24 1/2	50.6	54.7	-4.1 1	Rome	[31].
" 13, 5898	16.76	16.73	+0.03 1	27.0	24.7	+2.3 1	Clinton	[29].
" 14, 3592	22.20	22.95	-0.22 1/2	56.1	52.7	+3.4 1/2	Algier	[35].
" 14, 3762	22.62	22.01	+0.61 1/2	50.3	45.4	+5.4 1/2	Algier	[35].
" 14, 4703	25.65	25.48	+0.17 1	57.4	55.1	+2.6 1	Paris	[30].
" 14, 4978	27.24	27.07	+0.15 1	54.5	52.5	+2.0 1	Paris	[30].
" 14, 5614	21.77	21.47	+0.30 1	31.4	25.2	+6.2 1	Clinton	[18].

 $n = +0.04$ $n = +0.99$ $+0.60 W 9.$

W10

(2)

Oct. 15, 3554	26.37	26.39	-0.02 1/2	42.4	40.7	+1.7 1	Algier	[34].
" 15, 3973	24.59	24.02	+0.37 1/2	26.6	22.4	+4.2 1	Algier	[34].
" 15, 4847	28.44	28.82	+0.12 1	44.1	42.7	+1.4 1	Paris	[30].
" 16, 3917	28.17	28.00	+0.17 1	9.7	9.3	+0.6 1	Paris	[31].
" 16, 5408	20.57	20.65	+0.40 1/2	57.4	64.2	-6.8 1/2	Paris	[38].
" 16, 5408	20.77	20.65	+0.34 1/2	4.5	4.2	+0.3 1	Rome	[22].
" 17, 3638	43.97	43.85	+0.12 1/2	49	51	-0.2 1	Algier	[22].
" 17, 3781	42.77	42.85	+0.12 1/2	57.3	57.2	+0.1 1	Algier	[22].
" 17, 4799	36.33	36.24	+0.07 1	6.1	5.2	+0.9 1	Vienne	[27].
" 18, 4650	48.11	48.24	-0.13 1	6.5	5.1	+1.4 1	Rome	[22].

 $n = +0.13 1$ $n = +1.20$ $+1.77 W 7$

W. 9

(3)

Oct. 19, 5775	42.46	42.81	+0.15 1	57.5	57.1	+0.4 1	Clinton	[24].
" 19, 5904	42.11	42.11	+0.06 1	51.5	51.5	-0.2 1	Clinton	[26].
" 20, 3873	57.26	57.61	-0.35 1/2	9.4	4.1	+5.3 1/2	Switzerland	[37].
" 20, 5205	52.42	52.50	-0.08 1/2	6.6	6.2	+0.4 1	Paris	[30].
" 21, 3707	7.61	7.72	-0.31 1/2	57.7	57.5	+0.2 1	Paris	[30].
" 21, 4526	27.00	27.65	+0.25 1/2	21.7	27.8	+0.1 1	Paris	[20].
" 21, 5451	47.20	47.55	+0.35 1	47.6	41.8	+5.8 1	Clinton	[16].
" 22, 3607	16.44	16.77	-0.30 1/2	41.4	43.7	-2.3 1/2	Switzerland	[13].
" 23, 3080	24.20	24.16	+0.04 1	6.6	4.1	+2.5 1	Vienne	[27].

 $n = +0.08$ $n = +0.9$ $+1.2 W 6$

W. 8

11

1881.	26.3627	2.93	2.36 - 0.07	1/3	44.6	42.2 + 2.4	1	Streckendorf, [14].
"	26.36	2.94	2.36 - 0.07	1	44.6	42.2 + 2.4	1	"
"	27.3660	17.90	17.60 + 0.30	1/3	49.6	51.0 - 2.4	1	Streckendorf [2].
"	31.6351	22.78	22.37 + 0.41	1	7.7	6.9 + 0.8	1	Glinitze [27].
Nov.	2.5471	12.58	12.16 + 0.42	1	15.3	12.6 + 2.7	1	Glinitze, [11].
"	5.5303	40.46	40.15 + 0.31	1	37.4	33.4 + 4.0	1	Glinitze, [1].
"	6.5840	11.27	11.04 + 0.23	1	58.1	56.9 + 1.2	1	Glinitze [19].

$$u = +0.22$$

$$= +3.70 \text{ W.4}$$

$$u = +1.27$$

$$\text{W.7}$$

(5)								
Nov.	13.3420	56.29	56.03 + 0.26	1	2.4	1.4 + 1.0	1	Vienna, [27]
"	13.3992	55.55	55.28 + 0.27	1/2	47.6	48.0 - 0.4	1	Roma, [2].
"	16.3479	26.12	25.80 + 0.32	1/3	13.6	12.3 - 0.7	1	Streckendorf [29].
"	17.5014	17.14	16.67 + 0.47	1/2	7.7	7.4 - 0.3	1	Glinitze, [1].
"	18.5578	15.07	15.47 - 0.42	1/4	48.6	43.0 + 5.6	5	Glinitze, [3].
"	21.2042	15.85	16.31 - 0.43	1/2	12.8	12.2 - 0.6	1/2	Roma [2].

$$u = +0.127$$

$$= +1.91 \text{ W.3}$$

$$u = +0.23$$

$$\text{W.4}$$

(6)								
Dec.	3.2435	13.87	13.70 + 0.17	1/2	15.0	14.3 + 0.7	1	Berlin, [2].
"	6.6	11.1	10.78 + 0.32	1	54.1	51.1 + 3.0	1	Glinitze, [10].
"	9.4755	29.28	29.22 + 0.06	1	54.3	53.7 + 0.6	1	Glinitze, [28].
"	11.5000	45.64	45.55 + 0.09	1	34.5	36.6 - 2.1	1	Glinitze, [12].
"	13.4743	8.01	7.81 + 0.20	1	1.7	1.4 - 0.3	1	Glinitze, [10].

$$u = +0.111$$

$$= +1.76 \text{ W.4}$$

$$u = +0.26$$

$$\text{W.5}$$

(7)								
Jan.	5.138	27.07	27.20 + 0.13	1	4.6	7.9 - 3.3	1	Glinitze, [3].
"	11.5644	55.26	55.38 - 0.12	1	14.1	17.6 + 3.5	1	Glinitze, [40].
"	14.5335	48.56	48.16 + 0.40	1	53.7	46.8 + 7.1	1	Glinitze, [4].
"	15.2680	46.96	46.86 + 0.10	1	10.6	21.2 - 10.6	1	Vienna, [24].

$$u = +0.157$$

$$= 2.35 \text{ W.4.}$$

$$+0.78$$

$$\text{W.4}$$

Jan.	31.5511	15.04	15.00 + 0.04	1	12.0	10.8 + 1.2	1	Glinitze, [43].
Feb.	3.5346	52.15	52.14 - 0.01	1	52.5	50.3 + 2.2	1	Glinitze, [45].
"			52.14 - 0.01	1		11.7		
"			52.14 - 0.01	1		W.2.		
Feb.	6.5357	36.57	36.57 + 0.00	1	46.8	48.5 - 1.7	1	Glinitze, [44].
"	8.5355	42.01	42.01 + 0.00	1	32.3	31.4 + 0.8	1	Glinitze, [46].
"	11.5351	57.64	57.64 + 0.00	1	22.4	22.1 - 0.3	1	Glinitze, [47].

$$u = +0.06$$

$$= +0.94 \text{ W.3}$$

$$-1.23$$

$$\text{W.3}$$

March	9.5332	44.34	44.35 - 0.01		45.5	48.1 - 2.6		Glinitze, [48].
-------	--------	-------	--------------	--	------	------------	--	-----------------

7) Specializing

Equations of Condition

By dividing the observations into two groups, and taking the mean of the residuals of each group, in 1887 Jan. and Dec. we form with these residuals twenty equations of condition, ten of them arising from the residuals in R.A. and ten from those in Decl. But for the time for which the equations of condition are formed, we then have the following quantities for the right hand members of the equations of condition.

$\bar{r}$	Jan	$\bar{w}$	Dec	$\bar{w}$	
1887. Oct. 12.5	+ 0.60	9	+ 0.09	10	1887 Oct. 11 - 14
" " 16.5	+ 1.97	7	+ 1.20	9	" " 15 - 18
" " 20.5	+ 1.20	6	+ 0.90	8	" " 19 - 23
" Nov. 1.5	+ 3.30	6	+ 1.27	7	" " 26 - Nov. 6
" " 17.5	+ 1.91	3	+ 0.23	4	" Nov. 13 - 21
" Dec. 7.5	+ 1.76	5	+ 0.26	5	" Dec. 3 - 13
1888. Jan. 11.5	+ 2.35	4	+ 0.78	4	1888 Jan. 5 - 18
" Feb. 3.5	- 0.75	2	- 1.70	2	" " 31 - Feb. 3
" " 9.5	+ 0.94	3	- 1.23	3	" Feb. 6 - 13
" Mar. 9.5	- 0.15	1	- 2.60	1	" Mar. 9.

The computation for the differential

coefficients will be as follows:

Computations of the Functions of the First Kind X III.

	1917 Oct. 125	Oct 162	Oct 200	Oct 237	Oct 275
$\sin \alpha$	0.49746	0.497514	0.49757	0.49762	0.49767
Δ	0.00079	0.00080	0.00081	0.00082	0.00083
$\cos \alpha$	0.97740	0.97791	0.97841	0.97892	0.97943
$\frac{\sin \alpha}{\rho}$	0.51667	0.49134	0.46205	0.43791	0.41651
$\sin \delta$	0.31732	0.29980	0.28132	0.26482	0.24943
$\frac{\cos \alpha}{\rho}$	0.09661	0.09591	0.09520	0.09449	0.09378
$\cos \delta$	0.90043	0.90110	0.90192	0.90280	0.90374
ρ	0.98079	0.98000	0.97951	0.97900	0.97825
$\cos \delta \frac{d\alpha}{dx}$	0.51667 _n	0.49134 _n	0.46205	0.43791 _n	0.41651 _n
$\cos \delta \frac{d\alpha}{dy}$	0.09661	0.09591	0.09520	0.09449	0.09375
$\frac{d\delta}{dy}$	0.31303 _n	0.29571 _n	0.27462 _n	0.25444 _n	0.23569 _n
$\frac{d\delta}{dx}$	0.82344 _n	0.77114 _n	0.71452 _n	0.65274 _n	0.58585 _n
$\frac{d\delta}{dz}$	0.00964	0.00739	0.00540	0.00389	0.00260
$\cos(A+u)$	0.56584 _n	0.56207 _n	0.55812 _n	0.55412 _n	0.55006 _n
x	0.26232	0.25204	0.24553	0.24227	0.23920
$\cot(B+u)$	0.45386	0.41327	0.38513	0.36507	0.34920
y	0.97609	0.97372	0.97147	0.96927	0.96711
$\cot(C+u)$	0.21727	0.20854	0.20104	0.19440	0.18813
z	0.21862	0.54281	0.56540	0.62553	0.69188

	Oct. 12.5	Oct. 16.5	Oct. 20.5	Nov. 1.5	Nov. 15.5
1	0.7552	0.90253	0.83847	0.01617	0.00227
cos 2	0.06222	0.96255	0.96255	0.06255	0.01257
3	0.25232	0.25232	0.25553	0.24307	0.22202
sin 2	0.55010	0.59990	0.59990	0.59990	0.55010
2	0.51502	0.54281	0.56546	0.62262	0.61177
3 cos 2	0.72204	0.77103	0.80102	0.75577	0.66147
2 sin 2	0.11852	0.14271	0.16536	0.22223	0.27143
4	0.71348	0.72014	0.72605	0.74033	0.75542
$\frac{1}{\sin}$	0.83200 _n	0.86785 _n	0.89141 _n	0.96554 _n	0.94555 _n
$\frac{1}{\cos}$	0.83116	0.86207	0.89065	0.96520	0.94547
5	0.28500	0.25500	0.24500	0.19500	0.14000
$\frac{0.5}{\sin}$	0.11610 _n	0.11707 _n	0.13565 _n	0.16020 _n	0.18405 _n
$\frac{0.5}{\cos}$	0.22487	0.22163	0.21303	0.20562	0.19145
$\frac{1}{\sin}$	0.22299 _n	0.2261 _n	0.2236 _n	0.2115 _n	0.1917 _n
6	8.04100	8.05720	8.10700	8.15500	8.22250
$\frac{1}{\cos}$	8.29587 _n	8.50113 _n	8.72302 _n	8.9626 _n	9.4040 _n
$\frac{1}{\sin}$	0.86222	0.83501	0.85543	0.84297	0.81177
$\frac{1}{\cos}$	0.83540 _n	0.83135 _n	0.82650 _n	0.80992 _n	0.7720 _n
7	5.0553	5.51750	5.83514	5.89500	5.77213
$\frac{0.5}{\sin}$	5.62177	5.64585	5.66464	5.70792	5.75777

	Oct. 12.5	Oct. 16.5	Oct. 20.5	Oct. 24.5	Nov. 17.5
$\frac{d_1}{d_2}$	0.25116 _n	0.26207 _n	0.29065 _n	0.26520	0.04405
$\frac{d_2}{d_3}$	0.22405	0.22611	0.22360	0.21182	0.19176
$\frac{d_3}{d_4}$	0.23287	0.23135	0.22650	0.20977	0.178290
r	0.20060	0.20175	0.20245	0.20670	0.20197
r_{11}	0.90854	0.91001	0.91108	0.91550	0.91822
r_{111}	0.19914	0.19179	0.18402	0.15520	0.11715
c_{1a}	0.59832 _n	0.59522 _n	0.59322 _n	0.59522 _n	0.59172 _n
c_{1b}	0.59832 _n	0.59522 _n	0.59322 _n	0.59832 _n	0.59832 _n
c_{1c}	0.96426	0.96426	0.96426	0.96426	0.96426
$\frac{d_1}{d_4}$	0.20976 _n	0.20011 _n	0.20222 _n	0.205652 _n	0.20547 _n
$\frac{d_2}{d_4}$	0.17546 _n	0.17501 _n	0.175235	0.174652 _n	0.17547 _n
$\frac{d_3}{d_4}$	0.16240	0.15605	0.14870	0.12246	0.08141
x	0.26232	0.25908	0.25573	0.24707	0.22202
y	0.77669	0.80353	0.82547	0.91617	0.99555
z	0.81862	0.84281	0.86546	0.87563	0.89155
r	0.20060	0.20175	0.20245	0.20670	0.20192
$\frac{d_1}{d_7}$	0.99172	0.96720	0.96257	0.94637	0.92010
$\frac{d_2}{d_7}$	0.45549	0.51675	0.54549	0.61947	0.69696
$\frac{d_3}{d_7}$	0.22502	0.25102	0.27245	0.32893	0.38963

[illegible]

	31075	31076	31077	31078	31079
1	0.07929	0.15015	0.22744	0.23556	0.27905
2	0.06255	0.06255	0.06255	0.06255	0.06255
3	0.15807	0.10446	0.02791	0.00422	0.85860
4	0.59990	0.59999	0.59999	0.59999	0.59999
5	0.75701	0.54009	0.87573	0.55715	0.91960
6	0.04184	0.14273	0.18099	0.20041	0.24150
7	0.35691	0.43998	0.47862	0.48704	0.51949
8	0.76648	0.76130	0.75551	0.74018	0.79743
9	0.12339 _m	0.22125 _m	0.26713 _m	0.27722	0.31692 _m
10	0.12255	0.22032	0.26670	0.27681	0.31655
11	0.09500	0.02500	0.00000	0.07500	0.93000
12	0.21755 _m	0.24582 _m	0.26670 _m	0.25181 _m	0.24655 _m
13	0.15062	0.06701	0.99046	0.76677	0.52115
14	0.15921 _m	0.07878 _m	0.00523 _m	0.05254 _m	0.54386 _m
15	8.30050	8.43960	8.53900	8.56800	8.72990
16	8.45112 _m	8.50601 _m	8.52746 _m	8.52477 _m	8.5105 _m
17	0.78797	0.70435	0.64780	0.60411	0.45849
18	0.74033 _m	0.63635 _m	0.53945 _m	0.50883 _m	0.31057 _m
19	0.06420	0.22714	0.35333	0.38974	0.60831
20	5.60453	5.86540	8.9275	8.9857	8.91858

	Oct 7.5	Nov 11.5	Feb 3.5	Mar 11.5	Mar 01.5
$\frac{1}{4}$	0.12285 _m	0.2-0-0 _m	0.2000 _m	0.27681 _m	0.1659 _m
$\frac{1}{4}$	0.15021	0.27578	0.20523	0.98254	0.84186
$\frac{1}{4}$	0.74033	0.686	0.5344	0.50883	0.1007
r	0.30876	0.2-1-2 _m	0.2-0.46	0.33160	0.34176
$\sin u$	0.4442	0.57110	0.39655	0.2700	0.50520
$r \sin u$	0.05319	0.26230	0.72631	0.66560	0.14677
$\cos a$	0.59832 _m	0.59854 _m	0.59859 _m	0.59859 _m	0.59859 _m
$\cos b$	0.58832 _m	0.58833 _m	0.58833 _m	0.58833 _m	0.58833 _m
$\cos c$	0.96420	0.96420	0.96426	0.96426	0.96426
$\frac{d}{dt}$	0.65151	0.4705 _m	0.2490 _m	0.26719 _m	0.74556 _m
$\frac{d}{dt}$	0.64151 _m	0.48063 _m	0.31464 _m	0.25693 _m	0.73530 _m
$\frac{d}{dt}$	0.01445	0.85656	0.69057	0.63286	0.11122
x	0.18207	0.10446	0.02791	0.00422	0.85860
y	0.07929	0.18018	0.22744	0.22786	0.27895
z	0.75901	0.84009	0.57873	0.55715	0.91960
r	0.30876	0.32120	0.32046	0.33160	0.34176
$\frac{1}{4}$	0.87931	0.75326	0.69847	0.67262	0.51623
$\frac{1}{4}$	0.77052	0.87297	0.89798	0.90626	0.92710
$\frac{1}{4}$	0.44525	0.51889	0.54927	0.55555	0.57752

	$\alpha = 2$	$\alpha = 1.7$	$\alpha = 1.5$	$\alpha = 1.5$	$\alpha = 1.5$
$\frac{1}{\sin \theta}$	9.91576	1.11107	9.91576	9.91576	1.11107
$\frac{1}{\cos \theta}$	0.57091	1.58017	9.91576	9.91576	9.91576
$\frac{1}{\sin \theta} + \log \cos \theta$	9.91576	8.91576	8.91576	8.91576	8.91576
$\frac{1}{\sin \theta} - \log \cos \theta$	0.30596	0.30596	0.30596	0.30596	0.30596
$\frac{1}{\sin \theta}$	0.30596	0.30596	0.30596	0.30596	0.30596
$\frac{1}{\sin \theta} + \log \cos \theta$	0.32722	0.32722	0.32722	0.32722	0.32722
r^2	0.58120	0.58120	0.58120	0.58120	0.58120
$\frac{1}{r^2}$	0.58120	0.58120	0.58120	0.58120	0.58120
$t - \pi$	1.90037 _n	1.87795 _n	1.85431 _n	1.77452 _n	1.65814 _n
$\frac{1}{\sin \theta} + \log \cos \theta$	9.44352	9.44352	9.44352	9.44352	9.44352
$2 - \frac{1}{\sin \theta}$	8.61545	8.61545	8.61545	8.61545	8.61545
r	0.29060	0.29178	0.29178	0.29060	0.30192
$2\pi(2.062648)$	5.91605	5.90723	5.90843	5.91215	5.91707
$5u$	3.51414	3.51414	3.51414	3.51414	3.51414
$-\frac{1}{2} \cdot \frac{1}{u} (2.062648)$	2.31111 _n	2.34309 _n	2.34309 _n	2.34309 _n	2.40323 _n
$a \tan \theta \sin f(t - \pi)$	1.24374 _n	1.28153 _n	1.26737 _n	1.21277 _n	1.20407 _n
$\frac{1}{\sin \theta}$	0.03334	0.03236	0.03127	0.02747	0.02662
$\frac{dr}{d\mu}$	2.42526 _n	2.42545 _n	2.42556 _n	2.42548 _n	2.42985 _n
$\frac{df}{d\mu}$	1.97343 _n	1.97343 _n	1.94739 _n	1.86016 _n	1.71369 _n
$\frac{d\theta}{d\mu}$	0.16276 _n	0.14076 _n	0.13600 _n	0.09071 _n	0.01572 _n
$\frac{d\theta}{d\mu}$	0.19813	0.20757	0.21642	0.23977	0.26427
$\frac{d\theta}{d\mu}$	1.31352	1.40352	1.41306	1.43355	1.46558
$\frac{d\theta}{d\mu}$	0.09794	0.09784	0.09548	0.09308	0.08564

	1957. Oct. 12.5	Oct. 16.5	Oct. 20.5	Nov. 4.5	Nov. 17.5
$\cos \frac{dx}{dy}$	0.5111	0.49134 _n	0.4625 _n	0.37791 _n	0.28641 _n
$\frac{dx}{dy}$	0.97172	0.96730	0.96255	0.94637	0.92010
$\cos \frac{dx}{dy}$	0.99661	0.99591	0.99330	0.97461	0.94275
$\frac{dx}{dy}$	2.48540	0.51675	0.54549	0.61947	0.69646
$\cos \frac{dx}{dy}$	0.48839 _n	0.45864 _n	0.4260 _n	0.3241 _n	0.20701 _n
$\frac{dx}{dy}$	0.48210	1.51166	0.52571	0.59408	0.62671
$\cos \frac{dx}{dy}$	8.16420	0.12207	0.46971	0.6351 _n	0.71171
$\frac{dx}{dy}$	7.64610 _n	8.55072	0.89629	0.25091	0.11558
$\cos \frac{dx}{dy}$	0.51667 _n	0.49134 _n	0.4625 _n	0.37791 _n	0.28641 _n
$\frac{dx}{dy}$	0.83116 _n	0.96207 _n	0.96065 _n	0.96520 _n	0.94498 _n
$\cos \frac{dx}{dy}$	0.99661	0.99591	0.99330	0.97461	0.942975
$\frac{dx}{dy}$	0.78746 _n	0.75011 _n	0.71775 _n	0.6165 _n	0.50547 _n
$\cos \frac{dx}{dy}$	0.34783	0.35341	0.35460	0.34311	0.32189
$\frac{dx}{dy}$	0.22656	0.22277	0.21690	0.18646	0.12151
$\cos \frac{dx}{dy}$	0.65343	0.65503	0.65587	0.65521	0.66532
$\frac{dx}{dy}$	0.25149	0.25785	0.27271	0.24904	0.18087
$\frac{dx}{dy}$	+1.00760	+1.50602	+1.87520	+1.75650	+1.53759
$\cos \frac{dx}{dy}$	0.51667 _n	0.49134 _n	0.46395 _n	0.37791 _n	0.28641 _n
$\frac{dx}{dy}$	7.11616 _n	7.1107 _n	7.13568 _n	7.16020 _n	7.18473 _n
$\cos \frac{dx}{dy}$	0.99661	0.99591	0.99430	0.97461	0.942975
$\frac{dx}{dy}$	8.29557 _n	8.30913 _n	8.32506 _n	8.36362 _n	8.40707 _n

	Oct. 12.5	Oct. 16.5	Oct. 16.5	Nov. 1.5	Nov. 17.5
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	6.63252	6.60841	6.7966	6.87811	6.47189
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	8.20293 _n	8.20009 _n	8.11828 _n	8.2387 _n	8.33682 _n
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	1.65003	1.68781	1.71009	1.79308	1.55596
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	8.70746 _n	8.70677	8.70777	8.7119 _n	8.23055 _n
	-0.2195	-0.0107	-0.2042	-0.0146	-0.0147
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	4.49661	4.49591	4.47320	4.47461	4.42075
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	4.77544 _n	4.78011 _n	4.77228 _n	4.74652 _n	4.70547 _n
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	4.51667 _n	4.49134 _n	4.46308 _n	4.37791 _n	4.25691 _n
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	8.70746 _n	8.79011	8.75208 _n	8.75652 _n	8.71547 _n
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	4.78107 _n	4.77602 _n	4.76862	4.7711 _n	4.7777 _n
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	8.11717	8.28167	8.24020	8.12442	8.0007
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	1.45407	1.48043	1.50600	1.57531	0.62260
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	4.76010 _n	4.76155 _n	4.75221 _n	4.70074 _n	4.62408
$\Delta S \delta \frac{1}{\Delta t} \frac{dx}{dt}$	-0.55762	-0.57704	-0.56534	-0.51255	-0.42169
$\frac{dx}{dt}$	4.31343 _n	4.29571 _n	4.27462 _n	4.14914 _n	4.00569 _n
$\frac{dx}{dt}$	4.07172	4.06730	4.02655	4.01127	4.07210
$\frac{dx}{dt}$	8.20293 _n	8.29114 _n	8.24027 _n	8.60274 _n	8.45255 _n
$\frac{dx}{dt}$	4.47229	4.51677	4.54540	4.61047	4.69606
$\frac{dx}{dt}$	4.28765 _n	4.26301 _n	4.20117 _n	4.14751 _n	4.01579
$\frac{dx}{dt}$	8.31948 _n	8.30769 _n	8.27076 _n	8.22221	8.14981 _n
$\frac{dx}{dt}$	0.04458	0.04567	0.05034	0.04892	0.05543
$\frac{dx}{dt}$	4.33023 _n	4.30868 _n	4.27171 _n	4.19473 _n	4.1712 _n
$\frac{dx}{dt}$	4.23766	4.25842	4.27777	4.31052	4.32564
$\frac{dx}{dt}$	0.71691				
$\frac{dx}{dt}$	8.61342 _n	8.34712 _n	8.2722 _n	8.25106	8.2722

	12. 7. 2	12. 7. 3	12. 7. 4	12. 7. 5	12. 7. 6
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32864 _n	0.32864 _n	0.38563 _n	0.39855 _n	0.44800 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.78326	0.78326	0.69845	0.67262	0.51653
$\cos \frac{1}{2} \frac{dx}{dt}$	0.55607	0.71222	0.61191	0.55446	0.43780
$\cos \frac{1}{2} \frac{dx}{dt}$	0.97053	0.85998	0.59705	0.1620	0.03714
$\cos \frac{1}{2} \frac{dx}{dt}$	0.13450 _n	0.11190 _n	0.08408 _n	0.07117 _n	0.06484 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.62660	0.57120	0.50989	0.44072	0.37499
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32331	0.27401	0.22160	0.21153	0.19627
$\cos \frac{1}{2} \frac{dx}{dt}$	0.45751	0.35591	0.30568	0.28270	0.16111
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32864 _n	0.32864 _n	0.38563 _n	0.39855 _n	0.44800 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.78326	0.78326	0.69845	0.67262	0.51653
$\cos \frac{1}{2} \frac{dx}{dt}$	0.55607	0.71222	0.61191	0.55446	0.43780
$\cos \frac{1}{2} \frac{dx}{dt}$	0.97053	0.85998	0.59705	0.25693 _n	0.03714
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32864 _n	0.32864 _n	0.38563 _n	0.39855 _n	0.44800 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.78326	0.78326	0.69845	0.67262	0.51653
$\cos \frac{1}{2} \frac{dx}{dt}$	0.55607	0.71222	0.61191	0.55446	0.43780
$\cos \frac{1}{2} \frac{dx}{dt}$	0.97053	0.85998	0.59705	0.25693 _n	0.03714
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32864 _n	0.32864 _n	0.38563 _n	0.39855 _n	0.44800 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.78326	0.78326	0.69845	0.67262	0.51653
$\cos \frac{1}{2} \frac{dx}{dt}$	0.55607	0.71222	0.61191	0.55446	0.43780
$\cos \frac{1}{2} \frac{dx}{dt}$	0.97053	0.85998	0.59705	0.25693 _n	0.03714
$\cos \frac{1}{2} \frac{dx}{dt}$	0.32864 _n	0.32864 _n	0.38563 _n	0.39855 _n	0.44800 _n
$\cos \frac{1}{2} \frac{dx}{dt}$	0.78326	0.78326	0.69845	0.67262	0.51653
$\cos \frac{1}{2} \frac{dx}{dt}$	0.55607	0.71222	0.61191	0.55446	0.43780
$\cos \frac{1}{2} \frac{dx}{dt}$	0.97053	0.85998	0.59705	0.25693 _n	0.03714

	Feb. 2, 8	Mar. 11, 8	Feb. 2, 8	Feb. 2, 8	Mar. 11, 8
600g	1.7000	1.7000	1.6135	1.4000	1.1000
200g	1.7000	1.4430	1.4000	1.4000	1.4000
100g	1.7000	1.4000	1.4000	1.4000	1.4000
50g	1.7000	1.4000	1.4000	1.4000	1.4000
25g	1.7000	1.4000	1.4000	1.4000	1.4000
12.5g	1.7000	1.4000	1.4000	1.4000	1.4000
6.25g	1.7000	1.4000	1.4000	1.4000	1.4000
3.125g	1.7000	1.4000	1.4000	1.4000	1.4000
1.5625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.78125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.390625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.1953125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.09765625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.048828125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0244140625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.01220703125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.006103515625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0030517578125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00152587890625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000762939453125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0003814697265625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00019073486328125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000095367431640625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000476837158203125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00002384185791015625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000011920928955078125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000059604644775390625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000298023223876953125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000001490116119384765625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000007450580596923828125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000037252902984619140625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000000186264514923095703125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000000931322574615478515625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000004656612873077392578125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000000023283064365386962890625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000000116415321826934814453125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000000582076609134674072265625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000000002910383045673370361328125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000000014551915228366851806640625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000000072759576141834259033203125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.000000000363797880709171295166015625g	1.7000	1.4000	1.4000	1.4000	1.4000
0.0000000001818989403545856475830078125g	1.7000	1.4000	1.4000	1.4000	1.4000
0.00000000009094947017729282379150390625g	1.7000	1.4000	1.4000	1.4000	1.

	1897 Oct. 12.5	Oct. 16.5	Oct. 20.5	Nov. 1.5	Nov. 17.5
$\cos \frac{1}{2} \frac{1}{J_1}$	7.64610 _n	5.58072	5.59639	9.28941	9.41375
$\frac{1}{J_1}$	0.16276 _n	0.14970 _n	0.13600 _n	0.09071 _n	0.01882 _n
$\cos \frac{1}{2} \frac{1}{J_2}$	0.25049	0.27785	0.27277	0.24464	0.15654
$\frac{1}{J_2}$	0.19812	0.20757	0.21642	0.23977	0.2427
$\cos \frac{1}{2} \frac{1}{J_3}$	7.50286	5.73042 _n	9.03240 _n	9.65017 _n	9.14276 _n
$\frac{1}{J_3}$	0.47867	0.45537	0.45919	0.48441	0.47117
$\cos \frac{1}{2} \frac{1}{J_4}$	0.00001	0.00770	0.01844	0.02211	0.04428
$\frac{1}{J_4}$	0.47957	0.47772	0.47375	0.48130	0.46688
$\cos \frac{1}{2} \frac{1}{J_5}$	+ 3.01653	+ 2.00414	+ 2.97683	+ 2.82027	+ 2.85155
$\frac{1}{J_5}$	8.61342 _n	8.34713 _n	7.53540 _n	8.68106	8.97229
$\frac{1}{J_6}$	0.16276 _n	0.14970 _n	0.13600 _n	0.09071 _n	0.01882 _n
$\frac{1}{J_7}$	9.56004	9.56297	9.86283	9.54512	9.79071
$\frac{1}{J_8}$	0.19813	0.20757	0.21642	0.23977	0.26429
$\frac{1}{J_9}$	8.77618	8.49682	7.67129	8.77177 _n	8.99121 _n
$\frac{1}{J_{10}}$	0.05817	0.07157	0.07928	0.08459	0.08502
$\frac{1}{J_{11}}$	0.02211	0.01144	0.00169	0.02165	0.03920
$\frac{1}{J_{12}}$	0.05029	0.05195	0.05094	0.06324	0.01582
	+ 1.20308	+ 1.20775	+ 1.20486	+ 1.15676	+ 1.03709
$\cos \frac{1}{2} \frac{1}{J_{13}}$	7.64610 _n	5.58072	5.59639	9.28941	9.41375
$\frac{1}{J_{14}}$	9.39352	9.40257	9.41306	9.43835	9.46558
$\cos \frac{1}{2} \frac{1}{J_{15}}$	0.25049	0.27785	0.27277	0.24464	0.15654
$\frac{1}{J_{16}}$	0.09784	0.09545	0.09005	0.08564	0.07520
$\cos \frac{1}{2} \frac{1}{J_{17}}$	7.03963 _n	7.05430	5.30945	5.69776	5.58427
$\frac{1}{J_{18}}$	0.37523	0.37232	0.36855	0.33027	0.26204
$\frac{1}{J_{19}}$	0.00001	0.00177	0.00250	0.01000	0.01753
$\frac{1}{J_{20}}$	0.37512	0.37510	0.36065	0.34029	0.27457
	+ 2.53551	+ 2.57200	+ 2.54238	+ 2.15920	+ 1.91401

[illegible]

	0.8.16.2	0.8.16.3	0.8.16.4	0.8.16.5	0.8.16.6
$\frac{1}{1}$	86130 _n	86131 _n	86132 _n	86133 _n	86134 _n
$\frac{1}{2}$	43065 _n	43066 _n	43067 _n	43068 _n	43069 _n
$\frac{1}{3}$	28710 _n	28711 _n	28712 _n	28713 _n	28714 _n
$\frac{1}{4}$	21532 _n	21533 _n	21534 _n	21535 _n	21536 _n
$\frac{1}{5}$	17226 _n	17227 _n	17228 _n	17229 _n	17230 _n
$\frac{1}{6}$	14355 _n	14356 _n	14357 _n	14358 _n	14359 _n
$\frac{1}{7}$	12300 _n	12301 _n	12302 _n	12303 _n	12304 _n
$\frac{1}{8}$	10762 _n	10763 _n	10764 _n	10765 _n	10766 _n
$\frac{1}{9}$	9566 _n	9567 _n	9568 _n	9569 _n	9570 _n
$\frac{1}{10}$	8613 _n	8614 _n	8615 _n	8616 _n	8617 _n
$\frac{1}{11}$	7830 _n	7831 _n	7832 _n	7833 _n	7834 _n
$\frac{1}{12}$	7180 _n	7181 _n	7182 _n	7183 _n	7184 _n
$\frac{1}{13}$	6622 _n	6623 _n	6624 _n	6625 _n	6626 _n
$\frac{1}{14}$	6150 _n	6151 _n	6152 _n	6153 _n	6154 _n
$\frac{1}{15}$	5750 _n	5751 _n	5752 _n	5753 _n	5754 _n
$\frac{1}{16}$	5412 _n	5413 _n	5414 _n	5415 _n	5416 _n
$\frac{1}{17}$	5125 _n	5126 _n	5127 _n	5128 _n	5129 _n
$\frac{1}{18}$	4883 _n	4884 _n	4885 _n	4886 _n	4887 _n
$\frac{1}{19}$	4675 _n	4676 _n	4677 _n	4678 _n	4679 _n
$\frac{1}{20}$	4490 _n	4491 _n	4492 _n	4493 _n	4494 _n
$\frac{1}{21}$	4326 _n	4327 _n	4328 _n	4329 _n	4330 _n
$\frac{1}{22}$	4180 _n	4181 _n	4182 _n	4183 _n	4184 _n
$\frac{1}{23}$	4050 _n	4051 _n	4052 _n	4053 _n	4054 _n
$\frac{1}{24}$	3935 _n	3936 _n	3937 _n	3938 _n	3939 _n
$\frac{1}{25}$	3833 _n	3834 _n	3835 _n	3836 _n	3837 _n
$\frac{1}{26}$	3742 _n	3743 _n	3744 _n	3745 _n	3746 _n
$\frac{1}{27}$	3661 _n	3662 _n	3663 _n	3664 _n	3665 _n
$\frac{1}{28}$	3589 _n	3590 _n	3591 _n	3592 _n	3593 _n
$\frac{1}{29}$	3526 _n	3527 _n	3528 _n	3529 _n	3530 _n
$\frac{1}{30}$	3471 _n	3472 _n	3473 _n	3474 _n	3475 _n
$\frac{1}{31}$	3423 _n	3424 _n	3425 _n	3426 _n	3427 _n
$\frac{1}{32}$	3381 _n	3382 _n	3383 _n	3384 _n	3385 _n
$\frac{1}{33}$	3344 _n	3345 _n	3346 _n	3347 _n	3348 _n
$\frac{1}{34}$	3312 _n	3313 _n	3314 _n	3315 _n	3316 _n
$\frac{1}{35}$	3284 _n	3285 _n	3286 _n	3287 _n	3288 _n
$\frac{1}{36}$	3260 _n	3261 _n	3262 _n	3263 _n	3264 _n
$\frac{1}{37}$	3239 _n	3240 _n	3241 _n	3242 _n	3243 _n
$\frac{1}{38}$	3221 _n	3222 _n	3223 _n	3224 _n	3225 _n
$\frac{1}{39}$	3205 _n	3206 _n	3207 _n	3208 _n	3209 _n
$\frac{1}{40}$	3191 _n	3192 _n	3193 _n	3194 _n	3195 _n
$\frac{1}{41}$	3178 _n	3179 _n	3180 _n	3181 _n	3182 _n
$\frac{1}{42}$	3166 _n	3167 _n	3168 _n	3169 _n	3170 _n
$\frac{1}{43}$	3155 _n	3156 _n	3157 _n	3158 _n	3159 _n
$\frac{1}{44}$	3145 _n	3146 _n	3147 _n	3148 _n	3149 _n
$\frac{1}{45}$	3136 _n	3137 _n	3138 _n	3139 _n	3140 _n
$\frac{1}{46}$	3127 _n	3128 _n	3129 _n	3130 _n	3131 _n
$\frac{1}{47}$	3119 _n	3120 _n	3121 _n	3122 _n	3123 _n
$\frac{1}{48}$	3111 _n	3112 _n	3113 _n	3114 _n	3115 _n
$\frac{1}{49}$	3104 _n	3105 _n	3106 _n	3107 _n	3108 _n
$\frac{1}{50}$	3097 _n	3098 _n	3099 _n	3100 _n	3101 _n
$\frac{1}{51}$	3090 _n	3091 _n	3092 _n	3093 _n	3094 _n
$\frac{1}{52}$	3084 _n	3085 _n	3086 _n	3087 _n	3088 _n
$\frac{1}{53}$	3078 _n	3079 _n	3080 _n	3081 _n	3082 _n
$\frac{1}{54}$	3072 _n	3073 _n	3074 _n	3075 _n	3076 _n
$\frac{1}{55}$	3066 _n	3067 _n	3068 _n	3069 _n	3070 _n
$\frac{1}{56}$	3060 _n	3061 _n	3062 _n	3063 _n	3064 _n
$\frac{1}{57}$	3054 _n	3055 _n	3056 _n	3057 _n	3058 _n
$\frac{1}{58}$	3048 _n	3049 _n	3050 _n	3051 _n	3052 _n
$\frac{1}{59}$	3042 _n	3043 _n	3044 _n	3045 _n	3046 _n
$\frac{1}{60}$	3036 _n	3037 _n	3038 _n	3039 _n	3040 _n
$\frac{1}{61}$	3030 _n	3031 _n	3032 _n	3033 _n	3034 _n
$\frac{1}{62}$	3024 _n	3025 _n	3026 _n	3027 _n	3028 _n
$\frac{1}{63}$	3018 _n	3019 _n	3020 _n	3021 _n	3022 _n
$\frac{1}{64}$	3012 _n	3013 _n	3014 _n	3015 _n	3016 _n
$\frac{1}{65}$	3006 _n	3007 _n	3008 _n	3009 _n	3010 _n
$\frac{1}{66}$	3000 _n	3001 _n	3002 _n	3003 _n	3004 _n
$\frac{1}{67}$	2994 _n	2995 _n	2996 _n	2997 _n	2998 _n
$\frac{1}{68}$	2988 _n	2989 _n	2990 _n	2991 _n	2992 _n
$\frac{1}{69}$	2982 _n	2983 _n	2984 _n	2985 _n	2986 _n
$\frac{1}{70}$	2976 _n	2977 _n	2978 _n	2979 _n	2980 _n
$\frac{1}{71}$	2970 _n	2971 _n	2972 _n	2973 _n	2974 _n
$\frac{1}{72}$	2964 _n	2965 _n	2966 _n	2967 _n	2968 _n
$\frac{1}{73}$	2958 _n	2959 _n	2960 _n	2961 _n	2962 _n
$\frac{1}{74}$	2952 _n	2953 _n	2954 _n	2955 _n	2956 _n
$\frac{1}{75}$	2946 _n	2947 _n	2948 _n	2949 _n	2950 _n
$\frac{1}{76}$	2940 _n	2941 _n	2942 _n	2943 _n	2944 _n
$\frac{1}{77}$	2934 _n	2935 _n	2936 _n	2937 _n	2938 _n
$\frac{1}{78}$	2928 _n	2929 _n	2930 _n	2931 _n	2932 _n
$\frac{1}{79}$	2922 _n	2923 _n	2924 _n	2925 _n	2926 _n
$\frac{1}{80}$	2916 _n	2917 _n	2918 _n	2919 _n	2920 _n
$\frac{1}{81}$	2910 _n	2911 _n	2912 _n	2913 _n	2914 _n
$\frac{1}{82}$	2904 _n	2905 _n	2906 _n	2907 _n	2908 _n
$\frac{1}{83}$	2898 _n	2899 _n	2900 _n	2901 _n	2902 _n
$\frac{1}{84}$	2892 _n	2893 _n	2894 _n	2895 _n	2896 _n
$\frac{1}{85}$	2886 _n	2887 _n	2888 _n	2889 _n	2890 _n
$\frac{1}{86}$	2880 _n	2881 _n	2882 _n	2883 _n	2884 _n
$\frac{1}{87}$	2874 _n	2875 _n	2876 _n	2877 _n	2878 _n
$\frac{1}{88}$	2868 _n	2869 _n	2870 _n	2871 _n	2872 _n
$\frac{1}{89}$	2862 _n	2863 _n	2864 _n	2865 _n	2866 _n
$\frac{1}{90}$	2856 _n	2857 _n	2858 _n	2859 _n	2860 _n
$\frac{1}{91}$	2850 _n	2851 _n	2852 _n	2853 _n	2854 _n
$\frac{1}{92}$	2844 _n	2845 _n	2846 _n	2847 _n	2848 _n
$\frac{1}{93}$	2838 _n	2839 _n	2840 _n	2841 _n	2842 _n
$\frac{1}{94}$	2832 _n	2833 _n	2834 _n	2835 _n	2836 _n
$\frac{1}{95}$	2826 _n	2827 _n	2828 _n	2829 _n	2830 _n
$\frac{1}{96}$	2820 _n	2821 _n	2822 _n	2823 _n	2824 _n
$\frac{1}{97}$	2814 _n	2815 _n	2816 _n	2817 _n	2818 _n
$\frac{1}{98}$	2808 _n	2809 _n	2810 _n	2811 _n	2812 _n
$\frac{1}{99}$	2802 _n	2803 _n	2804 _n	2805 _n	2806 _n
$\frac{1}{100}$	2796 _n	2797 _n	2798 _n	2799 _n	2800 _n

	acc. 7c	acc. 7c	acc. 7c	acc. 7c	acc. 7c
$\cos \frac{1}{2} \frac{dx}{dt}$	0.45731	0.35591	0.30565	0.28270	0.16111
$\sin \frac{1}{2} \frac{dx}{dt}$	0.00282	0.00731	0.05004	0.24553	0.50286
$\cos \frac{1}{2} \frac{dx}{dt}$	0.10235	0.08754	0.03612	0.02553	0.55506
$\sin \frac{1}{2} \frac{dx}{dt}$	0.26005	0.30010	0.30693	0.30621	0.20645
$\cos \frac{1}{2} \frac{dx}{dt}$	0.36164	0.32211	0.20000	0.20000	0.66207
$\sin \frac{1}{2} \frac{dx}{dt}$	0.20142	0.20000	0.24300	0.23170	0.15451
$\cos \frac{1}{2} \frac{dx}{dt}$	0.04227	0.00000	0.00450	0.00000	0.01290
$\sin \frac{1}{2} \frac{dx}{dt}$	0.24546	0.20000	0.23855	0.23093	0.19742
	+0.22577	+1.87220	+1.73200	+1.01990	+1.57550
$\cos \frac{1}{2} \frac{dx}{dt}$	0.05457	0.00000	0.86094	0.53455	0.62511
$\sin \frac{1}{2} \frac{dx}{dt}$	0.00282	0.00731	0.05004	0.24553	0.50286
$\cos \frac{1}{2} \frac{dx}{dt}$	0.10235	0.08754	0.03612	0.02553	0.27341
$\sin \frac{1}{2} \frac{dx}{dt}$	0.26005	0.30010	0.30693	0.30621	0.20645
$\cos \frac{1}{2} \frac{dx}{dt}$	0.36164	0.32211	0.20000	0.20000	0.12707
$\sin \frac{1}{2} \frac{dx}{dt}$	0.04227	0.00000	0.00450	0.00000	0.56456
$\cos \frac{1}{2} \frac{dx}{dt}$	0.04227	0.00000	0.00516	0.00000	0.01542
$\sin \frac{1}{2} \frac{dx}{dt}$	0.04335	0.00212	0.04827	0.00000	0.55525
	+0.57776	+0.66547	+0.55370	+0.50527	+0.38484
$\cos \frac{1}{2} \frac{dx}{dt}$	0.45731	0.35591	0.30565	0.28270	0.16111
$\sin \frac{1}{2} \frac{dx}{dt}$	0.00282	0.00731	0.05004	0.24553	0.50286
$\cos \frac{1}{2} \frac{dx}{dt}$	0.10235	0.08754	0.03612	0.02553	0.55506
$\sin \frac{1}{2} \frac{dx}{dt}$	0.26005	0.30010	0.30693	0.30621	0.20645
$\cos \frac{1}{2} \frac{dx}{dt}$	0.36164	0.32211	0.20000	0.20000	0.66207
$\sin \frac{1}{2} \frac{dx}{dt}$	0.04227	0.00000	0.00450	0.00000	0.01290
$\cos \frac{1}{2} \frac{dx}{dt}$	0.04227	0.00000	0.00516	0.00000	0.01542
$\sin \frac{1}{2} \frac{dx}{dt}$	0.04335	0.00212	0.04827	0.00000	0.55525
	+1.55764	+1.13795	+0.07142	+0.03770	+0.51255

	1952 Jan 1	1952 Jan 11.5	1952 Jan 21	1952 Jan 31	mean 1952
$\frac{d^2}{dt^2}$	0.05457	8.95152	8.86994	8.82435	8.62511
$\frac{d^2}{dt^2} \frac{d}{d\lambda}$	0.40086	0.51625	0.52224	0.51229	0.51790
$\frac{d^2}{dt^2} \frac{d^2}{d\lambda^2}$	0.70010	0.54059	0.44150	0.41516	0.27341
$\frac{d^2}{dt^2} \frac{d^3}{d\lambda^3}$	0.00152	0.03664	0.02012	0.01554	0.00551
$\frac{d^2}{dt^2} \frac{d^4}{d\lambda^4}$	8.54542	5.49527	5.39215	0.35714	8.14201
$\frac{d^2}{dt^2} \frac{d^5}{d\lambda^5}$	0.76162	0.57722	0.46162	0.43100	0.26592
$\frac{d^2}{dt^2} \frac{d^6}{d\lambda^6}$	0.02563	0.03476	0.03552	0.03517	0.03134
$\frac{d^2}{dt^2} \frac{d^7}{d\lambda^7}$	0.78725	0.61104	0.49714	0.46617	0.30026
	+0.61270	+0.40925	+0.31415	+0.29253	+0.19965
$\frac{d^2}{dt^2} \frac{d^8}{d\lambda^8}$	0.45781	0.38891	0.30367	0.28270	0.16111
$\frac{d^2}{dt^2} \frac{d^9}{d\lambda^9}$	2.42210 _n	2.41627 _n	2.41192 _n	2.41073 _n	2.40565 _n
$\frac{d^2}{dt^2} \frac{d^{10}}{d\lambda^{10}}$	0.10538	0.07784	0.03612	0.02558	0.88806
$\frac{d^2}{dt^2} \frac{d^{11}}{d\lambda^{11}}$	1.43250 _n	1.00734	1.55794	1.62330	1.83749
$\cos \theta \frac{d^2}{dt^2} \frac{d^2}{d\lambda} \frac{d^2}{d\lambda}$	1.85000 _n	1.80218 _n	1.71760 _n	1.6742 _n	1.56676 _n
$\cos \theta \frac{d^2}{dt^2} \frac{d^2}{d\lambda} \frac{d^2}{d\lambda}$	1.53797 _n	1.05118	1.40406	1.54587	1.72555
$\frac{d^2}{dt^2} \frac{d^2}{d\lambda} \frac{d^2}{d\lambda}$	0.16245	0.09252	0.39541	0.54804	0.51391
$\cos \theta \frac{d^2}{dt^2} \frac{d^2}{d\lambda}$	2.04288 _n	1.70166 _n	1.32228 _n	1.14539 _n	1.21165
	-110.270	-51.2462	-21.0030	-13.9761	-16.2794
$\frac{d^2}{dt^2}$	0.05457	8.95152	8.86994	8.82435	8.62511
$\frac{d^2}{dt^2} \frac{d}{d\lambda}$	2.42210 _n	2.41627 _n	2.41192 _n	2.41073 _n	2.40565 _n
$\frac{d^2}{dt^2} \frac{d^2}{d\lambda}$	0.70010	0.54059	0.44150	0.41516	0.27341
$\frac{d^2}{dt^2} \frac{d^3}{d\lambda}$	1.43250 _n	1.00734	1.55794	1.62330	1.83749
$\frac{d^2}{dt^2} \frac{d^4}{d\lambda}$	1.47676 _n	1.39809 _n	1.25186 _n	1.24528 _n	1.03076 _n
$\frac{d^2}{dt^2} \frac{d^5}{d\lambda}$	1.13261 _n	0.63742	0.99944	1.03846	1.11696
$\frac{d^2}{dt^2} \frac{d^6}{d\lambda}$	0.16221	0.08287	0.32047	0.42150	0.77330
$\frac{d^2}{dt^2} \frac{d^7}{d\lambda}$	1.63897 _n	1.31522 _n	0.96139 _n	0.62377 _n	0.33751
	-43.548	-20.6646	-0.14940	-6.6648	-2.17525

	Nov. 1895	Nov. 1895	Nov. 1895	Nov. 1895
9.31303 _n	9.25571 _n	9.2746 _n	9.1944 _n	9.09565 _n
9.83116 _n	9.86207 _n	9.80065 _n	9.46220 _n	9.00000 _n
9.14509	9.18118	9.16527	9.16464	9.14067
8.83309 _n	8.70114 _n	8.74527 _n	8.60274 _n	8.45285 _n
0.22005	0.22691	0.22360	0.21182	0.19176
9.06304 _n	9.01505 _n	8.96877 _n	8.81456 _n	8.64461 _n
0.00964	0.00739	0.00340	9.05180	9.93601
9.83550	9.83135	9.82650	9.80992	9.78290
9.84553	9.82874	9.82090	9.79132	9.71591
9.21142 _n	9.29571 _n	9.27462 _n	9.19944 _n	9.09560 _n
7.11616 _n	7.11707 _n	7.13565 _n	7.16000 _n	7.18498 _n
6.43009	6.41278	6.41027	6.35064	6.28067
5.83300 _n	5.70114 _n	5.74527 _n	5.60274 _n	5.45285 _n
5.29587 _n	5.30913 _n	5.32508 _n	5.36362 _n	5.40707 _n
7.12956	7.10027	7.07025	6.96636	6.85992
6.00944	6.00739	6.00340	6.08180	6.03601
5.62172	5.64855	5.66464	5.70792	5.75603
5.61136	5.65624	5.66804	5.68081	5.69264
9.31303 _n	9.29571 _n	9.27462 _n	9.19944 _n	9.09560 _n
9.83116 _n	9.86207 _n	9.80065 _n	9.46220 _n	9.00000 _n
9.14509	9.08582	9.05607	9.05506	9.01116
8.83309 _n	8.70114 _n	8.74527 _n	8.60274 _n	8.45285 _n
8.75736 _n	8.78011 _n	8.77227 _n	8.74650 _n	8.70245 _n
8.62145	8.71155	8.71777	8.734026	8.75500
0.00964	0.00739	0.00340	0.08180	0.02601
0.16340	0.12605	0.13400	0.12246	0.05101
0.15201	0.10244	0.10160	0.10435	0.01740

$\frac{dx}{dt}$
 $\frac{dy}{dt}$
 $\frac{dz}{dt}$
 $\frac{dw}{dt}$
 $\frac{v}{dt}$
 $\frac{u}{dt}$

$\frac{dx}{dt}$
 $\frac{dy}{dt}$
 $\frac{dz}{dt}$
 $\frac{dw}{dt}$
 $\frac{v}{dt}$
 $\frac{u}{dt}$

$\frac{dx}{dt}$
 $\frac{dy}{dt}$
 $\frac{dz}{dt}$
 $\frac{dw}{dt}$
 $\frac{v}{dt}$
 $\frac{u}{dt}$

Oct. 12.5	Oct. 16.5	Oct. 20.5	Nov. 1.5	Nov. 11.5
+ 0.13066	+ 0.14381	+ 0.14631	+ 0.14610	+ 0.13825
- 0.11576	- 0.10424	- 0.09308	- 0.06825	- 0.04411
+ 0.71171	+ 0.65051	+ 0.67593	+ 0.61018	+ 0.52340
+ 0.71450	+ 0.72030	+ 0.72916	+ 0.71111	+ 0.61763
4.56001	+ 9.86099	9.86282	9.86111	9.99070
+ 0.00027	+ 0.00026	+ 0.00026	+ 0.00021	+ 0.00019
+ 0.00125	+ 0.00126	+ 0.00118	+ 0.00093	+ 0.00072
+ 0.04379	+ 0.04532	+ 0.04656	+ 0.04806	+ 0.04921
+ 0.04541	+ 0.04654	+ 0.04800	+ 0.05012	+ 0.05012
- 0.01207	+ 0.01215	+ 0.01140	+ 0.00003	+ 0.00647
+ 0.04152	+ 0.03726	+ 0.03203	+ 0.02235	+ 0.01440
+ 1.45050	+ 1.45603	+ 1.41805	+ 1.27160	+ 1.04093
+ 1.54425	+ 1.50638	+ 1.46228	+ 1.30245	+ 1.06180

Dec 25	1888 Jan 15	Feb 15	Mar 15	Mar. 15
+0.1522	+0.15611	+0.17174	+0.17407	+0.16964
-0.07050	-0.04664	-0.05586	-0.05762	-0.05848
+0.0201	+0.02740	+0.06040	+0.04265	+0.07652
+0.0120	+0.04250	+0.05165	+0.26011	+0.18268
0.0010	0.54059	0.44150	0.41516	0.27241
+0.00017	+0.00017	+0.00017	+0.00016	+0.00014
+0.00072	+0.00128	+0.00187	+0.00206	+0.00208
+0.04671	+0.04024	+0.02621	+0.07524	+0.03108
+0.04760	+0.04166	+0.03225	+0.02746	+0.00417
+0.00457	+0.00291	+0.00196	+0.00170	+0.00045
+0.01119	+0.01176	+0.01139	+0.01084	+0.00455
+0.07667	+0.09418	+0.02229	+0.19114	+0.04835
+0.07823	+0.40886	+0.24065	+0.0268	+0.05336

We now send the following

Differential equations of condition in which the coefficients are
expressed in logarithms -

$\cos \delta \Delta u$

0.25 0.49 4π	8.232286 _m	$\Delta \delta$	9.76910 _m	Δi	0.47955	Δq	0.27811	Δu	0
0.27 7.55	8.20622 _m		9.7618 _m		0.47715		0.27510	2.27536 _m	
0.27 2.77	8.20911 _m		9.75231 _m		0.47375		0.26965	2.27157 _m	
0.24 10.64	8.2110 _m		9.76174 _m		0.45130		0.27129	2.27471 _m	
0.18 6.24	8.22085 _m		9.62408 _m		0.4655		0.27087	2.27635 _m	

0.10538 4π	8.2008 _m	$\Delta \delta$	9.48620 _m	Δi	0.24886	Δq	0.19244	Δu	0
0.10 7.11	8.2052 _m		9.47406 _m		0.2501		0.05607	1.70966 _m	
0.10 6.12	8.1907 _m		8.89931 _m		0.23855		0.17741	1.2228 _m	
0.09 2.58	8.1012 _m		8.81140 _m		0.2002		0.07206	1.14539 _m	
0.08 5.06	8.06621 _m		8.12501 _m		0.19242		0.09987	1.24463 _m	

Δi

0.56004 4π	8.65715 _m	$\Delta \delta$	0.14871	Δi	0.04024	Δq	0.05299	Δu	0
0.50247	8.67062 _m		0.17792		0.08147		0.05775	1.17149 _m	
0.86283	8.68124		0.16506		0.08094		0.05545	1.80396 _m	
0.44512	8.70001		0.11494		0.06324		0.03741	1.80206 _m	
0.44072	8.70001		0.05544		0.0584		0.05185	1.55244 _m	

0.70010 4π	8.67761	$\Delta \delta$	0.80122	Δi	0.04335	Δq	0.078725	Δu	0
0.54059	8.61972		0.61157		0.82313		0.61199	1.31522 _m	
0.44150	8.52262		0.58138		0.74021		0.5714	1.110 _m	
0.41516	8.57357		0.30845		0.72038		0.46617	0.82271 _m	
0.27341	8.53364		8.72722		0.58525		0.30026	0.32751 _m	

Substituting in the preceding equations the calculated values, and substituting in the above coefficients, in numbers we have the following equations of condition from which to find the normal equations

[illegible]

In order to have these equations of condition more symmetrical and of a simpler form for calculation we make the following transformations in accordance with the equations:

$$h \Delta_{-1}^{+1} = h \Delta_{-1} M - \pi \Delta \mu$$

$$\Delta_{-1} M' = \Delta_{-1} M + \frac{h}{k} \Delta \mu$$

$$h \Delta_{-1}^{+2} = h \Delta i - h \Delta \delta$$

$$\Delta \delta' = \Delta \delta + \frac{h}{k} \Delta i$$

etc. etc.;

and

$$0.42169 u = 0.42169 \Delta i + 0.02142 \Delta \delta$$

$$u = \Delta i + [8.70583] \Delta \delta$$

$$\Delta i = u - [8.70583] \Delta \delta;$$

also

$$1.90491 t = 1.90491 \Delta M_0 + 2.55185 \Delta \varphi + 1.53789 \Delta \pi - 150.010 \Delta \mu$$

$$t = \Delta M_0 + [0.12698] \Delta \varphi + [9.90697] \Delta \pi - [89.65] \Delta \mu$$

$$\Delta M_0 = t - [0.12698] \Delta \varphi - [9.90697] \Delta \pi + [89.65] \Delta \mu$$

etc. etc.;

which will give the following transformed equations:

$+ 1.255552$	$- 0.15294 \Delta y$	$- 0.02040 \Delta \pi$	$- 0.553 \Delta u$	$- 0.58762 u$	$+ 0.01067 \Delta \delta$	$= + 0.60$	11
$+ 1.37200$	$- 0.17332$	$- 0.01452$	$- 1.505$	$- 0.57794$	$+ 0.00055$	$= + 1.07$	9
$+ 1.34234$	$- 0.16116$	$- 0.01674$	$- 2.445$	$- 0.56534$	$+ 0.00530$	$= + 1.20$	6
$+ 1.18920$	$- 0.10583$	$- 0.01058$	$- 2.199$	$- 0.51225$	$+ 0.00460$	$= + 3.30$	6
$+ 1.0491$	0.00000	0.00000	0.000	$- 0.42169$	0.00000	$= + 1.01$	3
$+ 1.55764$	$+ 0.14621 \Delta y$	$+ 0.01731 \Delta \pi$	$+ 12.369 \Delta u$	$- 0.30640 u$	$- 0.00443 \Delta \delta$	$= + 1.76$	5
$- 1.13779$	$+ 0.24902$	$+ 0.03071$	$+ 38.410$	$- 0.14930$	$- 0.00057$	$= + 2.32$	4
$+ 0.97142$	$+ 0.43067$	$+ 0.07910$	$+ 55.542$	$- 0.07930$	$- 0.00057$	$= - 0.75$	2
$- 0.92770$	$+ 0.44576$	$+ 0.05564$	$+ 50.510$	$- 0.06475$	$- 0.00042$	$= + 0.94$	3
$+ 0.51258$	$+ 0.44700$	$+ 0.11653$	$+ 50.309$	$- 0.01334$	$- 0.00955$	$= - 0.15$	1

$- 0.50740$	$+ 0.00000 \Delta y$	$+ 0.00013 \Delta \pi$	$+ 9.492 \Delta u$	$+ 1.54725 u$	$- 0.03303 \Delta \delta$	$= + 0.97$	10
$- 0.90312$	$- 0.00205$	$+ 0.00040$	$+ 8.473$	$+ 1.50638$	$- 0.02065$	$= + 1.20$	9
$+ 0.90256$	$- 0.00422$	$+ 0.00063$	$+ 7.446$	$+ 1.46235$	$- 0.02623$	$= + 0.90$	8
$+ 0.96578$	$- 0.00310$	$+ 0.00119$	$+ 4.650$	$+ 1.30205$	$- 0.01607$	$= + 1.27$	7
$+ 0.26152$	$- 0.01656$	$+ 0.00270$	$+ 2.736$	$+ 1.06190$	$- 0.00369$	$= + 0.23$	4
$- 0.61270$	$+ 0.05605 \Delta y$	$+ 0.00674 \Delta \pi$	$+ 4.731 \Delta u$	$+ 0.77543 u$	$+ 0.00507 \Delta \delta$	$= + 0.26$	5
$+ 0.41741$	$+ 0.11723$	$+ 0.01656$	$+ 11.573$	$+ 0.40556$	$+ 0.02059$	$= + 0.75$	4
$- 0.11117$	$+ 0.12786$	$- 0.02271$	$+ 15.625$	$+ 0.24065$	$+ 0.03603$	$= + 1.70$	1
$+ 0.20253$	$+ 0.13340$	$+ 0.02309$	$+ 16.385$	$+ 0.20365$	$+ 0.02711$	$= - 1.73$	3
$+ 0.19065$	$+ 0.11730$	$+ 0.02653$	$+ 17.907$	$+ 0.05336$	$+ 0.03146$	$= - 2.60$	1

Substituting in these equations $x = 10^{-10}$, $y = \Delta \pi = 100$, $u = \Delta \delta = 100$, we get the following simplified forms of the equations for solution:

+ 23.94	- 18.38	- 2.049	- 0.662	- 0.594	+ 1.77W	= + 0.60	10
+ 23.77	- 17.3	- 1.85	- 0.16	- 0.55	+ 0.96	= + 1.97	9
+ 23.4	- 16.1	- 1.67	- 0.24	- 0.57	+ 0.88	= + 1.9	8
+ 23.11	- 15.0	- 1.46	- 0.32	- 0.51	+ 0.90	= + 2.0	7
+ 1.04			- 0.42			= + 1.04	6
+ 1.54	+ 14.68	+ 1.739	+ 1.247	- 0.311	- 0.44W	= + 1.6	5
+ 1.14	+ 14.0	+ 1.46	+ 1.384	- 0.15	- 0.56	= + 2.35	4
+ 0.97	+ 13.1	+ 1.01	+ 1.55	- 0.08	- 0.94	= - 0.75	3
+ 0.94	+ 12.46	+ 1.56	+ 1.948	- 0.06	- 0.94	= + 0.94	2
+ 0.91	+ 11.7	+ 1.16	+ 1.803	- 0.01	- 0.86	= - 0.15	1

+ 0.88	+ 10.12	+ 0.19	+ 0.92	+ 1.54W	- 2.0W	= + 0.11	10
+ 0.8	+ 9.22	+ 0.04	+ 0.85	+ 1.51	- 2.07	= + 1.20	9
+ 0.72	+ 8.34	+ 0.06	+ 0.74	+ 1.46	- 2.63	= + 0.90	8
+ 0.67	+ 7.43	+ 0.12	+ 0.47	+ 1.30	- 1.61	= + 1.27	7
+ 0.61	+ 6.57	+ 0.27	+ 0.28	+ 1.06	- 0.37	= + 0.23	6
+ 0.51	+ 5.78	+ 0.67	+ 0.47	+ 0.79W	+ 0.51W	= + 0.51	5
+ 0.42	+ 4.97	+ 1.07	+ 1.16	+ 0.41	+ 2.09	= + 2.09	4
+ 0.31	+ 4.13	+ 1.58	+ 1.50	+ 0.24	- 0.60	= + 2.60	3
+ 0.21	+ 3.28	+ 2.2	+ 1.64	+ 0.20	+ 2.71	= + 2.71	2
+ 0.12	+ 2.47	+ 3.07	+ 1.79	+ 0.05	+ 3.15	= + 3.15	1

Next Third

Fourth Perturbations of (α) by Jupiter

Thus far we have proceeded to determine the elements of the planet as they would be if the motion were undisturbed. But a complete determination of the orbit requires the consideration of ~~any~~ ^{any} ~~any~~ that may be produced in the planet's motion by a disturbing force. Owing to their relative positions, it becomes necessary to take into account the perturbations arising from the disturbing influence of Jupiter.

Thus before applying the values which we have obtained, $\Delta\alpha$ and $\Delta\delta$ by substituting them in ~~our equation~~ ^{our equation} of condition and solving to determine the ~~error~~ ^{error} they produce upon the values of the elements, we will first compute the perturbations by Jupiter directly for the elements.

When combining the perturbations in the constants already obtained with the result in the equations of condition and solving to find the corrections, they will give the final elements.

Let δ be the numerical values which represent the disturbing force of the planet Jupiter for every forty days. These values can then be found for the times for which the equations of condition are found by numerical integration.

The numerical values of the constants which we have occasion to use are already known from the preceding investigation.

The formulas used in the computation of the perturbations are as follows:

Section XVI.

$$\alpha^{3/2} = \frac{2\pi}{u} \quad , \quad \log \alpha'' = 2.550007$$

$$\epsilon'' = \frac{\sin q}{\sin \epsilon} \quad \log \frac{1}{\alpha''} = 5.214425$$

$$M_1 = L - \pi$$

$$E'' - \cos \epsilon E'' = M_1$$

$$r \sin v = u \cos q \sin E$$

$$r \cos v = u (\cos E - \sin q)$$

$$\omega = \pi - \delta b$$

$$u = v + w$$

$$p = u \cos^2 \gamma$$

$$\{i:W\} = r \cos u$$

$$\{b:W\} = \frac{r \sin u}{s+1}$$

$$\{u:R\} = -\frac{2ku}{7a} \sin q \sin v; \quad w = 40.$$

$$\{u:\beta\} = -\frac{2ku}{7a} \cdot \frac{b}{r}$$

$$\{b:R\} = \frac{2ku}{7a} \sin q \cos v - r \cos \gamma$$

$$\{b:\beta\} = (1+r) \sin v \cos \gamma$$

$$\{b:u\} = r \sin u \tan \frac{1}{2} i$$

$$\{3T:R\} = -\frac{b}{\sin \gamma} \cos \epsilon$$

$$\{u, v\} = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial}{\partial r} \right)$$

$$\{u, v\} = u \cos \varphi \sin \varphi$$

$$\{u, v\} = u \cos \varphi [\cos \varphi + \cos \varepsilon].$$

Let δ be the

distance between the two points, δ is the distance between the

two points, δ is the distance between the

two points, δ is the distance between the

two points, δ is the mass of the disturbing planet.

$$u \sin \alpha = \sin \beta$$

$$u \cos \alpha = \cos \beta \sin (\beta' - \beta)$$

$$\cos B, \cos b = \cos \beta' \cos (\beta' - \beta)$$

$$\cos B, \sin b = u \cos (\alpha - i)$$

$$\sin B = u \sin (\alpha - i)$$

$$x = r \cos B, \cos (b - u)$$

$$y = r \cos B, \sin (b - u)$$

$$z = r \sin B$$

$$\xi \cos \delta \cos \Theta = \xi_1 \cos \delta_1$$

$$\xi \cos \delta \sin \Theta = \eta_1$$

$$\xi \sin \delta = \xi_1 \sin \delta_1$$

$$K = \frac{1}{\xi} - \frac{1}{\xi_1}$$

$$\tilde{A}_0 = K_1 \xi - \frac{c}{\xi}$$

$$\tilde{S}'_0 = K w_0$$

$$W_0 = K \xi_1$$

$$R = \left(\frac{u + \sqrt{u^2 - m_1^2}}{1 + \sqrt{1 - m_1^2}} \right) R_1$$

$$\tilde{S}' = \left(\frac{u + \sqrt{u^2 - m_1^2}}{1 + \sqrt{1 - m_1^2}} \right) S_0$$

$$W = \left(\frac{u + \sqrt{u^2 - m_1^2}}{1 + \sqrt{1 - m_1^2}} \right) W_0$$

$$\Delta i = \{i : W\} W$$

$$\Delta \Omega = \{\Omega : W\} W$$

$$w \Delta_i u = \{u : R\} R + \{u : S\} S$$

$$\Delta L_i = \{L : R\} R + \{L : S\} S + \{L : W\} W$$

$$\Delta \pi = \{\pi : R\} R + \{\pi : S\} S + \{L : W\} W$$

$$\Delta \varphi = \{\varphi : R\} R + \{\varphi : S\} S$$

Combinations for the Determinations by Jupiter.

1887, 1888, 1889.

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

" " " " " "

1887	Oct 22	Nov 22	Dec 10	Feb 10
1	24 11.7	24 11.7	45° 22.7	60° 29.7
2	24 11.7	24 11.7	55 25.1	68 29.0
3	24 11.7	24 11.7		
4	24 11.7	24 11.7		
5	24 11.7	24 11.7		
6	24 11.7	24 11.7		
7	24 11.7	24 11.7		
8	24 11.7	24 11.7		
9	24 11.7	24 11.7		
10	24 11.7	24 11.7		
11	24 11.7	24 11.7		
12	24 11.7	24 11.7		
13	24 11.7	24 11.7		
14	24 11.7	24 11.7		
15	24 11.7	24 11.7		
16	24 11.7	24 11.7		
17	24 11.7	24 11.7		
18	24 11.7	24 11.7		
19	24 11.7	24 11.7		
20	24 11.7	24 11.7		
21	24 11.7	24 11.7		
22	24 11.7	24 11.7		
23	24 11.7	24 11.7		
24	24 11.7	24 11.7		
25	24 11.7	24 11.7		
26	24 11.7	24 11.7		
27	24 11.7	24 11.7		
28	24 11.7	24 11.7		
29	24 11.7	24 11.7		
30	24 11.7	24 11.7		
31	24 11.7	24 11.7		
32	24 11.7	24 11.7		
33	24 11.7	24 11.7		
34	24 11.7	24 11.7		
35	24 11.7	24 11.7		
36	24 11.7	24 11.7		
37	24 11.7	24 11.7		
38	24 11.7	24 11.7		
39	24 11.7	24 11.7		
40	24 11.7	24 11.7		
41	24 11.7	24 11.7		
42	24 11.7	24 11.7		
43	24 11.7	24 11.7		
44	24 11.7	24 11.7		
45	24 11.7	24 11.7		
46	24 11.7	24 11.7		
47	24 11.7	24 11.7		
48	24 11.7	24 11.7		
49	24 11.7	24 11.7		
50	24 11.7	24 11.7		
51	24 11.7	24 11.7		
52	24 11.7	24 11.7		
53	24 11.7	24 11.7		
54	24 11.7	24 11.7		
55	24 11.7	24 11.7		
56	24 11.7	24 11.7		
57	24 11.7	24 11.7		
58	24 11.7	24 11.7		
59	24 11.7	24 11.7		
60	24 11.7	24 11.7		
61	24 11.7	24 11.7		
62	24 11.7	24 11.7		
63	24 11.7	24 11.7		
64	24 11.7	24 11.7		
65	24 11.7	24 11.7		
66	24 11.7	24 11.7		
67	24 11.7	24 11.7		
68	24 11.7	24 11.7		
69	24 11.7	24 11.7		
70	24 11.7	24 11.7		
71	24 11.7	24 11.7		
72	24 11.7	24 11.7		
73	24 11.7	24 11.7		
74	24 11.7	24 11.7		
75	24 11.7	24 11.7		
76	24 11.7	24 11.7		
77	24 11.7	24 11.7		
78	24 11.7	24 11.7		
79	24 11.7	24 11.7		
80	24 11.7	24 11.7		
81	24 11.7	24 11.7		
82	24 11.7	24 11.7		
83	24 11.7	24 11.7		
84	24 11.7	24 11.7		
85	24 11.7	24 11.7		
86	24 11.7	24 11.7		
87	24 11.7	24 11.7		
88	24 11.7	24 11.7		
89	24 11.7	24 11.7		
90	24 11.7	24 11.7		
91	24 11.7	24 11.7		
92	24 11.7	24 11.7		
93	24 11.7	24 11.7		
94	24 11.7	24 11.7		
95	24 11.7	24 11.7		
96	24 11.7	24 11.7		
97	24 11.7	24 11.7		
98	24 11.7	24 11.7		
99	24 11.7	24 11.7		
100	24 11.7	24 11.7		

18.8.8.

July 19.0

Aug 20.0

Oct 21.0

Nov 16.0

 ϕ $120^\circ 59.6$ $138^\circ 01.0$ $145^\circ 11.6$ $153^\circ 39.2$

E

 12.1 13.8 14.9 16.0 $\sin \delta$ 0.80752 0.81906 0.76449 0.72121 $\cos \delta$ 0.791712 0.57616 0.64552 0.69021 δ 0.07501 0.07501 0.07501 0.06419 $\cos E$ 0.94322 0.94322 0.94322 0.94322 $\sin E$ 0.23447 0.15012 0.08185 0.08185 $\cos \delta$ 0.791712 0.57616 0.64552 0.69021 $\sin \delta$ 0.80752 0.81906 0.76449 0.72121 $\cos \delta$ 0.791712 0.57616 0.64552 0.69021 $\sin \delta$ 0.80752 0.81906 0.76449 0.72121 δ 0.07501 0.07501 0.07501 0.06419 δ 0.07501 0.07501 0.07501 0.06419 $\cos \delta$ 0.94322 0.94322 0.94322 0.94322 $\sin \delta$ 0.07501 0.07501 0.07501 0.06419 $\cos \delta$ 0.94322 0.94322 0.94322 0.94322 $\sin \delta$ 0.07501 0.07501 0.07501 0.06419 δ 0.07501 0.07501 0.07501 0.06419 δ 0.07501 0.07501 0.07501 0.06419 $\cos \delta$ 0.94322 0.94322 0.94322 0.94322 $\sin \delta$ 0.07501 0.07501 0.07501 0.06419 δ 0.07501 0.07501 0.07501 0.06419 $\sin \delta$ 0.80752 0.81906 0.76449 0.72121 $[1+\delta]\sin \delta$ 0.51259 0.51259 0.51259 0.51259 $\sin \delta \sin \delta$ 0.03044 0.03044 0.03044 0.03044 $\cos \delta$ 0.94322 0.94322 0.94322 0.94322 δ 0.07501 0.07501 0.07501 0.06419 $\cos \delta + \cos E$ 0.11760 0.11760 0.11760 0.11760 $\sin \delta$ 0.80752 0.81906 0.76449 0.72121 $\sin \delta \sin \delta$ 0.03044 0.03044 0.03044 0.03044 δ 0.07501 0.07501 0.07501 0.06419

	1950-50.3	1951-51.0	1952-52.7	1953-53.4
$\{1:W\}$	0.5288 _m	0.06080 _m	0.1720 _m	0.1733 _m
$\{2:W\}$	1.0212 _m	1.55361	1.48947	1.1212 _m
$\{3:W\}$	1.0512 _m	0.109165 _m	0.26890 _m	0.20721 _m
$\{4:W\}$	0.1527 _m	0.15513 _m	0.17244 _m	0.15544 _m
$\{5:W\}$	0.50120 _m	0.50552 _m	0.60772 _m	0.11737 _m
$\{6:W\}$	0.1712 _m	0.16232	0.44567	0.49127
$\{7:W\}$	0.5057 _m	0.51207	0.41305	0.50710
$\{8:W\}$	1.08170 _m	0.95054 _m	0.81711 _m	0.51726 _m
$\{9:W\}$	1.16426	1.20947	1.30781	1.43843
$\{10:W\}$	0.08870	0.20926	0.28651	0.32531
$\{11:W\}$	0.57522	0.5616	0.34675	0.11272

	Sci. No. C	Sci. No. C	Sci. No. C	Sci. No. C
$\{v : W\}$	0.11178 _n	0.11178 _n	0.11178 _n	0.11178 _n
$\{u : W\}$	1.04555	1.04555	1.04555	1.04555
$\{u : R\}$	0.21944 _m	0.21944 _m	0.21944 _m	0.21944 _m
$\{u : S\}$	0.11178 _n	0.11178 _n	0.11178 _n	0.11178 _n
$\{L : R\}$	0.62878 _m	0.62878 _m	0.62878 _m	0.62878 _m
$\{L : S\}$	0.21944 _m	0.21944 _m	0.21944 _m	0.21944 _m
$\{L : W\}$	1.04555	1.04555	1.04555	1.04555
$\{x : R\}$	0.11178 _n	0.11178 _n	0.11178 _n	0.11178 _n
$\{x : S\}$	0.21944 _m	0.21944 _m	0.21944 _m	0.21944 _m
$\{y : R\}$	0.21944 _m	0.21944 _m	0.21944 _m	0.21944 _m
$\{y : S\}$	0.21944 _m	0.21944 _m	0.21944 _m	0.21944 _m

	$\lambda_{1,1}$	$\lambda_{1,2}$	$\lambda_{1,3}$	$\lambda_{1,4}$
$\{L, W\}$	0.8757 _n	1.2905 _n	0.8852 _n	0.0560 _n
$\{B, W\}$	1.4757 _n	1.5096 _n	1.0710 _n	1.7158 _n
$\{H, R\}$	0.1144 _n	0.08722 _n	0.96664 _n	0.78703 _n
$\{H, B\}$	0.04054 _n	0.05153 _n	0.08113 _n	0.07660 _n
$\{B, R\}$	0.6051 _n	0.67250 _n	0.67171 _n	0.68161 _n
$\{L, R\}$	0.1511 _n	0.1011 _n	0.18005 _n	0.0111 _n
$\{L, W\}$	0.82072 _n	0.52812 _n	0.0055 _n	0.65428 _n
$\{\pi, R\}$	1.00051	1.06115	1.10980	1.13687
$\{\pi, B\}$	1.33055	1.15425	1.12709	0.95075
$\{Q, R\}$	1.11151	0.10150	0.15115	0.50464
$\{Q, B\}$	0.45466 _n	0.12000	0.51211 _n	0.61504 _n

	Dec 26. c	1889 Feb. 4. c	1891. 16. c	1894. 28. c
$\{v : W\}$	0.012652 _n	0.65155 _n	8.92198 _n	0.490169
$\{v : W\}$	1.76016 _n	1.77996 _n	1.75653 _n	1.78015 _n
$\{u : R\}$	8.450950 _n	7.61075	8.56700	8.53951
$\{u : S\}$	0.07397 _n	0.07320 _n	0.07445 _n	0.07755 _n
$\{L : R\}$	0.65352 _n	0.65442 _n	0.65241 _n	0.65051 _n
$\{L : S\}$	8.65697	7.53833 _n	8.79391 _n	7.06474 _n
$\{L : W\}$	8.68864 _n	8.70544 _n	8.71501 _n	8.70866 _n
$\{\pi : R\}$	1.15224	1.15635	1.14953	1.13120
$\{\pi : S\}$	0.63452	0.70547 _n	0.74105 _n	1.01153 _n
$\{c : R\}$	0.47782	8.62530 _n	0.58461 _n	0.55712 _n
$\{c : S\}$	0.63317 _n	0.63799 _n	0.62095 _n	0.60543 _n

	Sep 2.0	Oct. 13.0	Nov 22.0	Dec 31.0	Jan 10.0	Feb 18.0	Mar 27.0
λ_0	$+1^\circ 16'$	$+1^\circ 41'$	$+1^\circ 18'$	$+0^\circ 20'$	$+0^\circ 26'$	$+0^\circ 26'$	$+0^\circ 26'$
λ_0	$221^\circ 17'.4$	$224^\circ 21'.0$	$227^\circ 25'.1$	$230^\circ 29'.2$	$233^\circ 33'.3$	$236^\circ 37'.4$	$239^\circ 41'.5$
$\lambda - \lambda_0$	$-33^\circ 16'.6$	$-32^\circ 40'.0$	$-32^\circ 22'.9$	$-32^\circ 09'.2$	$-31^\circ 56'.3$	$-31^\circ 43'.4$	$-31^\circ 30'.5$
$\sin(\lambda_0 - \lambda)$	0.55116_n	0.54050_n	0.52776_n	0.51078_n	0.49116_n	0.46947_n	0.44631_n
$\cos \lambda_0$	0.99992	0.99992	0.99993	0.99994	0.99994	0.99994	0.99994
$\cos(\lambda_0 - \lambda)$	0.942272	0.943702	0.945170	0.946083	0.947020	0.947880	0.948651
$\sin \lambda_0$	0.28717	0.271091	0.254609	0.23529	0.213404	0.189975	0.165449
$\sin \lambda$	0.999973	0.999970	0.999966	0.999961	0.999957	0.999952	0.999947
$\cos(\lambda - \lambda_0)$	0.73508_n	0.70042_n	0.65164_n	0.60874_n	0.56185_n	0.51115_n	0.45777_n
λ	$-2^\circ 17'$	$-2^\circ 5'.1$	$-2^\circ 15'.5$	$-2^\circ 25'.4$	$-2^\circ 35'.6$	$-2^\circ 45'.8$	$-2^\circ 55'.9$
$\lambda - i$	$-4^\circ 23'.3$	$-4^\circ 20'.7$	$-4^\circ 37'.4$	$-4^\circ 47'.0$	$-4^\circ 56'.2$	$-5^\circ 05'.4$	$-5^\circ 14'.5$
$\sin(\lambda - i)$	0.88375_n	0.89416_n	0.90636_n	0.92110	0.93814_n	0.95610_n	0.97410_n
η	0.73835_n	0.70072_n	0.65802_n	0.60913_n	0.55281	0.48833_n	0.41533_n
$\cos(\lambda - i)$	0.999973	0.999966	0.999952	0.999948	0.999936	0.999917	0.999891
$\cos B, \sin B$	0.73703_n	0.69938_n	0.65662_n	0.60761_n	0.55267_n	0.48800_n	0.41500_n
	0.92302	0.93723	0.94992	0.96102	0.97065	0.97856	0.98456
$\cos B, \cos b$	0.92404	0.93604	0.94963	0.96077	0.97044	0.97870	0.98570
b	$-33^\circ 7'.0$	$-30^\circ 3'.4$	$-26^\circ 59'.4$	$-23^\circ 54'.0$	$-20^\circ 49'.6$	$-17^\circ 43'.0$	$-14^\circ 36'.0$
$\cos B_1$	0.999962	0.999966	0.999971	0.999975	0.999977	0.999978	0.999979
η_1	0.73470	0.70361	0.65246	0.59227	0.52350	0.44609	0.36069
$\sin B_1$	0.62210	0.59458	0.56439	0.53021	0.49145	0.44901	0.40301
$b_1 - u$	$-143^\circ 40'.1$	$-156^\circ 8'.2$	$-169^\circ 47'.7$	$-179^\circ 33'.7$	$-185^\circ 21'.9$	$-188^\circ 15'.9$	$-189^\circ 25'.0$
$\sin(b_1 - u)$	0.99611_n	0.96110_n	0.92401_n	0.90946_n	0.89775_n	0.88770_n	0.87910_n
$\eta \cos B$	0.73382	0.70227	0.65107	0.59200	0.52312	0.44560	0.36000
$\sin(b_1 - u)$	0.77266_n	0.60695_n	0.32512_n	0.30969_n	0.16623	0.47770	0.47770

	Sept 30	Oct. 15.0	Nov. 15.0	Dec. 15.0	Jan. 15.0	March 21.0
S.	0.63094	0.60446 _m	0.72074 _m	0.71111	0.73377	0.70999
r	0.25051	0.24075	0.30044	0.31744	0.31115	0.29148
g	0.51601	0.54520	0.58443	0.55500	0.54182	0.52032
S-r	0.79742 _m	0.83895 _m	0.66257 _m	0.73311 _m	0.87360 _m	0.86600 _m
	0.94949	0.97919	0.94474	0.99993	0.99759	0.95975
g.	0.50648 _m	0.34025 _m	0.05717 _m	0.12164 _m	0.89752	0.20822
S-r-g	0.84703 _m	0.58976 _m	0.56813 _m	0.57341 _m	0.87601 _m	0.57625 _m
	0.94977 _m	0.99981 _m	0.99984 _m	0.99987 _m	0.99989 _m	0.99991 _m
z	0.35630	0.32849	0.29735	0.26248	0.22295	0.17800
S ⁻¹	0.15144	0.14003	0.17171	0.12646	0.12288	0.12366
S ⁻²	0.45552	0.42015	0.39513	0.27726	0.37164	0.37098
S ⁻³	0.79740	0.79917	0.80112	0.80325	0.80550	0.80702
z	0.07819	0.14413	0.18943	0.21849	0.20441	0.20023
S ⁻⁴	0.50371	0.56428	0.58456 _m	0.59777	0.60605 _m	0.61027 _m
S ⁻⁵	8.17365	8.25874	8.30730	8.22073	8.33262	8.32026
S ⁻⁶	7.73603	7.71090	7.69857	7.67682	7.70342	7.71666
z	0.24034	0.40321	0.48599	0.51776	0.51205	0.47917
S ⁻⁷	0.77637	0.11711	0.18456	0.14661	0.1637	0.17002
S ⁻⁸	8.04010	7.90453	7.64235	6.72956	7.50377 _m	7.51550 _m
S ⁻⁹	6.89001 _m	6.89277 _m	6.88191 _m	6.86035 _m	6.82900 _m	6.78527 _m
S ⁻¹⁰	0.44115	0.07892	0.14937	0.17942	0.17115	0.16064
S ⁻¹¹	0.00500	0.86934	0.60716	0.69437	0.46838 _m	0.78331 _m
S ⁻¹²	0.58377	8.85758 _m	8.84672 _m	8.82516	8.79281	8.75885

		Oct. 12.0	Nov. 22.0	1888 Jan 1	Feb. 10.0	March 21.0
J ₀	+ 0.008	+ 0.033	+ 0.110	+ 0.125	+ 0.130	+ 0.126
J ₁	- 1.105	- 2.762	- 2.169	- 1.444	- 0.696	- 0.013
J ₂	- 0.098	- 0.156	- 0.262	- 0.307	- 0.317	- 0.296
J ₃	- <u>1.286</u>	- <u>1.134</u>	- <u>0.602</u>	- <u>0.071</u>	+ <u>0.410</u>	+ <u>0.810</u>
J ₄	- 1.083	- 1.320	- 0.864	- 0.375	+ 0.093	+ 0.523
J ₅	- 1.717	- 4.762	- 5.713	- 6.264	- 6.456	- 6.297
J ₆	- 0.167	+ 0.170	+ 0.113	+ 0.015	- 0.095	- 0.195
J ₇	- <u>0.003</u>	- <u>0.002</u>	- <u>0.002</u>	- <u>0.001</u>	- <u>0.001</u>	- <u>0.000</u>
J ₈	- 2.250	- 4.594	- 5.602	- 6.250	- 6.552	- 6.492
J ₉	- 10.845	- 11.467	- 9.215	- 4.974	- 0.115	+ 4.256
J ₁₀	+ <u>14.766</u>	+ <u>18.004</u>	+ <u>9.499</u>	+ <u>1.358</u>	- <u>8.427</u>	- <u>17.300</u>
J ₁₁	+ 4.225	+ 3.627	+ 0.754	- 3.616	- 8.545	- 13.053
J ₁₂	+ 10.24	+ 1.941	+ 2.725	+ 5.191	+ 7.215	- 0.19
J ₁₃	+ 5.757	- 2.261	+ 0.599	+ 0.064	- 0.107	- 0.146
J ₁₄	+ 4.511	+ 4.209	+ 3.627	+ 3.261	+ 3.195	+ 3.425

	April 30	May 1	May 19 0	May 25.0	May 31	June 1
δ	$- 0^{\circ} 40.4$	$- 0^{\circ} 40.7$	$+ 0^{\circ} 43.0$	$+ 0^{\circ} 39.4$	$+ 0^{\circ} 35.5$	$+ 0^{\circ} 31.6$
λ	239 47.8	242 59	246 35	249 12.6	252 22	255 33
$\lambda - \delta$	$- 11^{\circ} 40.2$	$- 11^{\circ} 32.7$	$- 8^{\circ} 24.7$	$- 5^{\circ} 15.4$	$- 2^{\circ} 5.5$	$+ 1^{\circ} 4$
$\sin(\lambda - \delta)$	0.40355	0.30132 _n	0.16503 _n	0.06195 _n	0.0222 _n	0.27860
$\cos \delta$	0.999945	0.99996	0.99997	0.99997	0.99998	0.99999
$\cos(\lambda - \delta)$	0.99556	0.99113	0.99531	0.99817	0.99971	0.99992
δ	5.16181	5.1311 _n	5.0971 _n	5.05511	5.01275	4.96341
$\cos \delta \sin(\lambda - \delta)$	0.40350	0.30127 _n	0.16500 _n	0.06194 _n	0.0222 _n	0.27858
G	$- 30^{\circ} 16.8'$	$- 30^{\circ} 52.0$	$- 40^{\circ} 22.4$	$- 49^{\circ} 6.8$	$- 58^{\circ} 47.1$	$+ 23^{\circ} 49.6$
$G - i$	$- 50^{\circ} 38.4$	$- 6^{\circ} 13.6$	$- 7^{\circ} 17.0$	$- 47^{\circ} 25.4$	$- 18^{\circ} 5.7$	$+ 23^{\circ} 25.0$
$\sin(G - i)$	0.99245 _n	0.03528 _n	0.1106 _n	0.71640 _n	0.49336 _n	0.60012
i	0.40421 _n	0.30227 _n	0.16655 _n	0.06531 _n	0.0224 _n	0.27858
$\cos(G - i)$	0.99789	0.99742	0.991651	0.91403	0.97785	0.96251
$\cos B, \sin L$	0.40210 _n	0.29970 _n	0.16309 _n	0.05934	0.055679 _n	0.28679
	0.95564	0.99111	0.99534	0.99511	0.99972	0.99992
$\cos B, \cos L$	0.95555	0.99109	0.99528	0.99514	0.99969	0.99990
L	$- 140^{\circ} 37.5$	$- 110^{\circ} 30.2$	$- 80^{\circ} 22.3$	$- 50^{\circ} 13.5$	$- 20^{\circ} 3.9$	$+ 10^{\circ} 6.5$
$\cos B$	0.999986	0.999990	0.999994	0.999995	0.999997	0.999998
τ	0.72984	0.72894	0.72804	0.72701	0.72605	0.72492
$\sin B$	0.39666	0.33755	0.22102	0.18171	0.07222	0.02440
$L - u$	$- 205^{\circ} 47.3$	$- 15^{\circ} 27.1$	$- 22^{\circ} 35.1$	$- 27^{\circ} 16.7$	$- 33^{\circ} 21.0$	$- 38^{\circ} 44.4$
$\cos(L - u)$	0.95444 _n	0.96125 _n	0.68051 _n	0.83153 _n	0.97702 _n	0.970226
$\tau \cos B$	0.72970	0.72884	0.72794	0.72696	0.72595	0.72490
$\sin(L - u)$	0.63854	0.74134	0.71122	0.86608	0.90592	0.93639

	April 20.0	May 19.0	June 19.0	July 19.0	Oct. 19.0	Nov. 19.0
ξ_1	0.65414 _m	0.65019 _m	0.60844 _m	0.55849 _m	0.49897 _m	0.42716 _m
η	0.35002	0.37018	0.38014	0.38834	0.39417	0.29928
ζ	0.40360	0.46323	0.43001	0.39439	0.35626	0.31525
$\xi - \eta$	0.55222 _m	0.53141 _m	0.51015 _m	0.57577 _m	0.75101 _m	0.71453 _m
	0.97770 ₉	0.96264	0.94474	0.92425	0.90098	0.87448
η	0.35002	0.47018	0.54121	0.59304	0.61187	0.66129
$\xi - \eta$	0.87443 _m	0.87077 _m	0.86541 _m	0.85548 _m	0.85003 _m	0.84005 _m
	0.99993 _m	0.99993	0.99996 _m	0.99997 _m	0.99995	0.99999
ζ	0.12650	0.06649	0.01563	0.00872	0.00828	0.04022
ξ^2	0.12750	0.12122	0.13435	0.14149	0.14995	0.15914
ξ^3	0.37650	0.38734	0.40365	0.42447	0.44085	0.47082
η^2	0.1045	0.1218	0.1603	0.1897	0.2206	0.2524
ξ	0.23462	0.22122	0.19990	0.17004	0.13232	0.08466
K	0.01112 _m	0.00000	0.00355 _m	0.01481	0.05217 _m	0.06443 _m
ξK	0.29526	0.00000	0.21199	0.15330	0.08114	0.01174
η^2	0.1045	0.1218	0.1603	0.1897	0.2206	0.2524
ζ	0.42028	0.33000	0.22541	0.07500	0.05074	0.47143
$\bar{N}_0$	0.05740	0.09458	0.00920	0.88844	0.70434	0.35050
S_0	0.07936 _m	0.07904 _m	0.14476	0.15755 _m	0.21404 _m	0.22577 _m
N_0	0.05740	0.09458	0.59918 _m	0.50353	0.35045 _m	0.21580 _m
$\bar{N}$	0.12021	0.05939	0.07401	0.85325	0.66015	0.31534
S	0.14411 _m	0.04385 _m	0.10957 _m	0.15206 _m	0.17879 _m	0.19058
N	0.05740	0.04016 _m	0.56399 _m	0.46834 _m	0.34526 _m	0.17861

	Aug. 20.0	Sept. 1.0	Oct. 1.0	Nov. 1.0	Dec. 1.0	Jan. 16.0
Δ_1	+ 0.113	+ 0.097	+ 0.074	+ 0.051	+ 0.034	+ 0.018
Δ_2	+ 0.541	+ 0.520	+ 0.438	+ 0.361	+ 0.285	+ 0.202
Δ_{u_1}	- 0.258	- 0.195	- 0.141	- 0.081	- 0.043	- 0.013
Δ_{u_2}	+ 1.152	+ 1.111	+ 1.004	+ 0.920	+ 0.820	+ 0.750
Δ_{u_3}	+ 0.890	+ 0.815	+ 0.703	+ 0.605	+ 0.511	+ 0.437
Δ_{L_1}	- 5.871	- 5.213	- 4.362	- 3.355	- 2.222	- 0.993
Δ_{L_2}	- 0.270	- 0.210	- 0.216	- 0.285	- 0.234	- 0.160
Δ_{L_3}	+ 0.000	+ 0.001	+ 0.001	+ 0.001	+ 0.001	+ 0.001
Δ_{L_4}	- 6.141	- 5.522	- 4.677	- 3.642	- 2.476	- 1.152
Δ_{π_1}	+ 7.464	+ 6.109	+ 4.430	+ 2.257	+ 0.000	+ 2.533
Δ_{π_2}	- 28.804	- 27.490	- 27.054	- 26.552	- 26.099	- 14.129
Δ_{π_3}	- 16.430	- 15.201	- 13.524	- 11.255	- 8.702	- 11.296
Δ_{σ_1}	+ 2.622	+ 2.005	+ 1.465	+ 0.905	+ 0.450	+ 0.122
Δ_{σ_2}	+ 1.252	+ 0.421	+ 3.666	+ 4.825	+ 5.761	+ 6.533
Δ_{σ_3}	+ 2.885	+ 4.456	+ 5.121	+ 5.712	+ 6.217	+ 6.533

	Dec. 26 0	Jan. 1 16	Mar. 1 16	April 25.0
β_0	+ 0° 27.5	+ 0° 28.3	+ 0° 10.1	+ 0° 14.7
λ_0	258 48.1	161 57.4	265° 11.7	265° 26.5
$\lambda_0 - \delta$	+ 4° 17.1	+ 7° 27.7	+ 10° 43.7	+ 13 58.5
$\sin(\lambda_0 - \delta)$	8.57342	111560	3.26957	1.72207
$\cos \beta_0$	9.99999	9.99999	9.99999	9.99999
$\cos(\lambda_0 - \delta)$	9.99879	9.99227	9.99234	9.99606
$\sin \beta_0$	7.20345	7.82105	7.74476	7.63104
$\cos \beta_0 \sin(\lambda_0 - \delta)$	8.57341	111550	3.26956	1.72206
α	+ 6° 6.7	+ 2° 52.4	+ 1° 42.0	+ 1° 6.7
$\alpha - i$	+ 3° 45.1	+ 0° 20.5	- 0° 30.0	- 1° 20.7
$\sin(\alpha - i)$	8.51570	8.02954	8.05475	8.37055
λ	887581	4.11617	9.27005	9.38294
$\cos(\alpha - i)$	9.99997	9.99999	9.99997	9.99998
$\cos B, \sin L$	887486	9.11614	9.27002	9.38287
$\cos$	9.99878	9.99626	9.99233	9.98696
$\cos B, \cos L$	9.99878	9.99626	9.99233	9.98696
L	+ 4° 18.0	+ 7° 30.5	+ 10° 42.9	+ 13° 58.4
$\cos B,$	9.99999	9.99999	9.99999	9.99999
$r,$	0.72353	0.72270	0.72155	0.72000
$\sin B,$	7.69160	7.14771	7.12482	7.15554
$L, - u$	- 245° 40.0	- 251° 1.6	- 257° 22.1	- 263° 16.1
$\cos(L, - u)$	9.01471	9.21157	9.23651	9.26504
$\cos B, r,$	0.72353	0.72270	0.72155	0.72000
$\sin(L, - u)$	9.95060	9.99999	9.99999	9.99999

[illegible]

	$\alpha_2 = 20.0$	$\beta_2 = 10.0$	$\gamma_2 = 10.0$	$\alpha_1 = 10.0$
J_1	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_2	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_3	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_4	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_5	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_6	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_7	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_8	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_9	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{10}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{11}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{12}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{13}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{14}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{15}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{16}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{17}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{18}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{19}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{20}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{21}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{22}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{23}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{24}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{25}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{26}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{27}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{28}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{29}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{30}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{31}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{32}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{33}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{34}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{35}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{36}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{37}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{38}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{39}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{40}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{41}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{42}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{43}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{44}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{45}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{46}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{47}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{48}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{49}	+ 0.000	+ 0.000	- 0.000	+ 0.000
J_{50}	+ 0.000	+ 0.000	- 0.000	+ 0.000

The integration means of mechanical quadratures is performed according to the following formulae -

$$\frac{1}{2} \tilde{f}(u - \frac{1}{2}w) = -\frac{1}{24} f''(u - \frac{1}{2}w) + \frac{1}{5760} f^{(4)}(u - \frac{1}{2}w) + \dots$$

$${}''\tilde{f}(a) = \frac{1}{24} f''(a-w) - \frac{1}{5760} \{ -f^{(4)}(a-w) + f^{(4)}(a) \} + \dots$$

$$\int_0^{a+iw} \tilde{f}(x) dx = \frac{1}{2} \tilde{f}(a+iw) - \frac{1}{12} \tilde{f}'(a+iw)$$

$$\iint \tilde{f}(x) dx dy = {}''\tilde{f}(a+iw) + \frac{1}{12} (a+iw).$$

$$L = L_0 + u_0 t + \Delta L_1 + \Delta L_2$$

$$= L_0 + u_0 t + \int \left(\frac{dL}{dt} \right) dt + \iint \frac{d^2 L}{dt^2} dt^2$$

$$\Delta L_0 = \Delta L - \Delta \pi - \Delta u t,$$

$$T = \text{Jan. 0.0 1898.}$$

1887				1888		1889
Sept. 1.0				-3.105		
	-1	+345			+4.111	
Oct. 13.0		+200		2.762		+1.472
	-118				+2.113	
Nov. 22.0		+132		-2.164		+1.125
1888	-114	+775			-0.031	
Jan. 1.0		+25		-1.444		-0.316
	-88	+745			-1.475	
Feb. 10.0		-65		-0.646		-1.584
	-44	+683			-1.171	
Mar. 21.0		-129		-0.012		-2.230
	-36	+554			-2.114	
Apr. 30.0		-165		+0.541		-1.753
	-16	+354			-1.643	
June 1.0		-181		+0.730		-1.203
	+4	+208			-0.713	
July 19.0		-177		+1.138		-0.154
	+22	+31			+0.425	
Aug. 28.0		-155		+1.169		+1.016
	+36	-124			+1.514	
Oct. 7.0		-119		+1.045		+1.136
	+34	-243			+2.621	
Nov. 16.0		-80		+0.802		+2.065
	+56	-323			+3.441	
Dec. 26.0		-24		+0.477		+2.707
	+58	-347			+3.424	
1889 Jan. 4.0		+24		+0.132		+2.114
	+57	-313			+4.051	
Mar. 16.0		+84		-0.181		+0.815
		-120			+2.871	
April 25.0				-0.005		

1887						$\frac{dR}{dt}$
Sept. 3.0			-6.01	+4,223		
Oct. 13.0		2,247	-2,843	+3,627	+4,225	-2,278
Nov. 22.0	+6.5	1,557		+4,784		+2,111
1888	+1,120		-4,400		+4,186	
Dec. 1.0		-2,211		-3,616		-1,218
	+9,50		-4,424			
Feb. 10.0		+421		-1,545		-2,320
	+710		-4,500		-11,775	
Mar. 21.0		+1,131		-13,000		-18,160
	+1,112		-1,373		-2,702	
Apr. 30.5		+1,516		-16,430		-33,021
	+1,12		-1,361		-41,458	
June 9.5		+1,620		-11,243		-50,710
	+106		-0,213		-57,749	
July 19.5		+1,712		-18,524		-1,171,176
	-278		+1,289		-78,273	
Aug. 28.0		+1,244		-17,235		-1,27,054
	-371		+4,531		-72,500	
Oct. 7.0		+811		-14,702		-1,43,113
	720		+3,406		-1,50,200	
Nov. 16.0		+1,511		-11,246		-1,6,164
	-224		+3,777		-2,1700	
Dec. 26.0		+1,78		-2,500		-2,771
1889	-650		+1,584		-2,0045	
Feb. 4.0		+1,211		-3,777		-2,11,217
	600		+1,200		-2,13,000	
Mar. 16.0		+1,522		-1,144		-2,13,770
			+1,239		-2,14,140	
Apr. 1.0						

1347				Di		
Sept. 1.0	5	5	5	+0.042		
			+5		-0.194	
Oct. 1.0	8	8		+0.083		-0.155
	-4		+25		-0.111	
Nov. 22.1	-12			+0.110		-0.058
Dec. 1.0	+1		+15		-0.001	
Jan. 1.0	-10			+0.125		+0.061
	+1		+5		+0.124	
Feb. 10.0	-7			+0.130		+0.189
	0		-4		+2.254	
Mar. 21.0	-7			+0.126		+0.318
	+4		-1		+0.380	
Apr. 30.0	-5			+0.113		+0.438
	+2		-18		+0.493	
May 9.0	-5			+0.095		+0.542
	+1		-21		+0.588	
June 19.0	0			+0.074		+0.627
	+2		-21		+0.662	
July 28.0	+3			+0.053		+0.670
	+1		-17		+0.715	
Aug. 7.0	+3			+0.035		+0.734
	+2		-16		+0.749	
Sept. 16.0	+5			+0.015		+0.759
	0		-11		+0.767	
Oct. 26.0	+5			+0.007		+0.771
Nov. 8.0	0		-6		+0.774	
Dec. 4.0	+5			+0.001		+0.775
	-2		-1		+0.775	
Jan. 6.0	0			-0.001		+0.775
			+2		+0.775	
Feb. 2.0						

1887				59		
2000				+4,211		
2001			-602		-2820	
2002	12.1	+20		+4,211		2,666
		+196	-582		-3,611	
2003	22.0	+216		+3,627		-1,211
1888		+84	-66		+4,016	
2004	1.0			+3,261		1,665
		-4	-66		+3,277	
2005	10.0	+246		+3,125		+4,868
		-66	+230		+6,472	
2006	21.0	+230		+3,425		+8,156
		-89	+460		+2,117	
2007	1.0	+141		+3,885		+11,845
		-97	+601		+13,872	
2008	4.0	+44		+4,486		+1,173
		-87	+645		+13,213	
2009	14.1	-43		+5,131		+20,782
		-75	+602		+23,177	
2010	2.0	-118		+5,731		+20,210
		-58	+434		+29,132	
2011	2.0	-176		+6,217		+22,201
		-44	+301		+3,5349	
2012	16.1	-225		+6,725		1,175
		-25	+11		+41,874	
2013	26.0	-245		+6,613		+47,111
1889		-3	-7		+41,417	
2014	4.0	-44		+6,416		+51,211
		+15	-41		+6,416	
2015	1.0	-202		+6,071		+51,211
			-41		+6,071	
2016	1.0					

$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$	$\frac{1}{2} \frac{d^2 u}{dt^2}$
Sept. 2.0	-364	-1,634	-3,024			
	+92	-1,520	-0,860	+1,469	+0,037	-0,070
Oct. 13.0	+456		+0,844			
	+30	-0,864	-0,016	+0,372	+0,009	-0,081
Nov. 22.0	+406		-0,020			
Dec. 1.0	-15	-0,378	-0,020	-0,247	-0,010	-0,067
	+471		-0,398			
Jan. 10.0	-41	+0,043	-0,414	-0,000	-0,010	-0,026
	+430		-0,305			
Feb. 21.0	54	+0,220	-0,789	-0,077	-0,002	-0,615
	+76		+0,218			
Mar. 30.0	-62	+0,844	-0,711	+0,640	+0,116	0,446
	+4		+1,117			
Apr. 1.0	-64	+1,211	+0,460	+1,700	+0,043	+0,617
	+3	+250	+1,520			
May 11.0	-41	+1,463	+2,926	+3,044	+0,076	+1,430
	+189					
June 28.0	-64	+1,652	+4,719	+4,606	+0,115	+4,857
	+125		+1,445			
July 7.0	-45	+1,777	+12,164	+6,326	+0,158	+12,312
	+60		+7,222			
Aug. 16.0	-45	+1,837	+18,386	+1,107	+0,201	+19,117
	-8		+9,059			
Sept. 26.0	-73	+1,832	-28,445	+9,978	+0,244	+22,748
	-78		+10,891			
Oct. 4.0	-81	+1,814	+39,336	+11,778	+0,294	+41,402
	-159		+12,645			
Nov. 16.0	-92	+1,814	+51,981	+13,460	+0,337	+55,775
	-251		+15,000			
Dec. 27.0		+1,814	+66,000			

[illegible]

12			
.7			
100, 1	-5,666		
29	4,111		
100, 2	-3,789	+1,111	
12	-2,742		
22	-6,758	-6,485	
100, 2	-6,726		
12	-6,090	+1,000	
22	+0,772		
Jan, 1	+1,665		
11	+2,478		
21	+1,747	+1,100	
31	+4,054		
Feb, 1	+4,868		
20	+5,671		
Mar, 1	+6,482	+1,288	
11	+7,230		
21	+8,156	+1,401	
31			
Apr, 10	+7,748		
20			
30	+11,845		

11.

1887

1/1	1	+1,473			
	2	+2,674			
	3	+1,195	-26		
	11	+1,575			
	21	+1,575			
	2	+1,575			
	11	-0,074	-1,601		
	21	-0,474			
	1	-1,176			
	11	-1,140			
	21	-1,421	-1,063		
	1	-1,677			
	10	-1,884			
	20	-2,014			
	1	-2,141	-1,060		
	11	-2,206			
	21	-2,230			
	1	-2,160	+0,278		
	10	-1,575			
	20				
		-1,2			

1887

1887					
		- 2,220			
		- 1,671	+ 0,496	- 1,647	
	2	- 1,671		+ 1,671	- 1,722
	12	- 0,164			
	22	+ 0,111			
	2	+ 0,046			
	12	- 0,007	- 1,327		
	22	- 0,448			
	1	- 1,218			
	11	- 2,287			
	21	- 3,661	- 6,078		
	21	- 1,465			
	10	- 7,276		4,771	- 1,271
	20	- 7,592	- 2,276		
	1	- 12,132	- 10,867		- 1,477
	11	- 15,089			
	21	- 18,165			
	1				
	10	- 25,367	- 14,771		
	20				
	30	- 22,821			

1887

Jan.	1	+0.005			
"	2	+0.007			
Apr.	2	+0.011	-0.002		
"	12	+0.012			
"	22	+0.007			
May	2	+0.007			
"	12	+0.011			
"	22	+0.012			
Jun	1	-0.006			
"	11	+0.007	-0.008		
"	21	+0.007			
"	1	+0.009			
Jul	1	+0.011			
"	20	+0.007			
Aug.	1	+0.007			
"	11	+0.007			
"	21	+0.002			
"	31	+0.002			
Sept.	10	+0.011			
"	20	+0.011			
"	30	+0.011			

11

1000

1000	10	+7,000		2,000	
	20	+6,111			
1000	30	+5,157	-4,000		
	40	+4,000			
	50	+2,809		-1,600	
1000	60	+1,000			
	70	+0,002	-1,000		
	80	+0,000			
1000	90	-0,000			
1000	100	-0,000			
	110	-0,000			
	120	-0,000			
	130	-0,000			
	140	-0,000			
	150	-0,000			
	160	-0,000			
	170	-0,000			
	180	-0,000			
	190	-0,000			
	200	-0,000			
	210	-0,000			
	220	-0,000			
	230	-0,000			
	240	-0,000			
	250	-0,000			
	260	-0,000			
	270	-0,000			
	280	-0,000			
	290	-0,000			
	300	-0,000			
	310	-0,000			
	320	-0,000			
	330	-0,000			
	340	-0,000			
	350	-0,000			
	360	-0,000			
	370	-0,000			
	380	-0,000			
	390	-0,000			
	400	-0,000			
	410	-0,000			
	420	-0,000			
	430	-0,000			
	440	-0,000			
	450	-0,000			
	460	-0,000			
	470	-0,000			
	480	-0,000			
	490	-0,000			
	500	-0,000			
	510	-0,000			
	520	-0,000			
	530	-0,000			
	540	-0,000			
	550	-0,000			
	560	-0,000			
	570	-0,000			
	580	-0,000			
	590	-0,000			
	600	-0,000			
	610	-0,000			
	620	-0,000			
	630	-0,000			
	640	-0,000			
	650	-0,000			
	660	-0,000			
	670	-0,000			
	680	-0,000			
	690	-0,000			
	700	-0,000			
	710	-0,000			
	720	-0,000			
	730	-0,000			
	740	-0,000			
	750	-0,000			
	760	-0,000			
	770	-0,000			
	780	-0,000			
	790	-0,000			
	800	-0,000			
	810	-0,000			
	820	-0,000			
	830	-0,000			
	840	-0,000			
	850	-0,000			
	860	-0,000			
	870	-0,000			
	880	-0,000			
	890	-0,000			
	900	-0,000			
	910	-0,000			
	920	-0,000			
	930	-0,000			
	940	-0,000			
	950	-0,000			
	960	-0,000			
	970	-0,000			
	980	-0,000			
	990	-0,000			
	1000	-0,000			

Perturbations in R, A and Q .

Perturbations in L, λ, Ω , etc, etc. as computed in the differential equations already found in the preceding section, these quantities being first then interpolated for the negative date etc. when the differential equations are found, we find the following values for the variations produced in the co-ordinates u and v .

J^0	J^1	J^2	J^3	J^4	J^5	J^6	J^7	J^8	J^9	J^{10}	J^{11}	J^{12}	J^{13}	J^{14}	J^{15}	J^{16}	J^{17}	J^{18}	J^{19}	J^{20}	J^{21}	J^{22}	J^{23}	J^{24}	J^{25}	J^{26}	J^{27}	J^{28}	J^{29}	J^{30}	J^{31}	J^{32}	J^{33}	J^{34}	J^{35}	J^{36}	J^{37}	J^{38}	J^{39}	J^{40}	J^{41}	J^{42}	J^{43}	J^{44}	J^{45}	J^{46}	J^{47}	J^{48}	J^{49}	J^{50}	J^{51}	J^{52}	J^{53}	J^{54}	J^{55}	J^{56}	J^{57}	J^{58}	J^{59}	J^{60}	J^{61}	J^{62}	J^{63}	J^{64}	J^{65}	J^{66}	J^{67}	J^{68}	J^{69}	J^{70}	J^{71}	J^{72}	J^{73}	J^{74}	J^{75}	J^{76}	J^{77}	J^{78}	J^{79}	J^{80}	J^{81}	J^{82}	J^{83}	J^{84}	J^{85}	J^{86}	J^{87}	J^{88}	J^{89}	J^{90}	J^{91}	J^{92}	J^{93}	J^{94}	J^{95}	J^{96}	J^{97}	J^{98}	J^{99}	J^{100}	J^{101}	J^{102}	J^{103}	J^{104}	J^{105}	J^{106}	J^{107}	J^{108}	J^{109}	J^{110}	J^{111}	J^{112}	J^{113}	J^{114}	J^{115}	J^{116}	J^{117}	J^{118}	J^{119}	J^{120}	J^{121}	J^{122}	J^{123}	J^{124}	J^{125}	J^{126}	J^{127}	J^{128}	J^{129}	J^{130}	J^{131}	J^{132}	J^{133}	J^{134}	J^{135}	J^{136}	J^{137}	J^{138}	J^{139}	J^{140}	J^{141}	J^{142}	J^{143}	J^{144}	J^{145}	J^{146}	J^{147}	J^{148}	J^{149}	J^{150}	J^{151}	J^{152}	J^{153}	J^{154}	J^{155}	J^{156}	J^{157}	J^{158}	J^{159}	J^{160}	J^{161}	J^{162}	J^{163}	J^{164}	J^{165}	J^{166}	J^{167}	J^{168}	J^{169}	J^{170}	J^{171}	J^{172}	J^{173}	J^{174}	J^{175}	J^{176}	J^{177}	J^{178}	J^{179}	J^{180}	J^{181}	J^{182}	J^{183}	J^{184}	J^{185}	J^{186}	J^{187}	J^{188}	J^{189}	J^{190}	J^{191}	J^{192}	J^{193}	J^{194}	J^{195}	J^{196}	J^{197}	J^{198}	J^{199}	J^{200}	J^{201}	J^{202}	J^{203}	J^{204}	J^{205}	J^{206}	J^{207}	J^{208}	J^{209}	J^{210}	J^{211}	J^{212}	J^{213}	J^{214}	J^{215}	J^{216}	J^{217}	J^{218}	J^{219}	J^{220}	J^{221}	J^{222}	J^{223}	J^{224}	J^{225}	J^{226}	J^{227}	J^{228}	J^{229}	J^{230}	J^{231}	J^{232}	J^{233}	J^{234}	J^{235}	J^{236}	J^{237}	J^{238}	J^{239}	J^{240}	J^{241}	J^{242}	J^{243}	J^{244}	J^{245}	J^{246}	J^{247}	J^{248}	J^{249}	J^{250}	J^{251}	J^{252}	J^{253}	J^{254}	J^{255}	J^{256}	J^{257}	J^{258}	J^{259}	J^{260}	J^{261}	J^{262}	J^{263}	J^{264}	J^{265}	J^{266}	J^{267}	J^{268}	J^{269}	J^{270}	J^{271}	J^{272}	J^{273}	J^{274}	J^{275}	J^{276}	J^{277}	J^{278}	J^{279}	J^{280}	J^{281}	J^{282}	J^{283}	J^{284}	J^{285}	J^{286}	J^{287}	J^{288}	J^{289}	J^{290}	J^{291}	J^{292}	J^{293}	J^{294}	J^{295}	J^{296}	J^{297}	J^{298}	J^{299
-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	-----------	----------

[illegible]

J_{π}	J_0	J_2	J_4	J_6	J_8
$0^{+}, 1^{-}, 2^{+}$	-1.174	$+0.012$	$+0.011$	-0.004	$+0.007$
$0^{+}, 2^{+}, 3^{+}$	$+2.0825n$	$0.17406n$	-0.001	-0.001	$+0.006n$
$0, 3, 7, 10, n$	$0.6221n$	0.6379	-0.005	-0.001	-0.0510
$0, 5, 4, 0, 9$	$3.6197n$	0.61157	0.00212	-0.000	$1.317 - n$
$0, 3, 5, 0, 3, n$	3.27046	$3.13752n$	0.6006	$0.4004n$	$0.575 - 0n$
$0, 0, 1, 2, 5, n$	$3.68103n$	3.82536	-0.005	$0.000n$	$0.160 - n$
$0^{+}, 1^{-}, 2^{+}$	$+0.012$	-0.014	$+0.004$	-0.002	-0.001
$0^{+}, 1^{-}, 2^{+}$	-0.043	$+0.022$	$+0.001$	-0.002	-0.004
$1^{+}, 1, 2, 2$	-0.015	$+0.162$	$+0.002$	-0.001	-0.001
$0, 9, 3, 6, 12$	$3.12207n$	$3.0931n$	-0.001	-0.001	-0.001
$0, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000$	0.44150	0.38138	0.44111	0.44111	0.44111
$0, 2, 1, 5, 2, n$	3.27030	$3.12205n$	-0.001	-0.001	-0.001
$0, 1, 2, 5, n$	$3.68103n$	3.64110	0.000	0.000	0.000
$0^{+}, 1^{-}, 2^{+}$	$+0.023$	-0.013	$+0.014$	-0.001	$+0.001$
$0^{+}, 1^{-}, 2^{+}$	-0.062	$+0.040$	$+0.002$	-0.001	$+0.002$

$$\begin{array}{l}
\delta_{\lambda\lambda}^{\lambda\lambda} \quad q_1 = \quad J\pi \quad J\lambda \quad J\mu \quad J\eta \quad J\alpha \\
- 9.10^{+1} \quad - 1.57^{+1} \quad + 0.75 \quad + 4.12 \quad - 0.015 \quad - 0.001 \\
992555 \quad 5.10^{+1} \quad 5.1140^{+1} \quad 0.122^{+1} \quad 1.143^{+1} \quad 1.143^{+1} \\
085715^{+1} \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \\
941516 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \\
0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \\
0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416 \quad 0.1416
\end{array}$$

$$\begin{array}{l}
J\alpha = - 5.12 \\
J\beta = - 1.530
\end{array}$$

$$\begin{array}{l}
\delta_{\lambda\lambda}^{\lambda\lambda} \quad q_2 = \quad J\pi \quad J\lambda \quad J\mu \quad J\eta \quad J\alpha \\
- 1.10^{+1} \quad - 1.10^{+1} \quad + 0.75 \quad + 4.12 \quad - 0.015 \quad - 0.001 \\
1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \\
1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \\
1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \\
1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1} \quad 1.10^{+1}
\end{array}$$

$$\begin{array}{l}
J\alpha = - 11.284 \\
J\beta = - 2.44
\end{array}$$

[illegible]

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	------

wa	wa	wa	wa	wa	wa	wa	wa	wa	wa
+51.409	-39.364	-43.880	-1.291	-12.601	+23.016	+4.302	-18.499		
+24.218	-28.701	-20.641	-2.634	-9.622	+15.926	-22.065	-28.459		
+22.855	-22.605	-23.447	-3.370	-8.003	+11.653	-9.126	-22.043		
+22.276	-12.025	-12.025	-2.205	-6.701	+11.653	-43.493	-52.522		
+10.944	0.000	0.000	0.000	-2.406	-0.000	-10.655	-2.120		
+11.858	+11.242	+13.321	+9.545	-2.357	-3.388	-14.322	+25.572		
+5.108	+15.914	+24.624	+17.510	-0.684	-3.921	-14.920	+43.521		
+1.882	+2.361	+15.345	+10.767	-0.155	-1.823	-0.136	+34.241		
+2.651	+12.277	+24.139	+16.564	-0.109	-2.651	-3.271	+50.140		
+0.656	+3.045	+9.469	+6.504	-0.009	-0.607	+1.020	+20.580		
+5.100	+0.090	+0.090	+8.550	+13.860	-20.700	-2.560	-6.570		
+2.200	+0.162	+0.324	+6.885	+12.231	-24.057	-8.745	-5.613		
+6.450	+0.255	+0.432	+5.328	+10.512	-18.936	-5.832	-1.225		
+5.200	+0.193	+0.31	+2.862	-7.017	-4.903	-6.294	+0.792		
+2.310	+0.517	+0.821	+0.851	+3.223	-1.125	-0.730	+5.867		
+1.560	+1.238	+2.044	+1.434	+2.379	+2.470	-0.458	+11.437		
+0.766	+1.465	+2.830	+1.949	+0.680	+3.511	-1.015	+9.744		
+0.102	+0.525	+1.414	+0.967	+0.149	+0.101	-1.225	+2.450		
+0.252	+1.157	+2.055	+1.427	+0.174	+2.355	+1.035	+3.461		
+0.040	+0.234	+0.530	+0.258	+0.010	+0.630	+0.566	+2.365		
+218.075	-45.400	-13.735	+50.284	+8.318	-35.721	-143.863	+67.958		
[a]	[a]	[e]	[d]	[e]	[a]	[u]	[u]		

210.2 + 67.058

Wb ₁	Wb ₂	Wb ₃	Wb ₄	Wb ₅	Wb ₆	Wb ₇
+ 30.140	+ 33.599	+ 0.689	+ 9.117	- 17.623	- 3.294	+ 14.164
+ 20.950	+ 22.405	+ 1.937	+ 7.024	- 11.626	+ 16.106	+ 25.045
+ 15.553	+ 16.132	+ 2.319	+ 5.506	- 8.018	+ 6.279	+ 15.166
+ 6.742	+ 6.742	+ 2.035	+ 3.243	- 0.318	+ 21.051	+ 25.567
+ 0.000	+ 0.000	+ 0.000	+ 0.000	- 0.000	- 0.000	+ 0.000
+ 10.658	+ 12.629	+ 9.052	- 2.263	- 3.212	- 13.579	+ 24.523
+ 48.720	+ 75.364	+ 53.606	- 2.004	- 12.005	- 45.370	+ 134.155
+ 37.157	+ 68.154	+ 47.841	- 0.689	- 8.103	- 0.603	+ 152.143
- 5.675	+ 14.533	+ 50.012	- 0.503	- 12.577	- 15.521	+ 27.896
- 23.717	+ 56.030	+ 39.106	- 0.049	- 4.155	+ 6.136	+ 125.597
- 0.001	+ 0.001	+ 0.035	+ 0.154	- 0.330	- 0.084	- 0.073
- 0.004	+ 0.007	+ 0.183	+ 0.272	- 0.535	- 0.194	- 0.131
- 0.007	+ 0.009	+ 0.257	+ 0.467	- 0.842	- 0.259	- 0.077
- 0.006	+ 0.025	+ 0.099	+ 0.273	- 0.338	- 0.121	+ 0.027
- 0.116	- 0.183	+ 0.190	+ 0.721	- 0.252	- 0.163	+ 1.312
- 16.257	+ 1.909	+ 1.339	+ 2.223	+ 2.309	- 0.456	+ 10.687
- 24.766	+ 7.909	+ 5.424	+ 1.013	+ 9.781	- 5.235	+ 27.144
- 3.535	+ 2.065	+ 4.149	+ 0.638	+ 0.692	- 5.267	+ 10.640
+ 2.307	+ 0.576	+ 6.543	+ 0.793	+ 10.813	- 4.748	+ 38.442
+ 1.164	+ 3.101	+ 2.004	+ 0.058	+ 3.686	+ 2.311	+ 13.852
- 43.500	- 43.500	- 27.227	- 12.115	- 22.056	- 32.111	- 35.610
		[kd]	[ke]	[kf]	[kg]	18

wee	wed	wee	wee	- wee	wee
+ 37.454	+ 1102	+ 10.832	- 119.645	- 3.672	+ 15.790
+ 23.957	+ 2072	+ 7.511	- 12.482	+ 17.223	+ 20.045
+ 16.733	+ 2405	+ 5.712	- 4.317	+ 6.513	+ 15.731
+ 6.741	+ 2.035	+ 3.243	- 0.315	+ 21.052	+ 22.867
+ 0.000	+ 0.000	+ 0.000	- 0.000	- 0.000	+ 0.000
+ 14.064	+ 10.726	- 6.681	- 3.806	- 16.059	+ 24.064
+ 116.640	+ 42.944	- 3.240	- 18.570	- 70.200	+ 207.576
+ 125.136	+ 87.501	- 1.265	- 14.571	- 1.107	+ 270.223
+ 219.521	+ 153.566	- 1.541	- 24.139	- 29.789	+ 456.590
+ 136.656	+ 93.871	- 0.117	- 10.053	+ 14.729	+ 261.455
+ 0.001	+ 0.095	+ 0.154	- 0.330	- 0.054	- 0.073
+ 0.014	+ 0.306	+ 0.544	- 1.069	- 0.359	- 0.263
+ 0.029	+ 0.355	+ 0.701	- 1.262	- 0.359	- 0.115
+ 0.101	+ 0.345	- 1.092	- 1.550	- 0.552	- 0.169
+ 0.242	+ 0.302	+ 1.145	- 0.400	- 0.259	+ 0.054
+ 2.245	+ 1.574	+ 2.613	+ 2.714	- 0.536	+ 12.563
+ 11.424	+ 7.542	+ 2.772	+ 14.125	- 7.706	+ 34.205
+ 10.397	+ 7.113	+ 1.094	+ 1.156	- 9.029	+ 15.240
+ 17.280	+ 11.809	+ 1.440	+ 19.512	- 8.569	+ 70.272
+ 7.023	+ 4.743	+ 0.132	+ 8.345	+ 7.499	+ 31.376
- 46.908	+ 471.055	+ 30.141	- 70.653	+ 64.547	+ 1534.475
(co)	[cd]	[ce]	[cf]	[cf]	[cf]

wee - wee

wee	wef	pen	ms
+ - 1.13	- 2.08	- 1.062	+ 4.700
+ 2.255	- 3.898	- 5.400	+ 4.410
- 1.440	- 2.520	+ 2.222	+ 5.200
+ 1.561	- 0.153	+ 10.129	+ 12.301
+ 0.529	+ 0.000	+ 2.343	+ 0.466
- 0.480	+ 0.682	+ 2.883	- 5.205
+ 0.090	+ 0.516	+ 1.950	- 5.766
+ 0.012	+ 0.150	+ 0.011	- 2.824
+ 0.011	+ 0.160	+ 0.209	- 3.200
+ 0.000	- 0.009	+ 0.013	- 0.255
+ 23.716	- 50.920	- 12.436	- 11.242
+ 20.521	- 40.363	- 14.677	- 9.920
+ 17.053	- 30.715	- 9.461	- 2.803
+ 11.330	- 14.651	- 9.555	+ 1.183
+ 4.444	- 1.569	- 1.018	+ 8.183
+ 5.042	- 2.159	- 0.624	+ 14.625
+ 0.672	+ 3.428	- 1.870	+ 9.512
+ 0.115	+ 0.125	- 0.950	+ 1.920
+ 0.120	+ 1.626	+ 0.714	+ 5.856
+ 0.003	+ 0.158	+ 0.142	+ 0.502
+ 91.656	- 140.671	- 26.162	+ 32.771
[e]	[f]	- [e]	[s]
		Check	+ 32.771

[3 f]	- w f n	w f s	www	- w w s
+ 10.304	+ 1.026	- 8.252	+ 0.260	- 1.548
+ 6.451	- 8.037	- 15.591	+ 12.382	+ 21.599
+ 4.134	- 3.237	- 7.591	+ 2.535	- 6.123
+ 0.015	- 0.493	- 1.206	+ 65.736	+ 79.837
+ 0.000	0.000	0.000	+ 10.379	+ 2.064
+ 0.965	- 4.092	- 7.392	+ 17.295	- 21.245
+ 2.058	+ 11.150	- 33.057	+ 42.250	- 124.930
+ 1.767	+ 6.132	- 23.182	+ 0.009	- 2.471
+ 2.651	+ 3.271	- 50.140	+ 4.037	- 61.574
+ 6.739	- 1.083	- 22.179	+ 1.585	+ 32.495
+ 108.000	+ 27.720	+ 24.090	+ 7.056	+ 6.132
+ 79.355	- 25.869	+ 19.512	+ 10.497	+ 7.096
+ 55.335	- 17.042	+ 5.049	+ 5.244	+ 1.555
+ 15.145	+ 11.524	- 1.465	+ 7.717	- 0.955
+ 6.545	+ 0.355	- 2.857	+ 0.231	- 1.553
+ 3.280	- 6.645	+ 15.187	+ 6.125	- 3.000
+ 17.472	- 9.530	+ 45.455	+ 5.195	- 26.443
+ 0.135	- 1.029	+ 2.080	+ 7.540	- 15.546
+ 22.032	+ 9.675	+ 79.349	+ 4.245	+ 24.843
+ 0.122	- 5.14	+ 37.277	+ 8.009	- 33.507
+ 345.144	+ 99.551	+ 47.882	+ 212.747	- 44.018
+ [3 f]	- [5 n]	[7 s]	[1 w]	- [1 s]
			clock	- 44915

$$\begin{aligned}
[u] &= +143.863 & [u] &= +218.073 & [u] &= +270.762 \\
[u] &= +32.714 & [u] &= -45.400 & [u] &= +435.283 \\
[u] &= +64.547 & [u] &= -13.735 & [u] &= +471.055 \\
[u] &= +30.930 & [u] &= +80.284 & [u] &= +257.224 \\
[u] &= +26.162 & [u] &= +8.318 & [u] &= +27.115 \\
[u] &= -99.551 & [u] &= -35.724 & [u] &= -52.686 \\
[u] &= +44.918 & [u] &= +67.958 & [u] &= +559.634 \\
[u] &= +100.151 & & & &
\end{aligned}$$

Normal Equations

$$\begin{aligned}
(1) & +218.073 - 45.400x - 13.735y + 80.284z + 5.318w = +143.863 \\
(2) & -45.400x + 270.762y + 435.283z + 257.224w = +32.714 \\
(3) & -13.735x + 435.283y + 746.908z + 471.055w = +64.547 \\
(4) & -80.284x + 257.224y + 471.055z + 42.644w = +30.930 \\
(5) & -26.162x + 27.115y + 42.644z + 52.686w = +26.162 \\
(6) & -99.551x - 52.686y - 97.052z + 140.671w = -99.551
\end{aligned}$$

The following is the solution of these normal equations:

	[u]	[u]	[u]	[u]	[u]	[u]
[u]	-45.400	-13.735	+80.284	+5.318	+443.863	+67.958
[u]	+270.762	+435.283	+746.908	+471.055	+2.1579491	+10.10061
[u]	+80.284	+257.224	+42.644	+52.686	+32.714	+14.1428
[u]	+52.686	+97.052	+140.671	+345.144	+62.6642	+52.715
[u]	+140.671	+345.144	+97.052	+10.10061	+1.7790371	+2.444030

[illegible]

[μ]	[μ]	[μ]	[μ]	[μ]	check
	[4, 214, 317 ₈]	+ 345, 1440	- 99, 5510	+ 147, 820	
		+ 5, 5512	- 23, 5649	- 11, 1316	
		+ 330, 2929	- 75, 4961	+ 59, 0136	+ 59, 0137
	[4, 561, 810 ₈]	+ 13, 8331	- 14, 4179	- 201, 0407	
		+ 325, 4898	- 61, 5652	+ 260, 0543	+ 260, 0543
	[4, 943, 006 ₂]	+ 23, 3081	- 26, 4057	+ 81, 2510	
		+ 302, 1517	- 35, 1625	+ 178, 5024	+ 178, 5024
	[0, 5, 40, 941 ₈]	+ 141, 1778	+ -1, 1466	+ 5, 1637	
		+ 160, 4541	- 56, 3591	+ 175, 2372	+ 175, 2372
		+ 46, 5125	- 4, 0959	+ 13, 4325	
	[6, 043, 538 ₂]	+ 114, 4413	- 47, 3636	+ 161, 8044	+ 161, 8045
		[2, 555, 770]	[0, 5, 40, 941 ₈]	[2, 555, 770]	

[n]	[n]	[n]
+ 212, 7470	+ 44, 9190	
+ 94, 4057	+ 44, 8316	
+ 117, 8413	+ 0, 0864	
+ 15, 0275	+ 209, 5305	+ 0, 0862
- 192, 5160	- 209, 5305	+ -0, 0862
+ 29, 9151	- 92, 0802	
+ 76, 8059	- 117, 4029	
- 17, 1711	+ 6, 8852	
+ 69, 2168	- 117, 4381	- 117, 4029
+ 17, 399	- 2, 5091	- 117, 4381
+ 67, 9770	- 115, 3400	- 115, 3402
+ 10, 6020	- 66, 9651	
- 48, 3750	- 48, 3746	

Attaining the necessary dimensions we find the following

w	u	$=$	x	y
-0.41356	+0.21351	-0.51928	-0.09377	+0.23951
	-0.45756	-1.43157	+0.36304	-0.09522
		+1.45152	-0.13741	+0.02691
			+1.12552	+1.57177
				-0.59145
				+0.23171
-0.41356	-0.24375	-1.40932	+0.35737	+1.15151
[0.01685-0.01]	[0.35094-0.01]	[0.17584-0.01]	[0.55311-0.01]	[0.06135-0.01]
$r \pm 0.12$	$r \pm 0.24$	$r \pm 0.55$	$r \pm 0.55$	$r \pm 0.55$

Calculation of the weights of the deduced quantities:

d	x	y	z	w
	0.03640	0.89510	0.14420	0.00502
		0.43760	0.57140	0.00502
			0.77196	0.00502
				0.00502
+0.0046	+0.0028	+0.0330	+0.0152	+0.00502
+0.0002	+0.0004	+0.0477	+0.0047	+0.00502
-0.0020	+0.0032	+0.1003	+0.0001	+0.00502
-0.0119	+0.0517	+0.0151		+0.00502
+0.0060	+0.0056			+0.00502
+0.0265	+0.1547	+0.1061	+0.1930	+0.00502
[0.57157]	0.80051	0.07952	0.71444	+0.00502
b_1	b_2	b_3	b_4	b_5
0.65	0.51	0.52	0.52	0.52

Calculation of the weights of the deduced quantities:

(11)	(12)	(13)	(14)	(15)	(16)	(17)
t_1 0.37840	0.37475	0.36922	0.24044	0.23163	0.18752	0.1640
x_1 0.23805	0.23805	0.20612	0.202314	0.00000	0.16435	0.1410
y_1 0.30963	0.26717	0.27221	0.025312	0.00000	0.13800	0.13051
z_1 0.77815	0.20412	0.38011	0.50515	0.00000	0.09342	0.1453
u_1 0.77400	0.76443	0.27872	0.70770	0.62325	0.41100	0.1760
w_1 0.02908	0.98227	0.11100	0.63047	0.00000	0.61070	0.1300

(18)	(19)	(20)
t_1 0.98677	0.97313	0.11049
x_1 0.63448	0.64833	0.6103
y_1 0.89818	0.9347	0.6711
z_1 0.74429	0.72600	0.7412
u_1 0.70304	0.71710	0.7100
w_1 0.97313	0.97313	0.97313

(21)	(22)	(23)	(24)	(25)	(26)	(27)
t_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044
x_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044
y_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044
z_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044
u_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044
w_1 0.97044	0.97044	0.97044	0.97044	0.97044	0.97044	0.97044

(28)	(29)	(30)
t_1 0.49136	0.46240	0.30100
x_1 0.12385	0.12385	0.12385
y_1 0.12385	0.12385	0.12385
z_1 0.12385	0.12385	0.12385
u_1 0.12385	0.12385	0.12385
w_1 0.12385	0.12385	0.12385

t_n	0.22317	0.22422	0.22467	0.22471	0.22476
x_n	0.22383	0.22443	0.22471	0.22471	0.22476
y_n	2.86272	2.82072	2.77340	2.77843	2.77843
z_n	8.95404	2.38001	2.5610	2.6110	2.6110
u_n	2.15777	2.15037	2.14281	2.14281	2.14281
v_n	2.62624	2.59912	2.53574	2.53574	2.53574

(2)	(2)	(3)	(4)	(4)
0.22476	0.22476	0.22476	0.22476	0.22476
0.22476	0.22476	0.22476	0.22476	0.22476
2.77843	2.77843	2.77843	2.77843	2.77843
2.6110	2.6110	2.6110	2.6110	2.6110
2.14281	2.14281	2.14281	2.14281	2.14281
2.53574	2.53574	2.53574	2.53574	2.53574

t_s	0.10371	0.10371	0.10371	0.10371	0.10371
x_s	8.06138	8.36241	8.66344	8.96447	9.26550
y_s	2.55312	8.15518	8.35127	8.54736	8.74345
z_s	0.15361	0.10521	0.04512	7.84799	9.64302
u_s	2.57446	2.56592	2.55129	2.50088	2.41222
w_s	0.13537	0.08962	0.03682	7.82269	9.11006

2.93480	2.77272	2.64080	2.41187	2.18294
2.1725	2.1117	2.1117	2.1117	2.1117
2.27119	2.27119	2.27119	2.27119	2.27119
2.24057	2.24057	2.24057	2.24057	2.24057
2.27903	2.27903	2.27903	2.27903	2.27903
2.52532	2.23701	2.01180	0.04902	0.04902

$-2u_n$	+0.20	-1.33	-0.65	-1.1	-1.6	-1.86	-1.1	-1.07
t_n	+2.37	+2.34	+2.30	+2.29	+2.20	+2.17	+1.61	+1.37
x_n	-2.11	-1.77	-1.85	-1.22	0.0	+1.68	+2.02	+2.96
y_n	-0.73	-0.66	-0.60	1.1	0.0	+0.62	+1.81	1.00
z_n	1.837	1.834	1.830	1.830	1.830	-1.86	-5.76	-8.32
u_n	+0.14	+0.14	+0.14	+0.12	0.0	+0.01	+0.04	+0.02
w_n	-0.44	-0.40	-0.34	-0.21	-1.0	+0.77	+0.36	+0.29
v_n	1.0	1.0	1.0	-1.42	+0.24	0.0	-1.05	+1.02

$-H_1$	-1.1	+1.2
f_1	+1.1	+1.1
γ_1	+1.1	+1.1
γ_2	+1.1	+1.1
γ_3	+1.1	+1.1
γ_4	+1.1	+1.1
γ_5	+1.1	+1.1
γ_6	+1.1	+1.1
γ_7	+1.1	+1.1
γ_8	+1.1	+1.1
γ_9	+1.1	+1.1
γ_{10}	+1.1	+1.1

$-H_1$	-1.1	-1.1	-1.1	-1.1	-1.1	-1.1
f_1	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_1	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_2	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_3	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_4	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_5	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_6	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_7	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_8	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_9	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_{10}	+1.1	+1.1	+1.1	+1.1	+1.1	+1.1

$-H_1$	-1.1	-1.1	-1.1	-1.1	-1.1
f_1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_1	+1.1	+1.1	+1.1	+1.1	+1.1
γ_2	+1.1	+1.1	+1.1	+1.1	+1.1
γ_3	+1.1	+1.1	+1.1	+1.1	+1.1
γ_4	+1.1	+1.1	+1.1	+1.1	+1.1
γ_5	+1.1	+1.1	+1.1	+1.1	+1.1
γ_6	+1.1	+1.1	+1.1	+1.1	+1.1
γ_7	+1.1	+1.1	+1.1	+1.1	+1.1
γ_8	+1.1	+1.1	+1.1	+1.1	+1.1
γ_9	+1.1	+1.1	+1.1	+1.1	+1.1
γ_{10}	+1.1	+1.1	+1.1	+1.1	+1.1

$\Sigma = 1 - 1.1$

$$1 - \frac{[v \bar{v}]}{m - \mu} \times 0.6745 \quad [v \bar{v}] \quad 1.68457$$

$$m - \mu \quad 1.14613$$

$$0.53844$$

$$\log y \quad 0.26922$$

$$9.81898$$

$$Y = \pm 0.012$$

$$r_{\ell} = \frac{r}{\rho_{\ell}} \quad \text{etc.}$$

With the substitutions we find

$$\begin{aligned} \Delta V_0 &= 100w \\ \Delta \Omega &= 0.12698 \Delta q - [0.06097] \Delta \pi + [1.89651] \Delta \mu \\ \Delta \mu &= 2.10 \\ \Delta \Omega &= 100y \\ \Delta q &= 10x \\ \Delta P_0 &= 1 - [0.12698] \Delta q - [0.06097] \Delta \pi + [1.89651] \Delta \mu. \end{aligned}$$

$$\begin{aligned} \log w &= 0.6168553n \\ u &= 0.3860446n \\ z &= 0.1728912n \\ y &= 0.5521181 \\ x &= 0.0613809 \\ t &= 0.1404747 \end{aligned}$$

$$\begin{aligned} \Delta i &= u - [8.70583] \Delta \Omega \\ &\quad - [8.70583] \Delta \Omega = [0.322688] = +2.10227 \\ u &= -0.24378 \\ \Delta i &= +1.8585 \end{aligned}$$

$$\begin{aligned} \Delta M_0 &= 1 - [0.12698] \Delta q - [0.06097] \Delta \pi + [1.89651] \Delta \mu \\ [1.89651] \Delta \mu &= -11.8142 \\ [0.06097] \Delta \pi &= -28.5462 \\ [0.12698] \Delta q &= -15.4208 \\ \Sigma &= -56.0902 \\ t &= +1.4108 \\ \Delta M_0 &= -54.6794 \end{aligned}$$

$$\begin{aligned} \Delta \Omega &= -41.346 \\ \Delta z &= +1.858 \\ \Delta \mu &= -0.1490 \\ \Delta \pi &= +38.737 \\ \Delta q &= +11.515 \\ \Delta V_0 &= -54.679 \end{aligned}$$

Applying these corrections to the elements together with the precession and the pericenter to reduce the elements to the epoch of 1884.0 we finally derive the following corrected elements

$$T = 1888.0$$

π	=	52° 21' 15"	$\Delta \pi$	=	+ 50.24
i	=	2 21 52	Δi	=	+ 62.11
δ	=	254 25 35	$\Delta \delta$	=	+ 62.11
$\delta + 72^\circ$	=	261 55 35	$\Delta \delta'$	=	+ 46.52
$\cos(\delta + 72^\circ)$	=	0.14451	$\Delta \delta$	=	+ 46.52
$\log 0.49$	=	0.69019	$\Delta \delta$	=	+ 62.11
$\sin(\delta + 72^\circ)$	=	0.98949	$\Delta \delta$	=	+ 62.11
$\cot i$	=	1.35481	Δi	=	+ 62.11
$\log 1.35$	=	0.13033	Δi	=	+ 62.11
δ'	=	11.57	Δi	=	+ 62.11
$\Delta \pi$	=	+ 50.24	Δi	=	+ 62.11
$\Delta \delta$	=	+ 62.11	Δi	=	+ 62.11
Δi	=	+ 62.11	Δi	=	+ 62.11

$$\begin{aligned} \log p &= 0.3321285 \\ \log q &= 0.0099045 \\ \log a &= 0.3420296 \\ \log h &= 3.5500066 \\ \log a^2 &= 0.5130429 \\ \log u &= 3.0360637 \\ u &= 1088.57 \end{aligned}$$

$$\begin{aligned} \Delta \pi &= + 50.24 \\ \Delta i &= + 62.11 \\ \Delta \delta &= + 62.11 \end{aligned}$$

Corrected Elements.

1884, January, 24.0 Greenwich M.T.

M	=	187° 31' 50.6	mean equinox and ecliptic 1884.0.
π	=	52 21 15	
δ	=	254 25 35	
i	=	2 21 52	
u	=	1088.57	

The author of the preceding paper, Charles Augustus Rufus Berst, was born in Middlebury, Windham County, State of New York.

His early education was acquired under a tutor. In the year 1871 he entered Clinton Liberal Institute where he remained four years, pursuing both the scientific and classical courses in which courses he was graduated in 1876. After graduation he was appointed Principal of the Union School at Cushman, N.H. where his appointment he accepted for one year.

He entered the Middlebury College in 1877 and at the expiration of four years was graduated with

1851 to the year of 1881

During this time he pursued in addition to the prescribed College course, graduate work in Mathematics and Astronomy under the Professor in Mathematics and the Director of the Litchfield Observatory, preparatory to the appointment as Assistant Astronomer in the Litchfield Observatory. This position was entered upon July, 1881 and held for seven years.

During this time he labored untiringly and his most important work is mentioned in the Observatory, especially may be mentioned the labor upon the "Celestial Charts" under construction, 30,000 of the 200 stars observed as a basis for twenty charts, were reduced ^{to} the common epoch of 1860.0. Also he made the reductions of 14,000 "Solar Spot" Observations and put the result in a form available for publication.

In the year 1886, pending a year's absence of the Director in Europe, he

to take charge of the Chair of Astronomy in the College,
and gave the required instruction in Astronomy.

In 1884 he received the Degree of
A. M. from Hamilton College.

As a special work in the service of
Astronomy the Author has, during the last seven years,
corrected from the astronomical literature the published
positions of the comparison stars used in various astronomical
investigations during the last half century and has reduced
them to a common epoch and formed two catalogues containing
together 25,000 star positions which work is ready for publication.

In June 1888 he was appointed
a Fellow in Astronomy in Johns Hopkins University and
in October he entered upon the work of setting and adjusting
the astronomical instruments and giving instruction in observing
and the reduction of observations.

The following year he was
appointed a member of the Academic Staff and has given instruction
in Astronomy up to the present time.

In the University he has attended
courses of lectures given by Professors Himel and Long and
under Professor Newcomb has followed the more advanced
studies in "Celestial Mechanics."

